

JAHRBUCH  
DES  
NORWEGISCHEN  
METEOROLOGISCHEN INSTITUTS  
FÜR  
1944

QC  
989  
.N8  
NL  
1944

HERAUSGEGEBEN  
VON  
DEM NORWEGISCHEN METEOROLOGISCHEN INSTITUT

LIBRARY

APR 2000

National Oceanic &  
Atmospheric Administration  
U.S. Dept. of Commerce

PREIS KR. 4.00

DRUCK BEI GRØNDHAL & SØN · OSLO 1945

**National Oceanic and Atmospheric Administration**

**Environmental Data Rescue Program**

**ERRATA NOTICE**

One or more conditions of the original document may affect the quality of the image, such as:

Discolored pages  
Faded or light ink  
Binding intrudes into the text

This document has been imaged through the NOAA Environmental Data Rescue Program. To view the original document, please contact the NOAA Central Library in Silver Spring, MD at (301) 713-2607 x124 or [www.reference@nodc.noaa.gov](mailto:www.reference@nodc.noaa.gov).

Information Manufacturing Corporation  
Imaging Subcontractor  
Rocket Center, West Virginia  
September 14, 1999

## **Die Barometer und die Barometerhöhen.**

Während der letzten drei Jahre sind die Instrumentkorrektion,  $c_1$ , aller norwegischen Barometer untersucht worden. Die Untersuchungen zeigen, dass die in den Jahrbüchern früher veröffentlichten Luftdruckwerte mehrerer Stationen korrigiert werden müssen. An einigen Stationen ist die Korrektion,  $d_{ps}$ , für alle Luftdruckwerte dieselbe, an anderen dagegen variiert sie mit dem Luftdruck. In diesen Fällen sind die Luftdruckintervalle mit den zugehörigen Werten von  $d_{ps}$  angegeben.

Durch Nivellement sind auch die Barometerhöhen ( $H_b$ ) kontrolliert und festgestellt worden. Die neuen Barometerhöhen einzelner Stationen in diesem Jahrbuch röhren deshalb nicht von irgend einer Verlegung der Stationen her, sondern nur von einer besseren Bestimmung der Barometerhöhen. Dies influiert in einigen Fällen auf die früher veröffentlichten Luftdruckwerte  $p_{0m}$  im Meeressniveau, so dass  $d_{ph}$  für einigen Stationen von  $d_{ps}$  verschieden ist.

Die früher veröffentlichten Luftdruckwerte der nachfolgenden Stationen sind deshalb mit den unten gegebenen Werten von  $d_{ps}$  und  $d_{ph}$  für die angegebenen Zeiträume für die folgenden Stationen zu berichtigten:

### **Nesbyen.**

1927--1940:  $d_{ps} = 0.3$  mb.

### **Gaustadtoppen.**

1934--1943: p: 760--775, 775--795, 795--815, 815--840, 840--860, 860--870 mb.

$d_{ps}$ : -- 1.0 -- 0.9 -- 0.8 -- 0.7 -- 0.6 -- 0.5

### **As:**

1940: p: 940--960, 960--1050 mb.

$d_{ps}$ : -- 0.5 -- 0.4 --

### **Dalen i Telemark.**

1929--1943:  $d_{ps} = 0.2$  mb.

1934--1943:  $d_{ph} = 0.3$  mb.

### **Lyngeør.**

1922--1937:  $d_{ps} = 0.2$  mb.

### **Tonstad.**

1936--1940: p: 960--980, 980--1010, 1010--1030 mb.

$d_{ps}$ : -- 0.6 -- 0.5 -- 0.4 --

### **Utsira.**

1922--1930:  $d_{ps} = 0.4$  mb.

### **Svandalsflona.**

1939--1940: p: 845--860, 860--880, 880--895, 895--905, 905--915, 915--925 mb.

$d_{ps}$ : -- 0.8 -- 0.9 -- 1.0 -- 1.1 -- 1.2 -- 1.3 --

### **Stirå.**

1936--1940:  $d_{ps} = 0.5$  mb.

## INHALT

Druckfehler und Verbesserungen . . . . .	S. V
Die Barometer und die Barometerhöhen . . . . .	S. VII
Vorwort . . . . .	S. IX
Zeichen- und Symbolerklärungen . . . . .	S. XIII
Verzeichnis der Stationen . . . . .	S. XIV
Stationskarte . . . . .	S. XVI
Registrierungen in Oslo (Blindern) von Luftdruck, Lufttemperatur, Relativer Feuchte, Wind und Niederschlag 1944 . . . . .	S. 1
Abweichungen der Monatsmittel vom Mittelwert 1901–1930 für Luftdruck und Lufttemperatur an ausgewählten Stationen 1944 . . . . .	S. 15
See-Temperatur für 11 Küstenstationen 1944 . . . . .	S. 15
Tägliche Beobachtungen (Extenso-Tabellen) 1944 in Oslo (Blindern), Bergen, Trondheim (Voll) und Tromsø . . . . .	S. 16
Monats- und Jahresübersichten 1944 für 140 Stationen . . . . .	S. 40
Pentadenmittel der Lufttemperatur 1944 für 38 ausgewählte Stationen . . . . .	S. 96

### Druckfehler und Verbesserungen.

**Im Jahrbuch für:**

													Steht	Lies
1921.	S.	119.	Kongens Grube.	Februar.	Bewölkung.	Mittel.....							7.3	7.1
1922.	»	103.	Plassen	Jahr.	Niederschlag.	Summe.....							683.9	583.9
1938.	»	76.	Sulstua	Jahr.	Windverteilung (Richtung) S.....								13.5	73.5
1939.	»	78.	Hattfjelldal.	April.	Windverteilung (Stärke) N.....								2.2	1.2
	»	78.	»	»	Jahr	»	»	»	»	»	»		1.3	1.2
1940.	»	124.	Vardo.	Juli.	Jp (1901—1930)								-5.0	-4.0
	»	124.	»	»	Jahr	»	»	»	»	»	»		0.7	0.8
	»	88.	»	»	Juli.	P <sub>m</sub>							06.1	07.1
	»	88.	»	»	Jahr	»							08.0	08.1
	»	88.	»	»	Juli	P <sub>om</sub>							07.6	08.6
	»	88.	»	»	Jahr	»							09.5	09.6
1941.	»	15.	Dombås.	Dezember.	Jp (1901—1930)								3.0	0.2
	»	15.	»	»	Jahr.	»	»	»	»	»	»		3.2	3.0
	»	40.	»	»	Dezember	P <sub>m</sub>							933.2	930.0
	»	40.	»	»	Jahr.	»							936.9	936.7
	»	40.	»	»	Dezember	P <sub>om</sub>							1013.3	1010.0
	»	40.	»	»	Jahr	»							1014.9	1014.7
1943.	»	44.	Vang på Hedmark.	November	T <sub>m</sub> , 19 Uhr								-0.6	-0.9
	»	44.	»	»	»	.	»	»	»	»	»		-0.9	-1.0
	»	44.	»	»	»	.	»	»	»	»	»		-2.9	-3.0

**1943: Grimstad: Mittlere Lufttemperatur.**

	Steht							Lies						
	8	14	19	Dies	Min	Min	Dat.	8	14	19	Dies	Min	Min	Dat.
Januar.....	-2.7	-1.4	2.0	-2.2	-4.5	-12.1	24	-3.0	-1.6	-2.3	-2.5	4.8	-12.1	24
Februar.....	3.0	5.8	3.7	3.8	1.1	-5.7	11	2.8	5.8	3.5	3.6	0.9	-5.9	11
März.....	3.4	6.9	5.1	4.6	1.5	-3.5	4	3.2	6.9	4.9	4.4	1.3	-3.7	4
November....	3.6	5.4	4.1	4.2	2.2	-4.0	19	3.4	5.2	3.9	4.0	2.0	-4.2	19
Dezember....	0.2	2.8	1.1	1.2	-1.7	-7.4	12	0.0	2.6	0.9	1.0	-1.9	-7.7	12
Jahr.....	7.8	10.1	8.6	8.1	5.0			7.8	10.0	8.5	8.0	4.9		

							Steht	Lies	
1943.	S.	56.	Kristiansand	S.	April.	T <sub>m</sub> 14 Uhr	.....	10.2	10.3
	*	*	*	*	*	*	Dies.....	7.0	7.1

Folgende Werte der geographischen Breite ( $\varphi$ ), der geographischen Länge ( $\lambda$ ) und der Stationshöhe ( $H$ ,  $H_s$ ) sind in den Jahrbüchern überall zu verbessern oder zu berichtigen:

**In den Jahrbüchern für:**

							Steht	Lies
1922—1926.	Svandalsflona	.....					H = 1081	H = 4048
1922—1934.	Nesbyen (Nes)	.....					H (H <sub>s</sub> ) = 165	H (H <sub>s</sub> ) = 164
	*	*	*	*	*	*	$\varphi = 60^{\circ} 35'$	$\varphi = 60^{\circ} 34'$
1922—1932.	Suul (Sul)	.....					H = 255	H = 233
1922—1943.	Nordli	.....					H (H <sub>s</sub> ) = 395	H (H <sub>s</sub> ) = 401
1927—1943.	Svandalsflona	.....					H (H <sub>s</sub> ) = 1060	H (H <sub>s</sub> ) = 1048
	*	Tonnes i Helgeland (Tonnes)	.....				$\varphi = 13^{\circ} 0'$	$\varphi = 13^{\circ} 1'$
1929—1943.	Tryvasshogda	.....					H (H <sub>s</sub> ) = 514	H (H <sub>s</sub> ) = 512
	*	*	*	*	*	*	$\varphi = 10^{\circ} 39'$	$\varphi = 10^{\circ} 41'$

		Steht	Lies
1931—1943.	Horten.....	$\lambda = 10^\circ 29'$	$\lambda = 10^\circ 28'$
"	" .....	$H(H_s) = 14$	$H(H_s) = 15$
1931—1932.	Tafjord .....	$H = \text{ca. } 24.5$	$H = 27$
1932—1943.	Østre Toten (Apelsvoll) .....	$\varphi = 60^\circ 43'$	$\varphi = 60^\circ 42'$
"	" .....	$\lambda = 10^\circ 51'$	$\lambda = 10^\circ 53'$
"	Hellisøy Fyr (Hellesøy) .....	$H(H_s) = 15$	$H_s = 20$
1933.	Tafjord .....	$H = \text{ca. } 24$	$H = 27$
1933—1943.	Sulstua (Sul) .....	$H(H_s) = 235$	$H(H_s) = 233$
1934—1943.	Vang på Hedmark (Vang) .....	$H(H_s) = 233$	$H(H_s) = 222$
"	Tafjord .....	$H(H_s) = 26$	$H(H_s) = 27$
1936—1943.	Karasjok .....	$H(H_s) = 135$	$H(H_s) = 131$
1940—1943.	Kjevli i Snåsa .....	$H_s = 216$	$H_s = 195$
1941—1943.	Sommarøy i Senja .....	$\varphi = 69^\circ 37'$	$\varphi = 69^\circ 38'$
"	" .....	$\lambda = 18^\circ 3'$	$\lambda = 18^\circ 1'$

### Hellisøy Fyr (Hellesey).

1931-1932;  $dp_s = -0.3$  mb.

### Lærdal.

1931-1943;  $dp_s = -0.5$  mb.

### Fanaråken.

1937-1940;  $dp_{2000\text{ gdm.}} = -0.2$  mb.

1941-1943;  $dp_s = -0.2$  mb.;  $dp_{2000\text{ gdm.}} = -0.4$  mb.

### Kinn:

1923-1931; p: 940-960, 960-990, 990-1020, 1020-1040 mb.

$dp_s = -0.4 \quad -0.3 \quad -0.2 \quad -0.1 \quad \rightarrow$

1941-1943; p: 940-960, 960-990, 990-1020, 1020-1040 mb.

$dp_s = -0.7 \quad -0.6 \quad -0.5 \quad -0.4 \quad \rightarrow$

### Tafjord.

1937-1943;  $dp_0 = 0.2$  mb.

### Ona.

1923-1936;  $dp_s = 0.2$  mb.

1937-1943;  $dp_s = -0.2$  mb.

### Sula Fyr.

1937-1943;  $dp_0 = -0.2$  mb.

### Trondheim.

1932-1943;  $dp_s = 0.2$  mb.

### Nordli.

1937-1943;  $dp_0 = 0.6$  mb.

### Nordøyan.

1930-1940;  $dp_s = -0.2$  mb.

### Alta.

1935-1939;  $dp_s = -0.6$  mb.

### Alta (Elvebakken)

1940-1943;  $dp_s = 0.6$  mb.

### Lingøy.

1925-1930;  $dp_s = 0.8$  mb.

1937-1943;  $dp_s = -0.4$  mb.

### Karasjok.

1922-1943; p: 935-950, 950-970, 970-990, 990-1005, 1005-1015, 1015-1025 mb.

$dp_s = -0.8 \quad -0.7 \quad -0.6 \quad -0.5 \quad -0.4 \quad -0.3 \quad \rightarrow$

1937-1943; p: 935-950, 950-970, 970-990, 990-1005, 1005-1015, 1015-1025 mb.

$dp_0 = -1.2 \quad -1.1 \quad -1.0 \quad -0.9 \quad -0.8 \quad -0.7 \quad \rightarrow$

## VORWORT

### Übersicht über den Inhalt.

Das Jahrbuch für 1944 enthält zweistündliche Werte (Registrierungen) für Luftdruck, Lufttemperatur, Relative Feuchte, Wind und Niederschlag in Oslo (Blindern). Ferner enthält es die täglichen Beobachtungen (Extenso-Tabellen) für Oslo (Blindern), Bergen, Trondheim und Tromsø, und die klimatologischen Daten (Monats- und Jahresübersichten) von 140 Stationen.

In Spezialtabellen sind die Abweichungen der Monatsmittel des Luftdrucks und der Lufttemperatur vom Mittelwert 1901 - 1930 für einige Stationen und die Monatsmittel der See-Temperatur für einige Küstenstationen angegeben. Pentadenmittel der Lufttemperatur für 38 Stationen sind auch in Spezialtabellen zu finden.

### Beobachtungen und Instrumente.

Von den 140 Stationen führen 66 Messungen des Luftdrucks aus. Die Messungen werden nur für 32 Stationen bearbeitet. Sämtliche Barometer sind Quecksilberbarometer (Gefäßbarometer mit reduzierter Skala). Von den Barometern haben 63 Millibarteilung, während 3 mit Millimeterteilung versehen sind. Diese letzteren sollen allmählich eingezogen werden. 57 Stationen haben Barograph.

Sämtliche Stationen messen die Lufttemperatur und dabei auch die Minimumstemperatur. Nur 31 der Stationen führen Messungen der Maximumstemperatur aus. Die Temperaturnessungen werden an 134 Stationen in speziellen Hütten, an 6 Stationen in kleinen Gehäusen am Fenster ausgeführt.

Die meisten Stationsthermometer sind Küchler-Thermometer mit Papierskala und  $\frac{1}{2}^{\circ}\text{C}$  Teilung. Die Minimumsthermometer sind gewöhnlicher Konstruktion mit Holzplatte und Milchglasskala mit  $\frac{1}{4}^{\circ}\text{C}$  Teilung. Die Extremthermometer sind Six-Thermometer mit  $\frac{1}{10}^{\circ}\text{C}$  Teilung. Die Temperaturextreme werden um 19 Uhr für die vorhergehenden 24 Stunden bestimmt und dem Datum des Messungstages zugeschrieben. 24 Stationen sind mit Thermograph versehen.

Messungen der Feuchte werden von 87 Stationen ausgeführt. Die Messinstrumente sind Haarhygrometer oder Psychrometer, und für die betreffende Station gibt das Stationenverzeichnis an, welches Instrument gebraucht und ob das Psychrometer aspiriert ist oder nicht. Die Haarhygrometer sind hauptsächlich die Russeltvedtschen Torsionshygrometer<sup>1)</sup>. An Stationen mit Psychrometerbeobachtungen ist die Relative Feuchte nach Jelineks und für Kältegrade nach Birkelands Tabellen berechnet worden. Auch für Kältegrade wird die Relative Feuchte im Verhältnis zur Sättigung über Wasser berechnet<sup>2)</sup>. An 6 Stationen befindet sich ein Hygrograph, an 7 ein Thermo-Hygrograph.

Sämtliche Stationen führen Windbeobachtungen aus. 81 Stationen haben Windfahne, während die Übrigen die Richtung schätzen. Die Windstärke wird immer nach der Beaufortskala angegeben<sup>3)</sup>. 22 Stationen haben Anemograph; an den Übrigen wird die Stärke geschätzt.

Niederschlagsmessungen werden an allen Stationen vorgenommen. Während des Sommers werden gewöhnliche Regenmesser mit kreisförmiger Auffangfläche benutzt; in Jahreszeiten aber, in denen der Niederschlag zum Teil als Schnee fällt, werden Schneemesser mit quadratischer Auffangfläche verwendet. Die Grösse der Auffangfläche ist 225 qcm. für sämtliche Niederschlagsmesser. Von den 140 Stationen sind 33 mit einem Nipherschen Windschutz versehen. Die Niederschlagshöhe wird stets durch Volumenmessung des aufgefangenen Wassers (Schmelzwasser wenn es sich um Schnee handelt) bestimmt. An 6 Stationen

<sup>1)</sup> Nils Russeltvedt: Ein neues Haarhygrometer. Met. Zeitschrift 1908, S. 396, 576.

<sup>2)</sup> B. J. Birkeland: Neue Feuchtigkeitstabellen für das Psychrometer unter dem Gefrierpunkt, Christiania 1907, Vorwort.

<sup>3)</sup> G. C. Simpson: The Velocity Equivalents of the Beaufort Scale, Professional Notes, No. 44, London 1926.

befindet sich ein Pluviograph. Die Niederschlagshöhe wird um 8 Uhr in Millimetern gemessen, und ist für denselben Tag eingetragen, an dem sie gemessen ist (viele Stationen messen auch die Niederschlagshöhe um 19 Uhr; diese Höhe wird der am folgenden Morgen gemessenen hinzugefügt). Um 8 Uhr wird auch die Schneetiefe in Zentimetern gemessen und die Schneedecke in der Skala 0—4 geschätzt.

#### Erläuterungen betreffend der Stationen.

In diesem Jahrbuch findet man dieselben Stationen wie im vorhergehenden ausser: Skudenes, Trondheim und Fleinvær. Neue Stationen sind: Glåben, Stavanger, Skudenes II, Maurset, Ørsta, Gjermundnes und Trondheim (Voll).

In Bezug auf die einzelnen Stationen ist folgendes zu erwähnen:

**Oslo (Blindern):** Am 2. Mai 1944 wurde das Barometer von einem Zimmer im 4. Stockwerk bis ins Barometerzimmer im Keller des Instituts verlegt. Dabei wurde die Barometerhöhe 95,6 m. Im Zeitraume 1. Januar—2. Mai 1944 sind aber alle Luftdruckwerte zu der neuen Barometerhöhe reduziert worden.

**Skudenes:** Die Station, die seit 1861 im Betrieb worden ist, wurde am 1. Januar 1944 durch eine neue Station, Skudenes II, ungefähr 650 m. W von der alten Station, abgelöst.

**Utsira:** Die neue Stationshöhe  $H_s$  und die neue geographische Breite  $\varphi$  führen von der Verlegung der Station am 27. Oktober 1943 her; siehe Jahrbuch 1943, Seite VI.

**Fanaråken:** Wegen mehrerer Lücken der Feuchtigkeitsbeobachtungen, ist die Relative Feuchte nicht veröffentlicht worden.

**Trondheim:** Am 12. Juni 1944hörten die Beobachtungen auf. Am 5. Juli 1944 fingen die Beobachtungen auf Voll, ungefähr 2,4 km SE von Trondheim, an. Auf Voll war schon früher eine private meteorologische Station im Betrieb und in den Extenso-Tabellen und Monatsübersichten sind deshalb die Beobachtungen auf Voll für das ganze Jahr 1944 gedruckt. Die meteorologische Station auf Voll wurde in den Jahren 1923—1931 vom Meteorologischen Institut getrieben und in den Jahrbüchern für 1927—1931 gedruckt.

Wegen der Evakuierung Finnmarks wurden auf Befehl des deutschen Wehrmachtsbefehlhabers die dortigen Stationen abgebrannt. Aus diesem Grund fehlen für mehrere Monate Übersichten für: Torsvåg, Loppa, Alta (Elvebakken), Galten, Ingøy, Kistrand, Sverholt, Sletnes Fyr, Tana, Vardø, Karibukt, Karasjok, Kautokeino und Siččajavre.

Die Sommerzeit ( $\Delta G = +2^h$ ) wurde in Norwegen am 3. April 1944 aufs neue eingeführt und hörte am 1. Oktober 1944 auf. Die Beobachtungen sind aber die ganze Zeit um 8,14,19 Uhr M.E.Z. beibehalten.

#### Verzeichnis der Stationen.

Die Seiten XIV und XV enthalten in Tabellenform die wichtigsten Erläuterungen über die im Jahrbuch für 1944 verwendeten 140 Stationen. Im Jahre 1944 waren noch 22 andere Stationen im Betrieb; von denen führten aber mehrere nur unvollständige Beobachtungen aus. Ausser den gedruckten Registrierungen in Oslo (Blindern), sind die Hyrogramme in Trondheim (bis Mai), die Thermo-, Hygro-, Anemo- und Pluviogramme in Bergen und die Thermo-Hyrogramme in Kristiansand S. ausgewertet worden.

#### Stationskarte.

Seite XVI enthält eine Karte über sämtliche Stationen, die in diesem Jahrbuch gedruckt sind. Die Karte ist in drei Teile geteilt: Süd-Norwegen, Nord-Norwegen und arktische Gebiete.

#### Die Registrierungen in Oslo (Blindern).

Die Seiten 1—14 enthalten die zweistündlichen Werte des Luftdrucks, der Lufttemperatur, der Relativen Feuchte, des Windes (Richtung und Geschwindigkeit) und des Niederschlags. Folgende Registrierinstrumente sind benutzt:

Ein Sprung-Fuess Laufgewichtsbarograph.

Ein Thermohygraph, Fuess Nr. 18463 M. I.

Ein Robinson Kontakt-Anemometer (2500). Die Registrierungen sind für jede zweite Stunde als Mittelwert der vorhergehenden Stunde angegeben. Windgeschwindigkeit in m/sek..

Ein Niederschlagsmesser, System Hellmann-Fuess Nr. 19415.

### Die Tabellen.

Die Tabellen sind nach den Beschlüssen der internationalen meteorologischen Organisation (Warschau 1935, Salzburg 1937) aufgestellt. Die verwendeten Symbole und Bezeichnungen sind in der Tabelle S. XIII gegeben.

Die Monatsmaxima und -minima von Luftdruck und Lufttemperatur und die Monatsminima der Relativen Feuchte sind in den Extenso-Tabellen fett gedruckt.

Ein gehobenes X gibt interpolierte Werte an.

### Die Extenso-Tabellen.

Die Seiten 16—39 enthalten die täglichen Beobachtungen an den 4 Stationen: Oslo (Blindern), Bergen, Trondheim (Voll) und Tromsø. Die Tabellen enthalten folgende Daten:

1. Den Monatstag.
2. Den Luftdruck an der Station in Millibar.
3. Die Lufttemperatur in Celsiusgraden.
4. Die Relative Feuchte in Prozent.
5. Die Windrichtung, in der Skala 01—32, und die Windstärke nach Beauforts Skala.
6. Die Sicht in der Skala 0—10, wo 10 eine Sichtweite grösser als 150 km. bedeutet.
7. Die Bewölkung, in der Skala 0—10, und das Wetter zum Termin mittels der internationalen Symbolen und Bezeichnungen auf Seite XIII.
8. Die Höhe des Niederschlags in Millimetern.
9. Die Schneehöhe in Zentimetern.
10. Den Witterungsverlauf mittels der internationalen Symbolen und Bezeichnungen auf Seite XIII. Die Zeitangaben sind auf 10 Minuten abgerundet.

### Die Monats- und Jahresübersichten.

Die Seiten 40—95 enthalten die klimatologischen Daten (Monatsmittel und Monatssummen) von 140 norwegischen Stationen. Die Tabellen enthalten:

1. Den Monat (I = Januar, . . . XII = Dezember).

2. Den Luftdruck in Millibar an der Station und auf das nächste Standard-Geopotential-niveau reduziert. (Jedoch für Røros und Dombås auf das Meeresniveau reduziert). Die Zahlen sind Mittel der drei täglichen Beobachtungen.

Vom 1. Januar 1944 sind neue Reduktionstabellen für die Barometer in Gebrauch genommen. Die neuen Tabellen sind gemäss: Arnt Eliassen: On the Correction and Reduction of Barometer Readings (Geof. Publ. Vol. XIII. No. 11) berechnet und geben zum Teil andere Werte für das Luftdruck im Meeresniveau als die alten Tabellen.

Für die Küstenstationen ist die Reduktion des Luftdrucks auf das Meeregniveau wie früher mit einem konstanten, vertikalen Temperaturgradienten ( $0.6^{\circ}/100\text{ m}$ ) vorgenommen. Für die Binnenlandstationen: Røros, Dombås, Rena, Flisa, Nordli und Karasjok ist ausserdem eine positive Temperaturkorrektion für niedrige Temperaturwerte benutzt worden. Die benutzte Temperaturkorrektion ( $\tau$ ) als Funktion von der Lufttemperatur ( $t_s$ ) geht aus der folgenden Tabelle hervor.

$t_s + 2$	0	-2	-4	-6	-8	-10	-12	-14	-16	-18	-20	-22	-24	-26	-28	-30	-32	-34	-36	-38	-40	-42	-44	-46	-48	-50
$\tau$	0.0	0.6	1.4	2.3	3.2	4.3	5.4	6.5	7.6	8.6	9.7	10.6	11.4	12.2	12.8	13.2	13.6	14.6	15.6	17.6						

Für die Stationen Dalen i Telemark und Vollen i Slidre ist die Reduktion des Luftdrucks auf das Meeres-niveau durch ein geographisches Interpolationsverfahren bestimmt (loc. cit. S. 10. Fourth method).

### 3. Die Lufttemperatur in Celsiusgraden. Die Monatsmittel (*Dies*) sind nach der Formel<sup>1)</sup>

$$m = n - k(n - \text{Min.})$$

berechnet, wobei  $n$  das einfache Mittel aus den drei festen täglichen Beobachtungen und  $k$  ein Faktor ist, der mit der Station und dem Monat wechselt<sup>2)</sup>.

4. Die Windverteilung. Für die 8 Hauptrichtungen (32 = N, 04 = NE, 08 = E, . . . . 28 = NW) sind für jede Richtung die Anzahl der Fälle mit der dazugehörigen mittleren Windstärke (Skala Beaufort) angegeben. Alle Beobachtungen mit ungerader Richtungszahl (01, 03, 05 . . . 31) sind gezählt, als ob sie zu der benachbarten Hauptrichtung gehörten (31 und 01 als 32, 03 und 05 als 04 . . . . ). Die Richtungen 02, 06, 10, 14, 18, 22, 26 und 30 sind mit einer Hälfte der Anzahl auf die beiden benachbarten Hauptrichtungen verteilt. (Deshalb kommt  $\frac{1}{2}$  in der Anzahl der Fälle vor). Die zugehörigen Zahlen der Windstärke werden entsprechend verteilt. Die Summe aller Windstärken für eine Hauptrichtung wird durch die entsprechende Anzahl der Beobachtungen dividiert, um die mittlere Windstärke der Richtung zu erhalten. Die Jahresmittel der Windstärke sind entsprechend ermittelt worden.

5. Die Relative Feuchte in Prozent. Die Monatsmittel sind nach der Köppen'schen Formel:

$$m = q + c(2p - q)$$

berechnet, wo  $q = \frac{1}{2}$  (Morgenbeob. + Abendbeob.) und  $2p = \text{Mittagsbeob.}^3)$ .

6. Die Bewölkung in der Skala 0—10.

7. Den Niederschlag in Millimetern. Monatssumme, nebst maximaler, täglicher Niederschlags Höhe mit Datum sind angegeben.

8. Zahl der Tage. Die 7 ersten Kolonnen brauchen keine Erklärung, wenn man sich nur daran erinnert, dass R in Millimetern gemessen wird.

Für die Stationen, die  $F_x$  (maximale Windstärke zwischen den Beobachtungsterminen) nicht beobachtet, wird die Aufzählung der Zahl Tage mit  $F \geq 6$ ,  $F \geq 8$ ,  $F \geq 9$  nur auf Grundlage der Terminbeobachtungen ausgeführt. Für die übrigen Stationen sind auch die Beobachtungen von  $F_x$  bei der Aufzählung zugrunde gelegt. (Im Stationenverzeichnis ist angegeben, welche Stationen  $F_x$  beobachten).  $F$  wird in Beaufort angegeben.

Als Regentage, Schneetage und Tage mit Regenschnee (Regen mit Schnee) sind diejenigen Tage gerechnet, an denen der Niederschlag  $\geq 0.1$  war. (Tage mit Nieseln sind auch als Regentage gerechnet, wenn der Niederschlag  $\geq 0.1$  gewesen ist). Tage mit Regenschnee sind nicht nur als Regenschneetage, sondern auch als Regentage und als Schneetage gerechnet. Als Tage mit Dunst sind nur diejenigen Tage gerechnet, wo der Dunst die Sichtweite auf 10 km. oder weniger reduziert hat. Als Tage mit Nieseln, Reifgräupeln, Frostgräupeln, Hagel, Gewitter, Nebel (Sichtweite  $< 1$  km.) und Sonnenschein sind diejenigen gerechnet, an denen die betreffende Erscheinung überhaupt beobachtet ist. Heitere Tage sind solche, an denen die Summe der Bewölkung für alle drei Beobachtungsstermine 5 oder weniger beträgt. Bewölkete Tage sind solche, an denen diese Summe 25 oder mehr beträgt. Als Tage mit Schneedecke sind die Tage mit Schneedecke 3 bis 4 gerechnet (mehr als die Hälfte des Bodens in der Umgebung mit Schnee bedeckt).

### Luftdruck- und Lufttemperaturabweichungen. See-Temperatur.

Seite 15 enthält die Abweichungen der Monatsmittel des Luftdrucks und der Lufttemperatur vom Mittelwert 1901—1930 für 16 bzw. 41 Stationen. Weiter enthält sie die Monats- und Jahresmittel der Temperatur des Oberflächenwassers für 11 Küstenstationen. Die See-Temperatur wird um 14 Uhr gemessen.

### Pentadenmittel der Lufttemperatur.

Die Seiten 96—97 enthalten die Pentadenmittel der Lufttemperatur für 38 ausgewählte Stationen. Die Mittel (*Dies*) sind nach der Köppen'schen Formel:

$$m = n - k(n - \text{Min.})$$

berechnet. Die Werte des Faktors  $k$  für die Pentaden sind im Jahrbuch für 1943 S. 96—97 angegeben.

<sup>1)</sup> H. Mohn: Mittheilungen aus dem Norwegischen Meteorologischen Institute, II. Die Temperatur der Luft. Met. Zeitschr. 1891, S. 253 ff.; B. J. Birkeland: Mittel und Extreme der Lufttemperatur, Geofys. Publ. XIV. 1, Oslo 1936, S. 9—10.

<sup>2)</sup> Jahrbuch des Norwegischen Meteorologischen Instituts für 1938, S. VIII und 135.

<sup>3)</sup> Die Werte des Faktors  $c$  sind im Jahrbuch für 1920, S. XI, angegeben.

*Oslo, im April 1945.*

## ZEICHEN- UND SYMBOLERKLÄRUNGEN.

**Symbole und Bezeichnungen, die in den Rubriken «Bewölkung und Wetter» und «Witterungsverlauf» der Extenso-Tabellen verwendet werden.**

∞	Höhenrauch.	└	Reif.
=	Dunst.	⤒	Glatteis.
☰	Nebel (Sichtweite < 1 km).	⤓	Rauhreif.
•	Nieseln.	⤔	Sturm ( $F_x \geq 9$ ).
•	Regen.	⦿	Sonnenschein.
*	Schnee.	⊕	Sonnen- oder Mondhalo.
*	Regen mit Schnee.	⊖	Sonnen- oder Mondkranz.
△	Griesel.	⤓	Regenbogen.
△	Eiskörnchen.	⤔	Nordlicht.
⤔	Eisnadeln.	n	nachts.
⤔	Regenschauer.	a	vormittags.
⤔	Schneeschauer.	p	nachmittags.
⤔	Schauer mit Regen und Schnee.	na	Zeit nach Mitternacht (frühmorgens).
*	Reifgraupeln.	np	Zeit vor Mitternacht (spät abends).
△	Frostgraupeln.	i	intermittierend.
▲	Hagel.	( )	Klammer wird verwendet für Erscheinungen in der Umgebung der Station.
⤔	Wetterleuchten.	0 und 2	und als obere Indices werden verwendet für Intensitätsangaben, 0 schwach oder leicht, 2 stark oder dicht.
⤔	Gewitter.		
+	Schneetreiben.		
⤔	Tau.		

### Übrige Symbole und Bezeichnungen.

P	Luftdruck.	$h_t$	Höhe der Kugel des Thermometers über dem Erdboden.
T	Lufttemperatur.	$h_a$	Höhe des Anemometers über dem Erdboden.
$T_1$	Seetemperatur.	$h_d$	Höhe des Windrichtungsanzeigers über dem Erdboden.
U	Relative Feuchte.	$h_r$	Höhe der Auffangfläche des Regenmessers über dem Erdboden.
D	Windrichtung.	$\Phi$	Geopotential.
v	Windgeschwindigkeit.	m	als untere Index, gibt das Mittel eines Elements an.
F	Windstärke.	n	als untere Index, gibt das Minimum eines Elements an (- Min).
C	Windstille.	x	als untere Index, gibt das Maximum eines Elements an (- Max).
V	Sichtweite.	—	über der Bezeichnung wird verwendet, um den Mittelwert anzugeben.
R	Niederschlagsmenge.	$\Delta$	Differenz.
N	Wolkenmenge.	$\Sigma$	Summe.
w	Wetter.	n	Zahl der Beobachtungen.
W	Witterungsverlauf.	An	Jahreswert.
$\varphi$	Geographische Breite.	M	Monatswert.
$\lambda$	Geographische Länge.	Dat	Datum.
g	Schwerebeschleunigung.	Dies	Tag.
$\Delta G$	Unterschied zwischen der benutzten Zeit und Greenwich Zeit.		
$H_s$	Höhe der Station über dem Meeresspiegel (nach den Richtlinien des Beschlusses von 1874 $H_s = H_r - h_r$ ).		
$H_b$	Höhe des Quecksilbergefäßes des Barometers über dem Meeresspiegel.		

# VERZEICHNIS DER STATIONEN

Station	Seite	<i>q</i>	<i>k</i>	<i>g</i>	H <sub>s</sub>	H <sub>b</sub>	ht	h <sub>a</sub>	hd	h <sub>r</sub>	Feuchte-Instrum. <sup>1)</sup>	Beob. von max. Windst.	Die Beobachtungs-termine Mittel-Europ. Zeit	Beobachter	
		N	E Gr.		m	m	m	m	m	m					
Åbjørsbråten .....	42	60° 55'	9° 18'		635		1.8	13.0	1.6	F <sub>x</sub>	8	14	19	O. Åbjørsbråten, Landmann.	
Ås .....	15, 52, 96	59 40'	10 46'		95		2.1	7.4	1.7	R	F <sub>x</sub>	8	14	19	Halvor Tønseth, Kontrollassistent
Alstahaug .....	80	65 54'	12 33'		ca. 8		2.0	1.2	1.7	R	F <sub>x</sub>	8	14	19	Irgens Kirkhus.
Alta (Elvebakken) .....	15, 90, 97	69 58'	23 22'	9.826	4	4.8	1.9	1.7	1.7	R	F <sub>x</sub>	8	14	19	Thomas E. Thomassen, Aufseher.
Alvdal .....	40, 96	62 1	10 48		485		1.8	1.5	1.5	R	F <sub>x</sub>	8	14	19	Frau Marit Nordrum Segård.
Andenes .....	15, 86	69 19'	16 7	9.826	5	7.0	1.9	10.9	10.2	R	F <sub>x</sub>	8	14	19	Aron Th. Hanssen, Leuchtturmwächter.
Anker .....	46	59 51'	10 26		157		1.9	2.0	2.0	R	F <sub>x</sub>	8	14	19	Landwirtschaftliche Schule.
Bergen (Fredriksb.) .....	15, 22, 64	60 24'	5 19	9.819	43	44.4	1.8	10.7	10.3	A,R	F <sub>x</sub>	8	14	19	Anton Bakke, Hausmeister d. Wet.dienstst.
Bergsdal .....	64	60 32'	6 3		540		1.9	2.9	2.9	R	F <sub>x</sub>	8	14	19	Frau Martha Bjerlo.
Berkåk .....	76	62 50'	10 1		425		1.8	10.2	1.8	R	F <sub>x</sub>	8	14	19	J. Asphaug, Kaufmann.
Bjørnfjell .....	84	68 26'	18 4		514		1.9	2.4	2.4	R	F <sub>x</sub>	8	14	19	Hagen Sundsfjord, Bahnhofsvorsteher.
Bodø .....	15, 82, 97	67 17'	14 28	9.824	33	35.0	1.8	15.0	15.0	R	F <sub>x</sub>	8	14	19	Hans B. Hansen, Versuchsassistent
Brandsøy i Kinn .....	68, 97	61 37'	5 8		10		3.8	2.2	2.2	R	F <sub>x</sub>	8	14	19	J. E. Søfteland, Pflanzschulleiter.
Brekke Sluse .....	52	59 9	11 34		114		2.0	8.5	1.5	R	F <sub>x</sub>	8	14	19	Harald Thorsen, Schleusemeister.
Brønnøysund .....	15, 78, 97	65 28'	12 12	9.823	4	5.3	2.0	8.8	1.5	P	F <sub>x</sub>	8	14	19	Peter Olsen, Kirchendiener.
Byglandsfjord .....	15, 56, 96	58 40'	7 48		207		1.9	10.9	1.7	R	F <sub>x</sub>	8	14	19	Ole A. Guldsmedmoen, Landmann.
Dagali .....	15, 50	60 25'	8 26		887		2.0	11.2	1.3	R	F <sub>x</sub>	8	14	19	Frl. Ragnhild Aasberg.
Dalen i Telemark .....	15, 54	59 27'	8 0	9.818	77	79.1	2.0	9.0	1.6	R	F <sub>x</sub>	8	14	19	Arne Bergland, Tischler.
Dikemark .....	48	59 48'	10 23		180		2.0	15.3	15.0	R	F <sub>x</sub>	8	14	19	Gunnar Aas, Diplomlandwirt.
Dividalen .....	15, 88	68 47'	19 44		202		1.5	1.2	1.2	R	F <sub>x</sub>	8	14	19	Joh. Stenvold, Forstbeamter.
Dombås .....	15, 40, 96	62 4	9 7	9.819	643	647.1	1.9	10	1.9	R	F <sub>x</sub>	8	14	19	Sverre Hodneland, Telegraphenbeamter.
Eggum .....	15, 86	68 18'	13 41		4		1.7	1.8	1.8	R	F <sub>x</sub>	8	14	19	Hans Eggvin, Lehrer.
Eidsberg .....	52, 96	59 30'	11 17		140		1.9	9.1	1.6	R	F <sub>x</sub>	8	14	19	Olav Bakka, Landmann.
Ekkerøy .....	94	70 4	30 6		7		1.7	1.9	1.9	R	F <sub>x</sub>	8	14	19	Einar Nielsen, Tischler.
Engerdal .....	15, 40	61 41'	12 1		479		2.0	15.0	1.8	A,R	F <sub>x</sub>	8	14	19	Frau Gunvor Sletmoen.
Fanaråken .....	68	61 31'	7 54	9.816	2064	2070.3	4.2	9.7	9.7	R	F <sub>x</sub>	8	14	19	Wetterwarte.
Fauske .....	82	67 15'	15 23		14		1.9	1.9	1.9	R	F <sub>x</sub>	8	14	19	Øistein Dragland, Telegraphenbeamter.
Ferde .....	15, 52	59 2	10 32	9.819	6	9.1	2.1	9.0	1.0	R	F <sub>x</sub>	8	14	19	M. Markussen, Leuchtturmwächter.
Fjærland .....	66	61 26'	6 46		5		1.6	12.0	1.1	R	F <sub>x</sub>	8	14	19	Ivar Boium, Landmann.
Flisa .....	15, 44, 96	60 37'	12 1		183		1.9	8.2	1.5	R	F <sub>x</sub>	8	14	19	Frau Ingeborg Sørknes.
Fokstua .....	42	62 7	9 17		952		1.8	6.8	1.5	R	F <sub>x</sub>	8	14	19	P. S. Kolstad, Telegraphist.
Fortun .....	66	61 30'	7 42	9.820	27	29.6	1.9	6.0	1.3	R	F <sub>x</sub>	8	14	19	Arne K. Fortun, Postbeamter.
Førde i Sunnfjord .....	68	61 27'	5 51		3		1.9	14.0	1.7	R	F <sub>x</sub>	8	14	19	Elisa Rydjqord, Telegraphenbeamtin.
Galten .....	15, 90	70 43'	22 44		4		1.9	1.8	1.8	R	F <sub>x</sub>	8	14	19	D. Schumacher, Kaufmann.
Gaustadtoppen .....	50	59 51'	8 40	9.815	1828	1828.8	2.1	4.5	1.3	R	F <sub>x</sub>	8	14	19	Wetterwarte, Hans Johnsen Tjonn.
Geilo .....	48	60 32'	8 13		795		1.9	2.6	2.6	R	F <sub>x</sub>	8	14	19	Dyrgrav, Bahnhofsvorsteher.
Gibostad .....	88	69 21'	18 5		ca. 6		2.0	1.8	1.8	R	F <sub>x</sub>	8	14	19	Einar Nyberg, Lehrer.
Gjermundnes .....	72	62 37'	7 10		51		1.8	5.6	1.4	R	F <sub>x</sub>	8	14	19	Finn H. Anfindsen, Lehrer.
Glomfjord .....	82	66 49'	13 59		39		1.6	1.8	1.8	R	F <sub>x</sub>	8	14	19	Kraftwerk, Glomfjord.
Globen .....	58	58 22'	7 27		364		1.8	6.0	1.8	R	F <sub>x</sub>	8	14	19	Frau Andrea Rosseland
Grimstad .....	56	58 20'	8 36		7		1.8	5.0	1.4	R	F <sub>x</sub>	8	14	19	Frantz L. Nilsen, Telegraphenbote
Grotøy .....	84	67 50'	14 47		6		2.1	1.5	1.5	R	F <sub>x</sub>	8	14	19	Alfred Dahl.
Gvær .....	15, 54, 96	59 24'	9 10		26		1.9	13.8	1.8	R	F <sub>x</sub>	8	14	19	Frau Marie Magnussen.
Haugastol .....	48	60 31'	7 52		990		2.0	7.8	2.4	R	F <sub>x</sub>	8	14	19	Frau Inez Hansen.
Helligvær .....	82	67 24'	13 54		14		2.0	1.7	1.7	R	F <sub>x</sub>	8	14	19	Harald Pedersen, Fischer.
Hellsøy Fyr .....	15, 64	60 45'	4 43		20		1.8	12.3	12.3	R	F <sub>x</sub>	8	14	19	Trygve Selvig, Leuchtturmwächter.
Horten .....	50, 96	59 25'	10 28		15		1.8	1.8	1.8	R	F <sub>x</sub>	8	14	19	Frau Inga Gundersen.
Ingegj .....	15, 90	71 4	24 9	9.827	4	4.3	1.9	10.9	10.6	R	F <sub>x</sub>	8	14	19	Oluf Digre, Kaufmann.
Jomfruland .....	54	58 52'	9 36		15		1.8	22.0	1.7	R	F <sub>x</sub>	8	14	19	Anders Johansen Gjøen, Leuchtturmwächter.
Karaajok .....	15, 94	69 28'	25 31	9.825	131	132.0	2.1	10.0	1.4	R	F <sub>x</sub>	8	14	19	Frau Anna Næss, Postbeamtn.
Karpbukt .....	15, 94, 97	60 40'	30 23		10		1.9		1.7	R	F <sub>x</sub>	8	14	19	Trygve Borthen, Kaufmann.
Kautokeino .....	94	69 0	23 2		308		1.9		1.8	R	F <sub>x</sub>	8	14	19	Frau Julie Oskal.
Kinn .....	15, 68	61 34'	4 48	9.820	8	8.2	1.8		1.4	R	F <sub>x</sub>	8	14	19	Peder Gjertsen, Telephonbeamter.
Kistrand .....	15, 92	70 27'	25 13		12		2.0		1.5	R	F <sub>x</sub>	8	14	19	Olaf Sætrum, Tischler.
Kjelvi i Snåsa .....	76, 97	64 10'	12 29		ca. 195		2.0	11.0	1.5	R	F <sub>x</sub>	8	14	19	Sverre Kjøbli, Landmann.
Klepp .....	15, 58, 96	58 48'	5 38		14		1.9		1.6	R	F <sub>x</sub>	8	14	19	Sverre Brørs, Pflanzschulleiter.
Kongeberg .....	50	59 40'	9 39		170		2.0	6.0	1.7	R	F <sub>x</sub>	8	14	19	Gottfred Loftus, Lagerwehrmann.
Kristiansand S. ....	50, 96	58 10'	7 59		23		2.0	12.1	1.6	R	F <sub>x</sub>	8	14	19	T. Nyberg, Agronom.
Krakene Fyr .....	15, 70	62 2	4 59		39		2.2	6.2	6.0	R	F <sub>x</sub>	8	14	19	Sverre Eriksen, Leuchtturmwächter.
Kutjern .....	44	60 34'	10 33		493		2.0	1.8	1.8	R	F <sub>x</sub>	8	14	19	Gudmund Gudmundsen, Telegraphist.
Leikanger .....	66, 97	61 11'	6 52		22		2.0		1.8	R	F <sub>x</sub>	8	14	19	Erling Kvale, Versuchsleiter.
Leka .....	78	65 6	11 42		ca. 50		2.1		1.7	R	F <sub>x</sub>	8	14	19	Knut Leknes, Landmann.
Lillehammer .....	15, 42, 96	61 6	10 29		226		2.0	10.9	1.4	R	F <sub>x</sub>	8	14	19	Thorleif A. Ulsaker, Landmann.
Listø .....	15, 58	58 6	6 34		13		2.1	6.2	5.7	P	F <sub>x</sub>	8	14	19	S. Rosstad, Leuchtturmwächter.
Loppa .....	90	70 20'	21 28		8		2.1		1.6	R	F <sub>x</sub>	8	14	19	Osvald Soelberg, Kaufmann.
Luster Samt. ....	66	61 26'	7 25		502		2.0	1.9	1.9	R	F <sub>x</sub>	8	14	19	Arne Skreiberg, Gärtner.
Lyngør .....	15, 54	58 38'	9 7		2		2.0		1.3	R	F <sub>x</sub>	8	14	19	N. C. Nielsen, Zollbeamter.

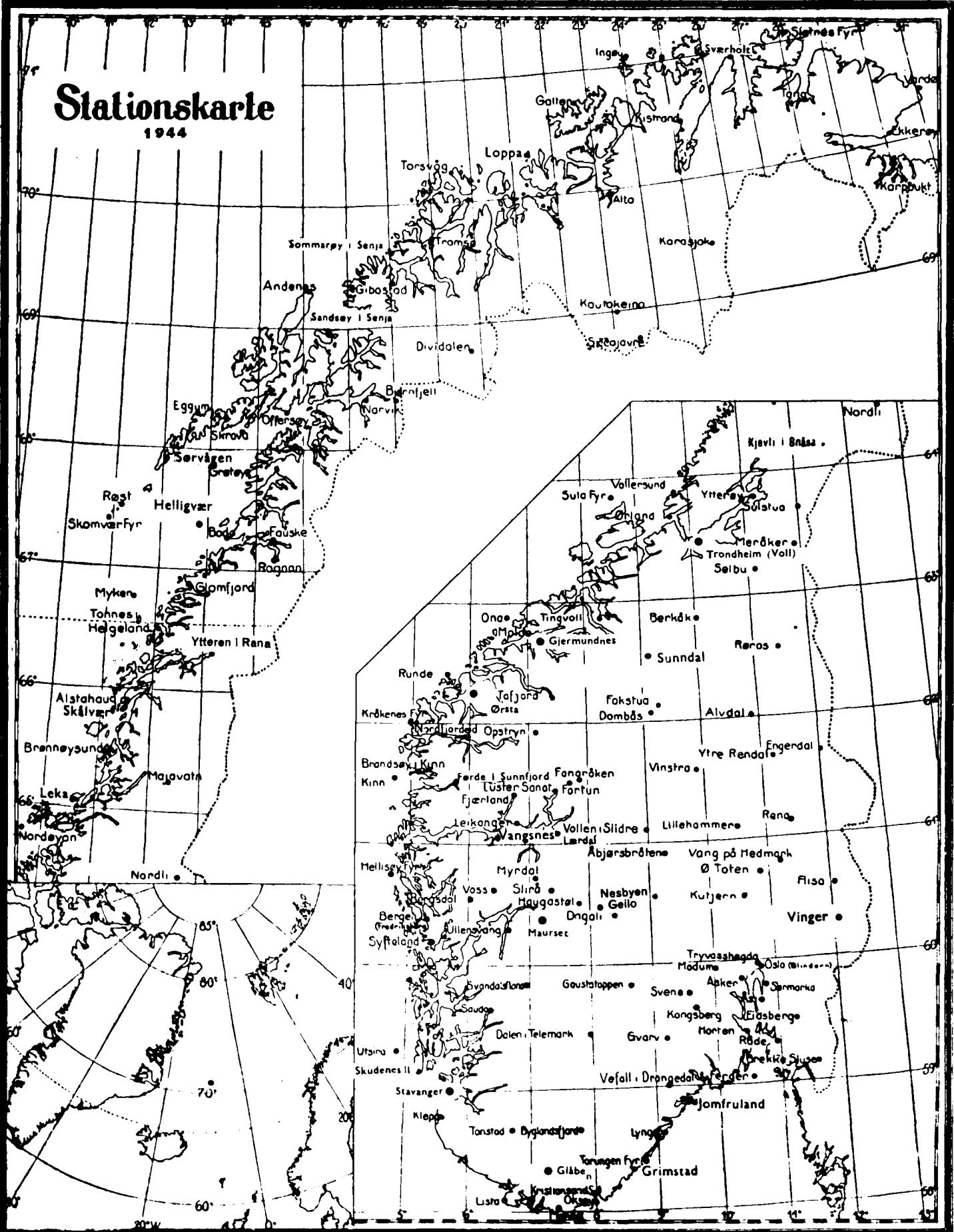
<sup>1)</sup> R: Russeltvedts Torsionshygr., A: Aspirations-Psychrometer, P: Gewöhnliches Psychrometer.

Station	Seite	$\varphi$	$\lambda$	g	H <sub>s</sub>	H <sub>b</sub>	ht	h <sub>a</sub>	hd	h <sub>r</sub>	Feuchte-Instrum. <sup>1)</sup>	Die Beobachtungs-terminen.	Mitteleurop. Zeit	Beobachter	
		N	E. Gr.		m	m	m	m	m	m	Beob. von max. Windst.				
Lærdal .....	15, 66	61° 6	7° 29'	9.819	3	4.0	1.8			1.4	P	F <sub>x</sub>	8	14	Ove Wangensten, Pensionist.
Majavatn .....	* 78	65 13	13 22		350		2.0			1.9	F <sub>x</sub>	8	14	A. Nilsen Kappfjelli, Landmann.	
Mandal .....	58	58 2	7 27		6		2.0		4.4	1.4	R	F <sub>x</sub>	8	14	Olav Nyvold, Telegraphenbeamter.
Maurset .....	62	60 25	7 20		778		2.0		12.7	2.0	R	F <sub>x</sub>	8	14	Leif Maurseth, Landmann.
Meråker .....	76	63 25	11 46		247		2.0		9.5	1.4	R	F <sub>x</sub>	8	14	Frau Astrid Olsen.
Modum .....	48, 96	59 58	9 58		133		2.0		6.6	1.3	R	F <sub>x</sub>	8	14	Chr. O. Ruud, Agronom.
Molde .....	72	62 44	7 10		50		1.9		17.3	1.7	R	F <sub>x</sub>	8	14	Edv. J. Kristensen, Kapitän.
Myken .....	15, 80	66 46	12 29		19		2.0			1.7	R	F <sub>x</sub>	8	14	Petter Moe, Dampfschiffsspediteur.
Myrdal .....	62	60 44	7 7		870		1.9	9.6	7.4	2.6	R	F <sub>x</sub>	8	14	Thorvald Johan Finkelsen, Telegraphist.
Narvik .....	84	68 25	17 23		40		1.9		ca. 9.6	1.8	R	F <sub>x</sub>	8	14	Arne Skindlo, Agronom.
Nesbyen .....	15, 48, 96	60 34	9 6		164		2.0		11	1.7	R	F <sub>x</sub>	8	14	Frl. Asta Wollo.
Nordfjordeid .....	68, 97	61 56	6 6		71		1.8			1.7	R	F <sub>x</sub>	8	14	Frau Pernille N. F. Leivdal.
Nordli .....	15, 78	64 28	13 36	9.821	401	402.2	1.9		10.1	1.4	R	F <sub>x</sub>	8	14	Birger Nordback, Telephonbeamter.
Nordøyan .....	15, 78	64 48	10 33		33		2.0	14.3	13	1.6	R	F <sub>x</sub>	8	14	H. Olufsen, Leuchtturmwächter.
Offerøy .....	15, 84, 97	68 20	15 38	9.825	16	20.4		14.1		1.7	P	F <sub>x</sub>	8	14	Magnus Os, Lehrer.
Oksoy .....	15, 56	58 4	8 3	9.818	9	10.2	2.1		8.1	1.8	R	F <sub>x</sub>	8	14	Arthur Boe, Leuchtturmwächter.
Ona .....	15, 72	62 52	6 33	9.821	12	14.6	1.8	6		1.1	P	F <sub>x</sub>	8	14	Sivert Jonas Viken, Postbeamter.
Opstryn .....	15, 70	61 56	7 13		205		1.9			1.8	R	F <sub>x</sub>	8	14	Frl. Ingebjorg Skære.
Oslo (Bindern) ...	1, 15, 16, 46	59 56	10 44	9.819	94	95.6	2.0	25.2	25.6	1.5	R	F <sub>x</sub>	8	14	Olsen, Bakken, Hausmeister d. Met. Inst.
Rena .....	44, 96	61 8	11 22	9.819	225	225.6	1.3		8.8	1.2	R	F <sub>x</sub>	8	14	Frl. Martha Alme, Photographin.
Rognan .....	82	67 5	15 22		ca. 28		2.0			0.9	R	F <sub>x</sub>	8	14	Petter Andreassen jr.
Runde .....	70, 97	62 24	5 39		22		1.8			1.3	R	F <sub>x</sub>	8	14	Frl. Karoline Runde, Telephonbeamtin.
Roros .....	15, 40, 96	62 34	11 23	9.819	628	630.0	1.8		14.4	1.9	R	F <sub>x</sub>	8	14	Harald Solbrække, Bahnhofsvorsteher.
Røst .....	15, 86	67 30	12 4	9.826	8	10.8	2.0	16.3	15.6	1.6	P	F <sub>x</sub>	8	14	Nils Cato Olsen, Telegraphenbeamter.
Røde (Tomb) .....	52	59 19	10 49		14		1.9			1.5	R	F <sub>x</sub>	8	14	Erling Magerey, Lehrer.
Sandsøy i Senja .....	84	68 57	16 40		17		2.1		8.0	1.8	R	F <sub>x</sub>	8	14	A. O. Skogslatten, Kaufmann.
Sauda .....	15, 60, 97	59 39	6 22		5		1.8			1.5	R	F <sub>x</sub>	8	14	O. Hana, Kontorist.
Selbu .....	74	63 12	11 7		197		2.0			1.4	R	F <sub>x</sub>	8	14	Olav Engen, Tischler.
Sicčjavro .....	15, 94	68 45	23 33		383		1.4			1.4	R	F <sub>x</sub>	8	14	E. E. Overgård, Landmann.
Skomvær Fyr .....	15, 86	67 25	11 53		13		2.3			1.5	R	F <sub>x</sub>	8	14	Alfred Skaar, Leuchtturmwächter.
Skrøva .....	84	68 9	14 39		11		2.0			1.7	P	F <sub>x</sub>	8	14	William Zahl, II. Leuchtturmwächter.
Skudeneshavn II .....	15, 60	59 9	5 15	9.819	7	9.2	2.0		3.0	1.8	R	F <sub>x</sub>	8	14	Lars Aadnesen, Landmann
Skálvær .....	80	65 52	12 11		4		1.9			1.7	R	F <sub>x</sub>	8	14	Henrik Jensen, Kaufmann.
Sletnes Fyr .....	15, 92	71 5	28 14	9.827	7	10.2	1.9	12.5	12.0	2.0	R	F <sub>x</sub>	8	14	Hermann Jensen, Leuchtturmwächter.
Slinå .....	15, 62	60 37	7 25		1300		3.2	11.5	10	4.0	R	F <sub>x</sub>	8	14	Sigurd Bergstrøm, Bahnaufseher.
Sommarøy i Senja .....	88	69 38	18 1		2		2.0			1.7	R	F <sub>x</sub>	8	14	Konrad Olsen, Aufseher.
Stavanger .....	60	58 57	5 44		85		2.4	10.0	10.0	1.2	R	F <sub>x</sub>	9	14	Eyolf Bakke-Eriksen
Sula Fyr .....	15, 74	63 51	8 28	9.822	27	30.0	2.0	5 4	12.2	1.6	R	F <sub>x</sub>	8	14	Johan Jostensen, Leuchtturmwächter.
Sulstua .....	5, 76	63 40	12 1		233		1.9			1.6	R	F <sub>x</sub>	8	14	John R. Brændmo, Landmann.
Sunddal .....	15, 72	62 33	9 7		195		2.0			1.6	R	F <sub>x</sub>	8	14	Frau Eli Nisja.
Svandalsflona .....	60	59 51	6 57		1048		3.1		8.2	3.3	R	F <sub>x</sub>	8	14	Torjuus Svandalsflona, Herbergswirt.
Svene .....	15, 50	59 46	9 35		176		1.9		8.5	1.6	R	F <sub>x</sub>	8	14	Frau Jørgine Hvila.
Sværholt .....	92	70 58	26 42		ca. 4		1.6			1.4	R	F <sub>x</sub>	8	14	Frau Lina Kraabol.
Syfteland .....	64, 97	60 14	5 27		53		5.6		7.5	1.2	R	F <sub>x</sub>	8	14	Wilhelm Jessen, Landmann.
Sormarka .....	46	59 48	10 49		157		2.0		11.6	1.5	R	F <sub>x</sub>	8	14	Ludvig Lande, Aufseher.
Sorvågen .....	86	67 54	13 2		20		1.9			1.4	R	F <sub>x</sub>	8	14	O. M. Rasmussen, Telegraphenbote.
Tafjord .....	70, 97	62 13	7 26	9.821	27	29.6	2.1		14.5	1.4	R	F <sub>x</sub>	8	14	Joh. Andersen, Maschinenmeister.
Tana .....	15, 92	70 27	28 16		5		1.7			1.7	R	F <sub>x</sub>	8	14	Adolf Henriksen, Kuhstallmeister.
Tingvoll .....	72, 97	62 50	8 19		51		1.8		9.7	1.6	R	F <sub>x</sub>	8	14	P. Oftedal, Maschinenmeister.
Tonnes i Helgeland .....	80	66 31	13 1		15		2.9			2.0	R	F <sub>x</sub>	8	14	Th. Lundlie, Telegraphenbeamter.
Tonstad .....	15, 58	58 40	6 42		57		2.0		9.5	1.4	R	F <sub>x</sub>	8	14	Frau Thrine Bjunes.
Torsvåg .....	90	70 15	19 30		22		1.9	4.8		1.8	R	F <sub>x</sub>	8	14	Einar Solem, Leuchtturmwächter.
Torungen Fyr .....	15, 56	58 24	8 48		12		2.0			1.4	R	F <sub>x</sub>	8	14	Christen S. Andersen, II. Leuchtturmwächter.
Tromsø .....	15, 34, 88, 97	69 39	18 57	9.825	102	114.5	2.8	12.3	20.7	1.7	A	F <sub>x</sub>	8	14	K. Lukkassen, Hausmeister, d. Wetter-dienst.
Trondheim (Voll) .....	15, 28, 74, 97	63 25	10 27	9.821	127	133.0	2.0		11.2	1.3	R	F <sub>x</sub>	8	14	Ole Tuset, Agronom.
Tryvasshøgda .....	46	59 59	10 41		51		2.1		20.3	2.0	R	F <sub>x</sub>	8	14	Widding-Danielsen, Telegraphenbeamter.
Ullensvang .....	15, 62, 97	60 19	6 40	9.819	15	12.3	2.4		8.5	1.8	R	F <sub>x</sub>	8	14	Frau Marita Aarhus.
Utsira .....	60	59 19	4 53		7		2.2			1.5	R	F <sub>x</sub>	8	14	Fridtjov Aspen, Leuchtturmwächter.
Vallersund .....	74, 97	63 51	9 44		4		2.0		7.8	1.4	R	F <sub>x</sub>	8	14	Kåre Stenstvedt, Telefonbeamter.
Vang på Hedm. ....	15, 44, 96	60 49	11 11		222		1.9		14.7	1.3	R	F <sub>x</sub>	8	14	Sigv. Gulbrandsen, Schulvorsteher.
Vangsnes .....	64	61 10	6 39		53		2.0		5.7	1.8	R	F <sub>x</sub>	8	14	Ole Larsen, Telefonbeamter.
Vardo .....	15, 92	70 22	31 6	9.826	10	12.1	1.9	9.2	10.0	1.8	R	F <sub>x</sub>	8	14	Frl. Ingerid Øien.
Vefall i Drangedal .....	54	59 0	9 13		68		2.0		12.3	1.6	R	F <sub>x</sub>	8	14	Hans Lautangen, Hausknecht.
Vinger .....	46	60 13	12 1		175		2.0			1.5	R	F <sub>x</sub>	8	14	Bjarne Sæbø, Schulvorsteher.
Vinstra .....	15, 42, 96	61 36	9 45		241		2.1			1.6	R	F <sub>x</sub>	8	14	Anton P. Thorsheim, Schmied.
Vollen i Slidre .....	15, 42, 96	61 6	8 58	9.819	403	404.6	2.0		12.0	1.7	R	F <sub>x</sub>	8	14	Frl. Olga Breyholtz.
Voss .....	62	60 38	6 26		62		2.0			1.7	R	F <sub>x</sub>	8	14	Torstein Seim, Hausmeister.
Ytre Rendal .....	40	61 41	11 12		253		1.9		14.5	1.6	R	F <sub>x</sub>	8	14	Frau Kjellang Åsheim, Berget, Postbeamter.
Ytteren i Rana .....	80, 97	66 21	14 8		29		1.9			1.6	R	F <sub>x</sub>	8	14	Frl. Othea Hjerpaa, Telefonbeamter.
Ytterøy .....	76	63 48	11 13		74		1.9		9.5	1.5	R	F <sub>x</sub>	8	14	Kristian Henning, Landmann.
Orland .....	74	63 41	9 40		12		1.9		11.1	1.5	R	F <sub>x</sub>	8	14	Petter Arnet, Agent.
Orsta .....	70	62 12	6 7		ca. 40		1.6			1.6	R	F <sub>x</sub>	8	14	Erik Berg, Assistent.
Ø. Toten .....	44 96	60 42	10 53		270		2.0		10.7	1.7	R	F <sub>x</sub>	8	14	Ivar Ørud, Diplomlandwirt.

<sup>1)</sup> R: Russeltvedts Torsionshygr., A: Aspirations-Psychrometer, P: Gewöhnliches Psychrometer.

# Stationskarle

1944



Registrierungen des Lufdrucks P

1944

**Oslo (Blindern)**

Januar I

$\varphi = 60^{\circ} 56' N$

$\lambda = 10^{\circ} 44' E$

$g = 9.819$

$\Delta G = +1^h$

$H_a = 94$

$H_b = 93.6$

$h_c = 2.0$

$h_d = 25.2$

$h_e = 25.6$

$h_f = 1.5$

Februar II

$\delta$	2	4	6	8	10	12	14	16	18	20	22	24	Max	Min	Dies	2	4	6	8	10	12	14	16	18	20	22	24	Max	Min	Dies	$\delta$		
1	89.2	84.2	80.0	76.8	76.6	76.1	75.7	76.7	76.8	80.3	81.4	82.7	92.8	75.6	79.88	95.8	95.7	95.3	94.7	93.6	90.7	88.6	85.8	82.2	79.7	78.5	95.9	78.5	89.64	1			
2	85.6	84.2	84.1	85.5	82.5	80.4	77.3	74.8	73.4	72.5	72.4	73.6	84.3	71.9	78.52	77.9	78.1	80.7	82.9	85.3	86.3	86.7	87.3	85.2	84.0	81.4	87.4	77.6	83.56	2			
3	74.1	73.8	73.2	73.6	75.6	76.2	77.0	77.8	78.7	80.2	83.1	85.7	95.7	73.0	77.42	79.4	77.6	76.4	75.2	74.2	73.0	71.2	69.6	68.6	67.9	67.5	66.9	81.4	66.9	72.29	3		
4	88.6	91.2	95.8	96.4	95.4	99.0	00.0	01.1	02.2	03.8	05.4	06.9	85.7	98.85	66.7	66.9	67.6	68.2	69.9	71.4	74.7	78.1	81.4	84.4	87.0	89.5	66.6	75.48	4				
5	86.5	89.6	10.4	10.9	10.6	09.5	05.2	01.1	97.7	93.6	88.7	11.3	88.7	04.38	91.5	95.2	94.9	97.3	99.8	01.8	02.6	04.0	05.8	07.4	09.0	10.4	89.5	01.48	5				
6	85.4	82.1	77.6	76.2	76.2	77.5	77.6	78.6	78.2	77.4	78.2	79.2	86.7	75.2	76.68	11.4	11.8	11.5	12.2	11.9	11.3	09.0	07.6	05.8	04.0	02.6	00.4	12.3	00.4	08.29	6		
7	79.2	80.0	80.3	81.1	85.2	85.4	87.2	89.3	91.2	92.5	93.5	95.8	86.30	97.9	94.5	90.8	87.0	82.5	78.9	75.7	72.6	70.0	69.5	67.6	00.4	67.6	80.06	7					
8	82.5	82.3	92.0	91.4	90.8	87.6	84.4	81.4	78.2	75.8	75.0	75.2	92.9	74.9	84.72	66.8	66.2	69.4	73.2	76.7	79.6	81.5	83.4	84.7	85.3	85.8	86.0	85.8	76.63	8			
9	73.2	75.8	74.6	74.8	75.1	75.9	76.1	77.6	78.9	80.4	81.8	82.1	77.36	85.9	85.7	85.6	85.9	84.7	85.6	83.1	82.8	83.1	83.9	84.8	86.0	84.8	84.58	9					
10	83.1	84.0	84.6	85.9	87.7	89.0	89.6	91.2	92.2	95.8	94.9	96.0	96.0	82.1	89.5	05.2	05.8	87.0	88.5	90.2	92.2	93.4	94.8	96.7	97.9	99.4	00.5	84.8	92.62	10			
11	96.8	97.1	97.0	97.4	98.3	98.8	99.7	01.1	02.1	02.8	03.4	04.2	94.2	96.0	99.89	00.4	00.7	00.9	01.2	01.4	01.6	01.5	02.0	02.8	04.4	06.3	06.3	00.2	02.05	11			
12	90.5	86.2	86.8	86.1	86.8	86.2	86.4	86.6	89.0	89.6	10.6	10.2	10.6	04.2	08.04	07.7	07.7	08.8	10.7	13.0	13.6	13.8	14.5	15.3	16.2	17.1	17.7	06.3	13.36	12			
13	10.7	10.6	10.2	09.8	09.1	08.3	07.1	05.8	02.9	00.5	96.3	95.3	95.3	05.42	17.8	17.8	18.1	18.9	18.8	18.6	18.2	17.4	17.1	16.6	16.5	16.4	16.4	17.70	13				
14	89.3	87.0	87.5	90.0	92.8	94.0	95.1	98.1	00.7	03.4	05.0	06.0	06.0	86.4	95.72	16.3	16.3	16.8	17.9	18.8	19.6	19.6	20.8	21.2	21.5	21.8	21.9	16.1	19.18	14			
15	86.5	87.1	88.3	10.0	11.7	12.7	14.2	15.2	15.8	16.6	16.9	17.3	06.0	12.70	22.0	21.9	22.2	22.5	22.4	21.4	21.0	20.8	20.5	20.1	19.9	22.8	19.9	21.38	15				
16	17.6	17.7	18.5	19.2	20.2	20.4	19.8	19.6	18.9	18.1	17.4	17.0	20.8	16.7	18.7	18.2	18.0	17.8	18.8	18.0	17.7	17.7	18.4	18.5	18.9	19.8	19.9	17.6	18.44	16			
17	17.0	17.2	17.0	16.8	16.9	15.5	14.4	13.0	11.4	09.8	09.1	09.0	13.92	20.2	20.5	21.3	21.9	22.7	25.1	22.9	23.0	23.5	24.1	24.4	25.0	25.0	19.8	22.72	17				
18	86.5	87.7	87.3	87.2	87.6	87.5	87.4	86.7	86.1	85.4	85.0	84.7	84.7	06.74	24.9	25.0	25.4	26.1	26.7	26.6	26.5	27.4	28.0	28.5	28.7	28.7	28.7	28.7	24.8	26.84	18		
19	85.8	85.7	85.3	85.9	84.4	84.6	84.6	85.1	85.4	85.9	86.4	86.4	86.4	03.1	04.79	26.8	26.8	26.8	26.8	26.1	27.4	27.5	27.5	27.6	27.6	27.6	27.6	27.6	28.10	19			
20	86.4	86.2	86.2	86.5	86.8	86.5	86.5	86.8	86.5	86.4	86.4	86.4	02.6	01.3	05.12	27.6	27.3	27.0	27.2	27.4	26.8	25.4	24.7	24.1	23.5	23.0	27.8	22.9	25.83	20			
21	99.3	96.9	95.8	90.8	89.8	89.0	88.0	87.8	88.4	88.7	88.8	88.5	01.3	88.5	90.82	25.0	22.3	22.3	22.0	21.0	21.0	20.2	20.0	19.8	19.1	18.3	17.2	17.2	20.52	21			
22	87.9	86.6	85.3	85.1	85.9	85.5	85.7	85.7	85.7	85.7	85.7	85.7	85.7	11.6	85.7	15.7	14.5	13.0	11.0	10.6	10.5	09.7	08.8	08.4	08.5	08.9	17.2	10.68	22				
23	72.1	71.5	70.6	68.6	69.5	62.1	58.7	57.0	57.1	58.1	59.2	60.0	72.4	57.0	60.9	09.5	09.4	09.3	09.5	10.0	09.9	09.3	09.0	10.1	11.5	12.2	12.3	12.4	10.17	23			
24	66.8	62.3	64.5	68.2	74.8	76.6	81.5	85.3	85.2	84.6	85.1	84.3	85.4	60.0	76.10	12.3	12.2	12.6	12.4	12.6	12.2	11.3	10.5	09.2	07.8	05.7	05.5	12.7	05.3	10.36	24		
25	80.9	80.6	78.9	77.1	75.9	74.3	72.1	71.1	70.5	70.3	71.1	72.3	04.3	70.2	74.59	04.2	02.0	02.0	02.0	02.0	02.0	02.0	02.0	02.0	02.0	02.0	02.0	02.0	02.0	02.0	02.0	25	
26	74.6	76.4	79.0	81.1	83.7	86.7	88.7	91.6	95.1	94.7	95.2	95.6	95.6	72.3	86.70	91.7	91.8	92.2	92.6	93.1	92.6	91.8	91.2	91.0	91.3	91.6	91.7	91.9	91.90	26			
27	95.8	92.7	89.1	86.5	85.7	81.1	79.0	76.2	75.3	76.2	77.8	80.0	95.6	74.8	82.62	91.4	91.4	91.3	91.8	95.1	95.7	95.8	94.1	95.0	95.8	96.5	96.6	95.71	27				
28	79.8	80.0	79.6	80.4	82.7	85.7	85.7	87.8	90.1	90.0	94.2	95.5	97.3	79.6	87.70	96.6	96.3	96.3	96.0	95.4	95.3	94.1	92.9	92.3	91.5	91.2	90.2	94.08	28				
29	80.2	81.6	81.9	81.5	81.0	80.1	80.1	80.6	80.6	80.6	80.6	80.6	80.6	80.7	87.05	97.05	97.05	97.05	97.05	97.05	97.05	97.05	97.05	97.05	97.05	97.05	97.05	97.05	97.05	97.05	29		
30	92.9	91.3	92.5	93.1	94.7	95.2	95.6	96.0	97.6	98.0	98.0	98.0	98.0	98.0	98.0	98.0	98.0	98.0	98.0	98.0	98.0	98.0	98.0	98.0	98.0	98.0	98.0	98.0	98.0	98.0	98.0	98.0	30
31	94.4	94.4	94.6	94.6	93.8	92.3	90.2	88.7	88.8	89.0	89.2	88.9	88.9	91.2	92.7	84.4	88.67	92.2	92.2	92.2	92.2	92.2	92.2	92.2	92.2	92.2	92.2	92.2	92.2	92.2	92.2	92.2	31
32	92.50	92.31	92.00	92.04	92.40	92.33	91.93	91.98	91.96	92.0	92.45	92.45	92.45	92.45	99.21	95.52	92.22	92.22	92.22	92.22	92.22	92.22	92.22	92.22	92.22	92.22	92.22	92.22	92.22	92.22	92.22	32	

März III

April IV

<

Registrierungen des Luftdrucks P

1944

Oslo (Blauborn)

Mai V

$\varphi = 59^{\circ} 56' N$

$λ = 10^{\circ} 44' E$

$g = 9.810$

$ΔG = +1^h$

$H_0 = 94$

$H_0 = 95.6$

$h_0 = 2.0$

$h_0 = 25.2$

$h_0 = 25.6$

$h_0 = 1.5$

Juni VI

D	2	4	6	8	10	12	14	16	18	20	22	24	Max	Min	Dies	2	4	6	8	10	12	14	16	18	20	22	24	Max	Min	Dies	D
1	96.5	95.9	95.5	95.0	94.0	92.5	91.2	91.2	92.1	93.0	93.7	97.7	91.0	93.69	93.9	04.0	04.4	04.7	04.6	05.8	05.3	02.4	01.0	01.4	01.6	04.8	00.8	03.02	1		
2	95.2	92.0	90.1	88.3	85.5	82.7	80.1	78.7	77.1	75.9	75.0	73.2	82.65	81.0	00.8	00.3	00.1	00.2	98.1	99.0	98.5	98.3	97.9	98.0	97.6	97.6	99.15	2			
3	72.4	71.7	71.8	71.7	72.0	72.7	74.1	76.0	78.4	80.4	82.9	84.7	71.5	73.73	97.6	97.6	97.8	98.0	98.2	98.3	98.3	98.3	99.0	99.1	97.4	98.20	3				
4	85.3	87.7	89.2	90.2	91.3	91.5	91.9	91.9	92.0	92.9	93.5	97.7	98.7	98.4	98.7	91.01	99.2	99.4	99.6	99.9	99.6	99.6	99.5	99.2	99.7	95.2	93.0	95.2	98.80	4	
5	93.4	93.2	93.1	93.6	93.6	93.3	93.3	93.6	94.2	95.3	96.8	98.4	98.4	98.1	94.32	95.6	95.2	91.1	91.4	90.8	90.4	90.7	91.0	91.2	91.3	91.6	92.3	92.5	90.3	91.58	5
6	99.8	91.2	82.4	83.5	84.7	85.4	86.1	87.1	88.3	89.0	90.0	92.2	94.0	96.22	92.5	92.7	92.9	93.6	94.0	94.0	94.0	94.5	94.9	95.2	95.1	94.1	95.3	98.5	95.96	6	
7	14.3	15.0	15.8	16.6	16.8	16.1	15.7	15.2	14.9	15.3	16.0	16.8	14.0	15.69	92.9	92.2	93.0	94.4	95.8	96.3	96.3	96.1	96.6	96.6	96.6	96.6	96.1	94.78	7		
8	17.0	16.9	17.5	17.6	17.5	16.6	15.5	14.4	13.8	14.1	14.2	14.0	13.8	15.76	92.7	92.6	92.2	92.4	92.1	91.9	91.5	90.8	90.7	90.6	90.6	90.2	90.6	91.68	8		
9	13.9	13.8	13.8	13.6	13.0	11.8	10.7	9.9	9.9	9.9	9.9	9.9	9.9	9.9	11.40	90.0	89.6	89.5	89.1	88.5	87.6	86.1	85.5	82.4	81.0	80.2	80.0	86.35	9		
10	07.3	06.6	05.9	05.4	04.4	05.4	05.4	05.4	02.6	01.5	01.4	01.4	01.4	01.4	08.62	88.8	88.1	87.5	88.1	81.0	82.0	85.2	84.2	85.2	86.5	87.9	87.9	83.3	83.15	10	
11	01.7	01.6	02.0	02.0	02.3	02.3	01.8	02.4	03.2	04.1	05.3	06.3	01.4	02.91	88.3	89.1	89.9	90.2	90.7	90.9	90.8	91.2	91.5	91.4	91.5	91.5	91.4	90.47	11		
12	06.4	07.3	07.5	08.0	08.2	08.0	08.2	08.5	08.8	09.6	10.0	10.3	06.1	08.40	91.1	91.1	91.1	91.4	91.0	90.8	91.2	91.6	92.5	92.5	92.5	92.5	91.66	12			
13	10.4	09.6	09.7	08.9	08.7	07.3	06.6	05.3	04.4	05.9	05.6	02.7	10.4	06.76	95.4	96.2	97.4	98.1	98.5	98.4	98.2	98.0	97.7	97.1	97.1	97.1	98.6	97.42	13		
14	02.2	01.5	01.3	00.9	00.9	00.4	00.4	00.3	00.5	00.5	00.5	02.7	00.59	93.1	90.8	88.0	84.2	87.5	89.2	90.1	90.5	91.1	91.7	91.7	91.7	91.7	90.88	14			
15	01.3	01.6	01.0	02.2	05.1	05.4	05.6	02.0	00.8	03.4	05.5	05.5	00.1	02.46	92.0	92.0	92.2	92.5	92.2	92.1	92.6	92.9	93.3	93.5	93.5	93.7	91.7	92.58	15		
16	07.7	09.0	10.5	11.4	12.5	12.9	13.1	13.1	13.5	14.5	14.6	14.6	05.5	12.12	95.9	94.2	94.3	94.7	95.4	95.6	96.4	97.5	99.3	91.3	92.0	92.0	95.6	96.70	16		
17	14.6	14.2	14.3	14.4	14.2	13.9	13.3	12.7	12.0	12.1	12.3	12.3	11.9	13.36	92.8	93.8	94.7	96.1	96.9	97.5	97.9	98.6	98.9	98.9	98.6	98.6	98.58	17			
18	12.0	11.7	11.9	12.1	11.5	10.5	09.5	08.7	08.0	07.9	08.1	07.8	07.8	09.38	93.9	90.9	10.1	10.4	10.4	09.7	09.0	08.6	09.0	09.2	09.9	09.9	10.4	10.5	08.6	09.66	18
19	07.9	07.3	06.9	06.4	05.2	03.5	01.7	09.9	98.5	97.6	98.5	00.9	07.9	97.2	92.86	10.7	11.2	11.7	11.8	11.6	11.1	10.4	10.0	09.7	09.6	10.3	10.2	10.0	10.19	19	
20	02.9	03.3	05.0	05.0	02.7	02.0	01.5	01.0	00.3	00.4	01.1	03.4	00.1	01.82	98.8	90.6	09.4	08.8	08.0	07.1	05.7	05.4	05.2	05.2	05.2	05.2	05.2	07.32	20		
21	99.3	97.8	96.0	95.9	95.4	92.3	90.9	89.5	89.3	89.2	89.6	89.6	01.1	89.2	92.57	05.0	05.2	06.0	06.9	06.1	05.6	04.9	03.4	02.5	02.6	03.5	04.1	06.9	04.65	21	
22	89.6	90.5	91.5	92.2	92.0	94.0	94.6	95.8	97.0	98.5	99.3	00.0	00.0	89.6	94.65	04.0	03.6	03.7	02.6	01.6	00.3	98.5	97.2	96.8	97.4	99.0	04.1	96.4	00.12	22	
23	20.1	00.5	00.7	00.9	00.6	00.3	00.1	00.3	00.3	00.3	00.3	00.3	00.3	00.3	98.5	98.5	99.2	99.3	99.2	99.0	98.8	98.6	98.5	98.7	98.7	98.7	98.7	98.08	23		
24	97.2	95.5	94.1	93.9	92.5	93.8	94.6	96.2	96.2	97.1	97.9	98.5	98.5	99.2	95.62	00.8	00.7	00.6	00.1	99.5	98.6	97.8	97.0	96.8	96.8	97.1	97.0	00.8	00.8	24	
25	98.4	98.3	98.4	97.8	97.8	97.0	96.1	94.7	95.4	95.6	95.6	95.6	95.0	95.72	96.7	96.5	96.6	96.9	97.0	96.8	96.5	96.7	96.7	96.7	96.7	96.7	96.78	25			
26	94.6	95.7	97.4	96.6	96.9	97.7	00.2	00.8	01.9	05.3	04.6	05.8	06.6	06.6	95.6	00.77	96.7	96.8	97.1	97.9	97.7	97.6	97.6	97.6	97.0	97.0	97.0	97.21	26		
27	07.3	08.1	09.0	09.5	10.2	10.3	10.8	10.9	11.4	12.3	13.6	14.7	14.7	10.68	96.6	96.2	96.0	95.8	94.6	94.6	94.6	94.6	94.6	94.6	94.6	94.6	94.61	27			
28	16.1	17.0	18.3	18.9	19.2	18.9	19.0	18.4	18.4	18.0	18.2	18.4	19.2	19.2	18.23	89.7	89.6	91.5	95.4	95.2	95.7	96.7	97.6	98.2	99.0	99.0	98.6	95.22	28		
29	17.4	16.9	16.7	16.7	16.7	15.9	15.1	14.3	13.1	12.4	11.9	12.0	11.8	11.8	14.52	97.6	95.5	95.0	95.0	95.3	95.4	95.3	95.3	95.3	95.3	95.3	95.3	95.28	29		
30	11.7	11.3	11.1	10.8	09.9	08.6	07.4	06.2	04.9	05.0	05.6	06.5	11.8	11.8	04.8	08.25	99.2	99.6	99.6	99.6	99.1	00.7	01.1	00.5	00.5	00.6	01.8	08.8	00.62	30	
31	06.7	06.7	06.8	06.7	05.9	05.0	04.5	04.1	03.7	03.6	05.8	04.1	07.0	03.4	05.13																
M	05.21	05.21	05.35	05.35	05.18	02.72	02.31	02.07	02.00	02.28	02.90	03.29	06.57	99.32	02.82	97.18	97.06	97.18	97.36	97.41	97.33	97.11	96.91	97.01	97.32	97.33	99.51	94.71	97.18	M	

Juli VII

August VIII

1	01.8	02.0	02.4	03.1	03.1	03.1	03.1	03.3	03.2	03.3	03.5	03.5	03.7	01.8	02.95	10.1	10.5	11.0	11.6	11.6	11.4	10.9	10.2	09.8	10.1	10.8	11.1	11.6	09.0	10.76	1
2	05.8	04.0	05.5	05.8	06.0	06.4	06.5	06.2	06.3	06.8	07.2	07.2	05.9	05.75	11.2	11.1	11.6	11.8	12.1	11.4	11.0	10.4	10.7	11.1	11.7	12.4	12.4	11.38	2		
3	07.4	07.3	07.2	07.3	07.4	06.5	05.8																								

# Registrierungen des Luftdrucks P

1944

**Oslo (Blindern)**  
September IX

$\phi = 60^{\circ} 36' N$

$\lambda = 10^{\circ} 44' E$

$g = 9.819$

$\Delta G = +1^h$

$H_a = 94$

$H_b = 93.6$

$h_t = 2.0$

$h_a = 25.2$

$h_b = 25.6$

$h_r = 1.5$

Oktober X

$\Sigma$	2	4	6.	8	10	12	14	16	18	20	22	24	Max	Min	Dies	2	4	6	8	10	12	14	16	18	20	22	24	Max	Min	Dies	$\Sigma$		
1	78.5	78.5	78.7	79.1	80.1	81.1	82.1	83.7	85.4	87.1	88.9	90.3	90.3	78.3	82.79	92.9	93.7	94.6	95.2	95.8	95.7	95.7	96.5	97.5	98.1	98.7	98.7	92.1	95.84	1			
2	92.6	95.5	95.2	96.1	99.3	99.4	99.4	99.7	98.3	98.2	99.7	99.7	99.7	90.3	97.99	99.3	00.1	01.2	01.6	01.1	01.0	01.3	01.2	01.1	02.1	02.1	02.1	98.7	00.93	2			
3	96.4	95.1	94.1	92.9	91.8	90.6	88.8	88.5	87.5	87.0	87.4	87.9	87.0	90.3	90.39	00.4	00.2	01.2	01.0	00.9	01.6	01.0	00.9	03.0	03.4	04.6	04.6	99.9	01.50	3			
4	88.4	88.9	89.8	90.4	92.3	92.4	92.7	92.7	92.9	93.5	93.5	93.2	93.5	87.4	91.71	05.3	06.0	07.2	08.8	10.1	10.2	10.1	10.3	11.0	11.6	11.4	11.8	04.6	09.47	4			
5	92.5	91.2	90.4	89.6	89.2	89.2	88.6	88.3	88.1	88.2	88.0	87.6	87.6	87.6	89.24	11.0	09.9	09.7	09.5	09.6	09.3	08.7	08.5	09.1	10.4	12.1	13.5	13.5	08.4	10.11	5		
6	87.8	85.7	85.1	85.6	86.2	86.8	87.7	88.7	89.8	91.3	92.4	95.2	95.2	85.1	88.36	13.9	14.2	14.1	14.4	14.1	11.9	09.9	07.6	05.8	04.6	04.5	05.0	14.7	05.0	09.85	6		
7	94.0	94.5	96.2	97.0	97.9	97.9	97.4	96.7	96.5	94.9	92.1	98.0	92.1	92.1	95.91	02.5	02.2	02.1	01.7	01.9	09.3	09.7	09.7	09.7	09.5	03.0	03.0	00.8	01.88	7			
8	87.9	84.9	85.8	82.2	80.3	78.3	76.4	77.1	80.6	84.0	86.5	88.2	82.1	75.7	82.52	99.2	98.7	97.5	97.6	97.7	97.7	98.3	00.0	01.5	03.1	04.0	04.0	97.5	00.88	8			
9	89.9	89.9	90.6	91.5	92.5	92.3	92.4	92.7	93.2	95.5	96.9	98.1	98.1	88.2	92.88	04.9	05.4	06.0	06.7	06.0	05.9	06.2	06.4	07.1	07.2	04.0	04.0	06.22	9				
10	99.8	01.1	02.2	03.7	04.7	05.3	05.6	05.7	06.1	06.9	07.2	07.2	07.2	98.1	04.82	07.1	06.9	07.1	06.7	05.3	05.7	03.7	03.1	02.6	02.1	01.4	04.98	10					
11	07.6	07.9	08.6	09.5	10.7	10.9	11.3	11.8	12.4	13.6	14.8	16.3	16.3	07.2	11.28	00.6	99.8	99.5	99.3	99.1	99.1	98.7	98.8	99.2	99.1	98.6	01.4	98.6	99.26	11			
12	17.5	18.9	19.7	20.6	21.5	21.5	21.3	21.1	21.2	21.4	21.4	21.5	21.5	16.3	20.48	98.1	97.9	98.1	98.7	98.9	99.1	00.5	00.5	00.7	00.7	00.5	00.5	00.8	97.7	99.18	12		
13	21.4	21.3	21.3	21.6	21.7	21.3	20.4	19.7	19.4	19.6	19.6	21.0	21.0	19.4	20.58	00.1	98.9	98.3	97.7	96.9	96.0	94.9	94.0	93.0	92.5	92.5	00.6	92.5	95.66	13			
14	19.4	19.2	19.2	19.5	19.5	18.9	18.4	17.7	17.2	17.5	17.7	19.6	17.2	18.49	95.5	95.3	95.3	95.6	94.0	95.7	92.3	91.2	90.5	89.6	88.9	87.8	91.81	14					
15	17.5	17.2	17.1	17.6	16.5	16.3	15.4	15.1	14.5	14.2	13.9	17.7	13.9	15.82	88.4	88.6	90.9	91.7	92.6	95.4	95.9	94.5	94.6	94.3	94.6	94.6	92.22	15					
16	13.7	13.0	12.7	12.6	12.5	11.9	11.5	10.1	9.8	08.6	08.7	08.9	13.9	08.6	11.12	94.1	94.0	94.5	94.8	94.3	95.2	92.4	91.8	90.9	89.8	88.7	87.9	94.8	87.7	92.64	16		
17	08.2	09.0	09.1	09.3	09.2	09.5	09.7	09.8	10.1	11.3	11.4	12.3	12.3	08.8	09.97	88.2	88.9	89.2	89.6	89.2	77.6	78.1	78.6	78.7	78.1	76.7	76.7	74.5	74.5	79.35	17		
18	12.8	15.2	15.9	15.5	16.2	16.1	15.8	16.0	16.4	16.9	17.4	17.5	17.5	12.3	15.84	65.5	65.2	66.1	67.4	67.6	67.9	69.4	70.9	72.4	73.5	73.5	74.3	74.3	65.1	68.35	18		
19	18.0	17.8	17.9	18.2	18.8	18.5	18.0	17.1	16.4	16.9	17.5	17.2	19.0	16.4	17.59	75.4	76.1	77.4	78.5	80.2	80.0	84.6	84.6	86.4	87.6	89.1	90.4	74.3	82.56	19			
20	16.7	15.3	14.4	13.8	13.0	12.5	11.9	11.4	11.6	12.2	12.8	13.5	17.2	11.4	13.26	91.5	95.1	95.3	95.5	96.4	96.6	97.9	98.7	99.3	99.3	90.4	95.66	20					
21	13.8	14.0	14.5	15.8	16.1	16.3	16.6	16.4	16.0	16.4	16.4	16.1	16.7	13.5	15.72	00.5	01.6	02.9	03.2	04.6	05.0	06.4	07.4	08.5	09.5	11.0	11.8	12.9	13.6	99.3	07.62	21	
22	15.7	14.7	14.4	14.8	14.4	13.5	12.0	11.2	10.7	10.3	09.3	08.2	16.1	08.2	12.43	14.0	14.6	14.9	15.7	15.9	15.6	15.4	15.2	14.9	14.1	13.3	13.9	14.8	14.8	14.8	14.85	22	
23	06.9	05.6	05.0	04.5	05.6	05.8	01.5	00.7	09.3	08.5	08.7	09.1	09.1	01.5	01.59	01.59	01.0	01.1	01.1	01.0	01.0	01.0	01.0	01.0	01.0	01.0	01.0	01.0	01.0	01.0	07.63	23	
24	92.9	92.2	92.3	92.6	92.2	92.5	92.9	92.7	92.5	92.5	92.5	92.5	92.5	92.2	92.57	07.4	08.4	09.9	10.1	11.1	12.2	13.1	13.5	13.9	14.4	14.4	14.5	14.5	14.6	14.6	14.6	12.25	24
25	92.7	93.0	93.3	93.5	93.5	93.2	90.9	88.9	86.4	85.2	85.2	82.7	80.0	80.9	83.3	73.4	13.5	13.6	13.6	13.6	13.6	13.7	14.1	14.4	14.4	14.5	14.5	14.6	14.6	14.6	13.89	25	
26	78.0	75.9	75.2	74.9	74.7	74.8	76.5	76.8	77.6	78.7	78.6	77.6	77.6	74.4	76.61	14.8	14.6	14.6	14.8	14.7	14.0	13.3	12.5	12.0	11.0	10.6	10.1	10.1	10.1	13.08	26		
27	77.2	76.6	76.9	77.9	78.7	78.8	79.4	79.8	80.8	82.2	82.9	83.6	83.6	76.6	79.57	08.9	07.5	06.8	06.9	06.7	05.9	05.2	04.1	04.0	03.2	02.4	02.2	01.0	01.0	05.32	27		
28	85.0	86.7	88.4	89.6	90.6	90.5	94.6	95.5	97.0	98.1	99.1	99.1	99.1	80.2	00.02	00.2	03.6	02.3	02.3	03.6	03.6	03.4	03.8	04.7	05.5	07.0	07.7	07.7	07.7	04.02	28		
29	01.1	01.2	01.2	01.1	00.0	00.0	96.5	95.7	94.5	92.9	90.8	99.0	99.0	01.5	01.0	00.96	06.8	08.6	09.8	10.7	11.2	11.4	11.7	12.2	12.5	12.8	13.5	13.5	13.7	10.92	29		
30	87.3	86.0	85.2	84.8	84.7	84.6	85.2	86.8	86.8	88.5	90.2	91.2	92.1	84.6	87.22	13.4	13.6	14.2	15.2	15.7	15.3	14.8	14.7	14.1	12.7	12.7	12.7	12.7	14.52	30			
	00.37	00.13	00.21	00.63	00.84	00.63	00.36	00.28	00.34	00.81	00.97	00.90	00.90	04.21	96.62	00.54	01.39	01.17	01.14	01.52	01.81	01.68	01.27	01.05	01.27	01.45	01.61	01.56	04.90	97.81	31		

November XI

Dezember XII

1	95.1	94.5	94.0	94.2	94.5	94.6	94.3	94.7	95.5	95.9	96.2	96.6	96.6	94.0	95.01	05.7	04.1	04.6	05.3	04.5	02.7	01.4	00.3	98.6	
---	------	------	------	------	------	------	------	------	------	------	------	------	------	------	-------	------	------	------	------	------	------	------	------	------	--

Registrierungen der Lufttemperatur T

1944

**Oslo (Blindern)**

Januar I

$\varphi = 60^{\circ} 56' N$

$\lambda = 10^{\circ} 44' E$

$g = 9.819$

$\Delta G = +1^{\circ}$

$H_a = 94$

$H_b = 95.6$

$h_c = 2.0$

$h_d = 25.2$

$h_e = 25.6$

$h_f = 1.5$

Februar II

Ø	2	4	6	8	10	12	14	16	18	20	22	24	Max	Min	Dies	2	4	6	8	10	12	14	16	18	20	22	24	Max	Min	Dies	Ø									
1	-4.1	-3.5	-1.9	-2.2	-4.6	-4.5	0.8	2.2	1.0	-2.4	-1.8	-1.9	2.9	-5.5	-1.91	-1.5	-2.2	-3.3	-2.4	-0.7	0.7	3.0	2.9	3.2	3.3	3.2	3.0	3.4	-3.3	0.77	1									
2	-3.2	-4.1	-3.9	-5.0	-5.1	-3.4	-2.0	-2.0	-2.2	-3.1	-5.1	-0.6	-5.7	-3.42	-2.7	-2.2	-1.5	-2.1	-4.9	6.2	7.2	4.9	1.5	0.7	-0.4	-0.4	7.2	-0.4	2.76	2										
3	-5.2	-4.8	-5.4	-4.5	-0.2	-2.1	-0.6	-1.2	-2.1	-4.3	-4.9	0.3	-5.4	-3.16	-0.3	0.0	-1.4	-0.5	-0.6	-0.3	0.4	0.8	0.0	0.0	-0.2	-0.2	0.8	-1.4	-0.19	3										
4	-5.1	-5.0	-6.9	-7.4	-8.7	-7.0	-4.9	-5.0	-1.4	-2.4	-1.9	-0.5	-0.5	-8.7	-4.75	-0.2	-0.2	-0.3	-0.6	-0.4	1.8	2.2	2.4	-1.9	-2.5	-0.7	-1.5	2.5	-0.6	0.94	4									
5	-0.5	-1.8	-3.9	-5.8	-6.1	-6.5	-4.7	-4.2	-2.0	0.9	2.5	4.1	4.1	-6.7	-2.33	1.5	1.5	2.3	1.6	0.6	1.3	1.4	0.5	-1.0	-1.5	-2.4	-4.5	2.3	-4.5	0.11	5									
6	4.3	4.3	4.3	4.6	7.0	5.9	5.6	4.4	3.7	3.4	3.3	3.2	7.0	2.4	4.90	-4.9	-6.3	-7.2	-8.0	-7.2	-4.4	-3.0	-2.4	-3.3	-4.4	-4.0	-2.3	-8.1	-4.0	-4.89	6									
7	2.9	2.1	1.7	1.2	1.2	2.0	2.0	0.5	-2.3	-3.2	-5.2	-6.1	3.2	-6.1	-0.27	-2.5	1.1	2.3	2.8	4.0	4.4	5.1	3.6	3.0	5.3	-4.0	2.69	7												
8	-5.8	-6.3	-6.0	-5.7	-5.6	-4.2	-3.1	-2.8	-2.6	-2.5	-3.2	-4.0	-2.5	-6.5	-4.32	2.8	2.0	0.0	1.4	4.0	5.0	3.7	2.7	0.9	-0.6	-3.4	-4.8	5.6	-4.8	1.14	8									
9	-5.8	-7.2	-8.2	-8.8	-8.7	-8.4	-7.2	-8.2	-10.5	-10.9	-11.3	-9.8	-4.0	-11.3	-8.75	-5.4	-4.6	-5.3	-4.6	-3.0	-0.1	2.0	2.0	-1.0	-1.9	-2.7	-2.9	2.5	-5.6	-2.29	9									
10	-11.1	-10.7	-12.8	-13.1	-14.8*	-13.0*	-11.0	-13.5*	-14.5*	-15.5*	-15.8*	-15.5	-9.8	-15.8	-13.44	3.0	-3.2	-3.0	-2.0	0.2	2.2	2.7	2.6	0.9	0.8	-0.1	3.0	-3.2	-0.41	10										
11	-16.0*	-16.0*	-16.0*	-15.0*	-11.0*	-4.5*	-0.6*	-4.2*	-5.2	-5.3	-7.2	-9.5	-0.6	-16.0	-9.21	0.6	0.8	-0.2	1.8	2.5	3.1	3.0	2.7	1.3	1.6	1.6	0.5	3.5	-0.3	1.61	11									
12	-6.2	-8.6	-9.7	-9.7	-10.7	-8.7	-8.2	-10.3*	-10.8*	-11.0	-11.3*	-9.3	-8.2	-11.3	-9.72	-1.6	-3.5	-5.1	-6.2	-3.5	-0.2	-0.6	-1.1	-4.0	-5.6	-6.3	-7.9	0.5	-7.9	-3.80	12									
13	-8.5*	-8.0*	-7.5*	-7.4	-6.2	-5.1	-4.3	-3.0	-1.6	-0.6	-0.7	-1.1	-0.6	-9.3	-4.90	-8.6	-8.9	-8.9	-6.8	-3.5	-2.2	-2.0	-3.2	-3.4	-3.7	-3.9	-1.8	-5.32	13											
14	-0.6	-0.5	-0.5	-1.1	-2.5	-1.8	-0.9	-3.1	-4.3	-2.4	-2.5	-2.1	-0.2	-4.5	-1.86	-3.9	-3.9	-3.6	-2.8	-2.0	-0.5	-0.5	-4.0	-4.7	-6.7	-7.9	-0.5	-7.9	-3.88	14										
15	-2.1	-3.3	-3.5	-3.3	-2.2	-1.5	-0.5	-0.6	-1.8	-2.4	-2.3	-2.2	0.2	-3.9	-2.14	-8.2	-9.0	-9.9	-10.9	-8.9	-5.7	-4.8	-4.8	-4.6	-4.0	-3.7	-3.2	-10.9	-6.48	15										
16	-3.1	-2.5	-2.9	-1.6	-3.0	-0.8	0.0	-0.2	-0.9	-3.1	-3.7	-2.4	0.9	-3.7	-2.02	-2.8	-2.4	-1.9	-1.8	-1.2	-0.9	-0.4	-0.6	-0.9	-1.1	-1.1	-0.4	-3.2	-1.35	16										
17	-3.1	-3.9	-5.5	-4.6	-3.5	-4.4	-2.1	0.2	0.9	-1.0	-1.2	-1.0	1.0	-5.5	-2.43	-1.2	-1.2	-1.3	-1.5	-0.8	-0.4	-0.2	-0.8	-1.0	-1.0	-1.2	-0.2	-1.5	-1.01	17										
18	-1.0	-1.0	-1.5	-1.7	-1.4	-1.4	-1.4	-1.2	-1.3	-1.4	-2.0	-2.4	-1.0	-2.4	-1.48	-1.8	-2.0	-2.4	-2.7	-2.6	-2.2	-2.8	-3.9	-4.4	-4.7	-5.0	-1.2	-5.0	-3.10	18										
19	-2.2	-0.1	1.0	1.8	1.8	2.3	2.4	2.3	1.6	0.8	0.3	-0.4	2.4	-2.5	0.97	-5.5	-5.6	-6.2	-5.8	-5.7	-5.7	-5.6	-5.7	-5.7	-5.7	-5.7	-5.0	-6.3	-5.72	19										
20	-1.3	-2.2	-3.1	-5.0	-6.3	-6.1	-5.1	-6.5	-7.0	-7.0	-6.5	-5.5	-0.4	-7.0	-5.13	-5.7	-5.9	-9.2	-10.2	-6.7	-4.4	-1.9	-0.9	-3.8	-5.1	-6.0	-6.5	-0.9	-10.2	-5.52	20									
21	-6.0*	-4.5*	-4.5*	-2.2	-0.7	0.0	0.6	0.0*	-2.0*	-3.0*	-4.0*	-4.0*	-3.0	-6.0	-2.44	-4.3	-5.8	-5.9	-0.9	1.7	2.8	3.3	3.3	1.1	-0.8	-1.1	-1.0	3.5	-6.7	-0.69	21									
22	-2.0*	-1.5*	-1.5*	-0.4	-2.0*	2.5*	3.8	4.0	4.0	2.5*	2.5*	2.0	4.0	-3.0	1.49	-1.0	-0.2	-3.5	1.5	1.8	4.9	7.5	7.5	4.2	1.5	0.1	-0.8	7.5	-1.1	-2.32	22									
23	2.0*	1.5*	1.5	2.3	2.6	2.5	2.8	1.8	1.0	0.5	1.1	2.8	-0.2	1.78	-0.9	-1.8	-2.1	-2.6	-0.6	3.3	5.8	7.8	1.7	2.4	-1.5	-2.1	7.9	-2.7	-0.78	23										
24	0.8	1.6	2.6	1.9	1.8*	2.0*	2.2	0.8	-2.8	-5.0*	-7.0*	-7.0*	-2.6	-7.0*	-0.68	-2.1	-2.8	-4.1	-5.1	-2.4	1.2	4.4	6.6	0.0	-2.7	-4.5	-3.9	6.7	-5.1	-1.28	24									
25	-7.0*	-5.5*	-4.5*	-2.8	-2.7	-3.0*	-3.6	-3.2	-3.2	-3.0	-2.3	-2.3	-2.3	-7.0*	-3.59	-4.0	-4.3	-2.6	3.5	5.3	5.1	2.9	0.5	0.5	-0.7	0.0	5.4	-4.4	0.57	25										
26	-2.2	-2.2	-2.3	-1.4	-1.6	0.6	-0.4	-0.9	-1.0	-3.3	-5.3	-6.0	0.6	-6.0	-2.17	-1.5	-2.2	-3.4	-4.0	-2.1	-0.2	-0.2	-2.6	-3.8	-3.6	0.0	-4.2	-2.28	26											
27	-5.7	-5.1	-3.8	-1.7	-0.2	2.8	3.0	1.9	1.4	0.6	4.4	3.6	4.5	-6.0	-0.10	-3.9	-4.3	-4.7	-5.0	-4.8	-3.5	-3.4	-5.6	-7.2	-7.6	-7.7	-3.3	-7.7	-5.09	27										
28	-0.7	0.8	1.7	0.4	0.7	4.6	6.7	5.4	2.7	2.4	1.6	0.5	6.8	-0.2	2.35	-10.0	-11.3	-15.4	-14.0	-9.5	-6.0	-4.4	-4.0	-8.0	-11.0	-12.0	-12.9	-4.0	-14.0	-9.71	28									
29	-2.4	-4.0	-3.6	-3.0	-2.1	-0.4	1.4	0.8	-0.7	0.1	0.6	-0.9	1.6	-4.2	-1.18	-9.8	-9.5	-8.8	-7.0	-2.7	-0.4	-0.4	0.6	0.8	0.8	0.6	0.8	-13.6	-4.18	29										
30	1.1	4.3	6.5	6.1	7.1	7.5	9.6	7.9	5.7	2.1	1.9	1.9	9.6	-0.9	5.12	-1.1	0.55	-0.7	2.2	3.0	3.3	5.8	6.0	5.2	5.7	5.4	4.8	6.1	2.9	-4.18	30									
31	2.3	0.8	0.3	-1.0	-1.0	0.5	1.5	1.5	1.3	0.7	0.3	-0.6	3.0	-1.1	0.55	-3.14	-3.13	-2.74	-1.73	-0.60	-1.14	-1.80	-2.44	-2.73	-2.01	0.89	-4.98	-2.39	-3.10	-3.23	-3.08	-3.55	-2.02	-1.77	-2.53	-2.85	1.57	-5.45	-1.83	M

März III

April IV

1	0.8	0.9	1.4	1.7	1.9	2.5	-0.9	-1.5	-4.5	-6.7	-7.6	-2.6	-6.7	-0.77	-4.9	-6.2	-6.8	-4.4	-2.4	0.0	1.6	2.3	2.4	-2.8	-4.3	-6.0	2.5	-7.3	-2.62	1
2	-6.8	-6.9	-7.5	-7.2	-4.1	-0.6	0.0	-2.1	-1.1	-1.1	-2.6	-7.6	-2.6	-6.8	-7.0	-4.8	-1.1	-1.9	1.9	4.5	5.5	4.8	2.0	-0.6	-2.8	5.7	-7.6	-1.02	2	
3	-1.5	-1.5	-1.6	-3.5	-2.8	-1.7	-0.4	1.6	-1.8	-0.2	-0.7	-2.9	-1.7	-3.5	-1.38	-3.5	-2.0	-1.8	-1.9	0.7	2.0	4.1	4.9	1.9	1.0	-1.8	5.1	-3.5	0.92	3
4	-1.4	-2.3	-3.2	-3.4	-1.6	-1.6	2.0	1.8	0.2	-2.1	-4.1	-6.1	2.2	-6.1	-1.55	-1.9	-2.6	-2.9	-0.8	1.2	2.3	2.4	3.1	2.8	1.3	0.7	3.3	-2.9	0.50	4
5	-7.8	-7.3	-7.3	-7.7	-7.7	-5.4	0.1	2.8	2.9	0.5	-2.8	-4.7	-6.3	3.2	-8.1	-3.42	0.3	0.1	0.3	0.0	1.3	2.5	3.3	3.0	-0.2	4.2	-0.7	1.22	5	
6	-7.4	-7.5	-7.5	-6.4	-3.5	-1.2	4.0	4.0	1.0	-1.8	-2.																			

## Registrierungen der Lufttemperatur T

194

Oslo (Bildern)

Mat V

$$\theta = 20^\circ \text{ N}$$

101 ME

R = 9.819

ACM SIGART

M-28

100

1-3

13

b4 = 35

九三

Juni V

X	2	4	6	8	10	12	14	16	18	20	22	24	Max	Min	Dies	2	4	6	8	10	12	14	16	18	20	22	24	Max	Min	Dies	X	
1	4.6	4.6	4.5	5.0	6.0	9.5	14.6	15.1	12.4	9.2	6.3	5.5	16.1	4.4	8.11	8.8	8.0	7.4	6.8	8.0	10.2	12.0	13.2	14.3	12.0	8.2	6.9	14.5	6.7	9.05	1	
2	4.8	3.7	3.6	2.6	1.2	2.5	3.2	4.1	4.7	4.0	3.5	3.0	5.5	1.2	3.38	7.1	7.4	10.3	11.6	13.5	12.3	10.9	9.8	10.8	9.7	8.9	8.2	14.8	6.9	10.04	2	
3	2.9	2.9	3.0	5.6	5.4	5.0	2.9	3.3	3.1	3.1	1.9	2.1	3.6	1.7	2.95	7.9	7.4	7.4	8.3	9.3	9.7	9.5	10.3	11.2	10.0	9.4	8.6	11.3	7.3	9.08	3	
4	1.7	1.1	1.8	5.3	5.2	5.3	6.1	6.2	6.2	4.0	0.8	0.2	6.3	0.2	3.49	8.0	7.6	7.9	9.8	11.1	12.5	10.4	9.9	8.3	8.1	8.6	12.7	7.5	9.19	4		
5	-0.6	-0.9	0.2	2.4	5.1	4.7	4.8	5.0	4.2	3.2	1.8	1.5	5.0	-1.0	2.45	8.8	9.3	9.4	10.0	10.2	11.0	14.3	14.2	13.5	11.8	10.2	9.3	14.3	8.6	11.00	5	
6	0.4	-0.6	0.4	3.9	5.2	6.5	7.8	8.5	8.4	6.1	2.8	-0.5	8.9	-0.6	4.08	9.2	9.2	9.9	10.5	12.1	12.8	14.1	13.0	12.6	12.0	10.4	10.1	14.4	9.2	11.32	6	
7	-1.0	-1.4	0.2	5.8	8.6	9.6	11.7	13.0	12.7	9.3	3.2	0.8	13.1	-1.4	6.04	9.8	9.4	9.5	10.4	11.0	11.2	12.4	12.7	12.9	12.0	11.8	13.5	9.4	11.26	7		
8	0.2	-0.9	0.6	7.0	10.5	14.1	15.4	16.3	16.2	12.5	5.7	2.9	16.4	-1.7	8.36	11.7	11.8	11.5	11.3	11.8	11.8	12.8	13.4	13.5	12.1	8.7	5.9	13.5	5.9	11.36	8	
9	1.9	0.7	3.5	8.5	12.6	15.0	16.1	17.6	14.5	12.4	8.3	5.9	17.7	0.2	9.75	4.9	5.9	6.9	11.3	13.6	16.0	17.8	18.9	17.9	14.9	12.1	10.5	18.9	4.7	12.56	9	
10	4.4	5.3	4.9	7.0	8.4	13.5	14.8	15.4	14.6	13.3	7.4	4.9	15.6	4.4	9.49	10.1	9.8	9.6	10.0	11.3	11.4	10.8	9.9	9.3	8.1	7.5	6.8	11.6	6.8	9.95	10	
11	3.5	2.0	4.7	10.0	13.2	16.3	17.8	18.4	16.6	13.5	10.6	6.4	18.5	1.6	11.06	6.6	6.2	6.4	7.4	9.8	12.3	14.3	14.6	13.5	11.6	10.8	10.8	15.4	6.1	10.36	11	
12	4.4	2.4	6.7	11.8	15.2	17.7	17.8	16.5	14.0	10.5	8.3	8.0	18.7	2.3	11.18	10.7	10.5	10.2	10.1	9.3	9.4	9.8	9.8	9.9	9.6	6.4	10.8	6.4	9.63	12		
13	7.7	7.3	7.3	8.7	10.9	14.2	16.2	17.1	15.9	14.9	13.2	8.0	17.6	7.2	11.78	4.3	4.1	7.8	13.0	15.4	16.4	17.0	15.4	13.7	13.0	11.4	9.8	17.4	3.9	11.78	13	
14	6.0	5.5	7.3	12.4	14.6	15.9	15.1	10.0	6.6	5.7	4.6	4.4	16.8	4.4	9.01	9.0	9.0	9.0	9.5	10.1	7.2	9.2	9.3	12.9	12.6	10.3	9.3	10.11	14			
15	4.4	4.2	4.8	5.8	6.5	7.0	7.7	8.5	6.9	6.5	6.9	6.9	8.6	4.2	6.34	9.0	8.9	9.4	12.2	14.0	13.4	16.4	13.8	12.6	12.2	10.0	8.1	16.4	8.1	11.67	15	
16	6.9	5.7	5.4	5.9	7.0	7.7	8.2	8.5	8.2	7.8	7.5	7.0	8.6	5.4	7.15	7.0	6.1	9.2	14.0	15.6	16.7	17.0	15.5	14.1	11.8	10.4	8.4	17.0	6.0	12.15	16	
17	6.5	6.1	5.1	7.2	8.4	9.7	10.8	11.9	13.0	12.4	11.5	10.8	13.2	6.1	9.53	9.0	9.1	11.5	12.7	14.1	15.8	17.8	19.3	16.2	16.3	11.3	11.6	19.3	7.1	13.72	17	
18	11.0	9.8	11.0	12.6	15.2	17.4	18.5	16.6	18.3	16.5	10.9	10.6	18.6	9.8	14.20	8.2	6.6	11.3	16.1	18.4	20.3	21.6	21.8	17.4	14.3	7.5	22.5	6.6	15.38	18		
19	9.9	8.1	10.9	14.6	15.8	17.4	18.3	19.2	19.0	16.2	10.8	6.5	19.3	6.5	13.86	5.9	5.3	11.8	17.6	20.4	22.7	25.8	25.8	22.9	20.1	15.4	9.9	24.3	5.2	16.63	19	
20	4.2	4.0	5.6	8.0	9.0	10.1	10.8	10.6	9.6	8.4	4.7	3.0	11.4	3.0	7.33	8.3	9.0	11.1	16.7	20.2	21.5	22.0	21.7	19.5	16.1	12.6	12.6	22.0	8.1	15.96	20	
21	2.7	3.0	4.1	4.8	5.2	5.2	8.2	9.0	4.8	6.0	3.7	3.6	9.6	2.2	4.81	10.7	14.3	14.1	14.0	15.8	17.8	18.2	19.0	20.3	17.6	12.6	9.0	20.7	9.0	15.28	21	
22	3.6	5.4	4.9	6.3	7.8	8.7	9.3	9.5	9.2	8.9	3.9	4.2	10.2	3.2	6.64	7.8	7.2	10.6	13.5	15.4	16.1	17.3	16.3	14.9	11.3	9.7	7.8	17.3	7.2	12.32	22	
23	3.9	5.7	5.3	7.6	9.5	10.1	10.9	10.2	9.6	7.9	5.5	3.2	11.9	3.2	7.26	6.2	6.2	8.4	10.6	12.1	13.9	14.8	15.4	14.1	12.5	9.3	7.8	16.2	6.2	10.94	23	
24	1.7	1.0	3.3	5.8	8.1	6.9	9.4	11.0	11.3	8.3	6.4	3.4	11.8	1.0	6.38	4.8	5.4	8.6	12.4	14.3	15.0	17.5	17.7	16.2	13.9	12.5	11.7	18.4	4.4	12.50	24	
25	2.2	1.9	4.5	7.6	10.2	11.2	11.5	10.5	8.6	7.7	7.0	5.6	11.6	1.7	7.38	11.6	11.8	12.4	13.7	14.5	15.1	15.1	14.2	12.7	12.6	12.0	16.3	11.6	13.11	25		
26	5.1	5.1	5.2	6.3	10.5	13.6	15.7	16.0	15.0	13.4	8.6	6.2	16.1	5.1	10.22	12.4	12.1	12.2	13.6	16.7	17.3	16.9	17.5	16.2	14.7	13.7	15.6	17.6	12.0	14.74	26	
27	5.7	5.1	7.6	10.0	10.2	11.1	11.6	12.2	13.1	10.6	10.4	13.1	4.7	9.74	13.5	13.2	14.6	16.1	17.4	21.5	23.2	18.5	17.8	19.1	16.0	23.2	13.2	17.19	27			
28	8.4	8.3	10.4	14.3	16.5	18.3	18.5	18.6	17.2	15.6	14.2	11.6	18.1	7.1	14.31	14.4	14.1	12.6	14.8	15.4	15.9	16.9	17.1	16.5	14.6	12.9	11.6	17.2	11.6	14.73	28	
29	10.6	9.5	10.1	11.0	11.5	13.8	15.6	17.5	16.6	15.3	15.3	10.5	17.5	9.3	12.94	12.3	13.5	12.9	12.9	13.7	15.8	16.6	16.3	17.5	15.6	14.1	11.0	17.7	11.0	14.35	29	
30	10.1	10.1	12.4	14.5	16.4	17.4	17.6	17.6	16.9	11.5	9.9	8.0	17.9	8.0	13.53	9.9	9.6	9.9	13.8	15.5	18.3	20.1	21.4	21.3	18.5	14.1	12.4	21.5	9.6	15.40	30	
31	8.0	7.1	8.4	11.7	13.5	14.6	15.3	13.5	13.1	12.0	10.4	9.7	15.3	7.0	11.44																	
32	4.70	4.12	5.43	8.00	9.54	11.19	12.34	12.54	11.60	9.97	7.23	5.62	13.34	3.56	8.52	8.93	8.93	10.11	12.09	13.60	14.56	15.63	15.80	14.98	13.56	11.41	9.80	16.82	7.76	12.43	33	

Juli VI

August VIII

1	12.8	13.6	14.7	16.0	16.6	17.8	18.0	17.6	16.0	15.8	15.6	15.0	18.5	12.2	15.79	15.0	14.2	14.8	19.8	23.7	24.9	21.3	26.6	26.8	24.5	19.4	17.5	26.8	14.0	20.71
2	14.9	14.7	14.8	15.0	15.3	16.5	17.5	20.1	18.6	16.7	15.3	12.7	20.1	12.7	16.01	16.1	16.2	17.4	21.4	24.4	25.6	26.6	25.4	20.5	19.2	16.0	27.1	16.0	21.45	
3	13.0	13.1	14.0	15.0	16.5	19.7	21.8	22.3	22.1	20.2	17.1	15.6	22.4	12.7	17.53	18.5	16.7	17.5	20.3	22.2	25.6	24.9	25.5	22.5	17.5	16.0	25.5	15.9	20.84	
4	13.7	13.4	16.6	20.0	22.6	25.2	25.4	26.1	25.8	25.8	19.0	15.8	26.4	13.5	20.41	15.1	13.9	15.7	19.8	22.1	24.3	25.3	24.8	23.8	21.3	17.0	14.8	25.4	13.8	20.82
5	14.4	13.3	16.4	20.8	24.0	25.8	27.2	27.3	26.0	25.5	19.8	16.1	27.4	13.5	21.22	13.4	15.0	14.1	17.9	21.6	24.0	25.9	25.8	24.6	21.6	19.3	16.4	26.0	12.9	19.82
6	14.6	13.8	16.9	20.6	24.1	26.6	27.3	26.5	23.7	22.6	19.9	17.3	27.3	13.8	21.16	16.8	15.8	15.7	19.3	21.8	23.3	24.6	25.6	25.2	20.4	18.0	17.4	26.0	14.8	20.32
7	15.4	15.8	16.4	17.8	20.6	23.7	25.8	26.9	25.0	23.0	20.2	15.7	26.9	15.4	20.52	17.3	17.1	16.9	21.7	21.3	22.8	25.6	21.8	18.6	18.2	16.9	23.6	16.7	19.05	
8	14.0	13.5	16.4	19.9	23.5	26.5	28.0	27.1	26.2	24.2	20.2	17.3	20.0	13.1	21.37	16.1	16.5	16.2	16.4	18.3	21.6	25.0	22.8	21.5	19.4	17.2	16.4	23.1	15.7	18.77
9	16.9	16.8	19.1	22.4	23.8	26.8	29.3	30.4	28.4	26.5	19.7	19.9	30.4	16.6	23.38	16.1	15.3	15.3	16.2	16.7	18.2	19.6	21.2	20.5	17.8	15.0	13.1	21.6	13.1	17.08
10	20.4	18.5	19.0	19.3	20.1	20.4	21.0	20.2	18.4	16.7	15.0	19.12	12.3	11.9	13.7	19.4	17.2	19.8	20.5	19.9	19.2	18.1	14.9	12.8	20.5	11.8	16.31			
11	15.2	15.1	15.2	17.4	18.8	19.5	19.8	20.1	19.2	16.8	15.7	14.4	20.4	14.4	17.27	12.3	11.9	12.8	17.1	18.5	18.3	19.8	21.1	20.7	18.2	16.2	16.0	21.1	11.9	16.91
12	15.3	15.1	14.0	16.0	18.8	17.2	13.8	15.5	15.1	15.6	13.3	13.1	18.8	12.9	14.90	15.0	13.3	13.3	17.1	18.2	19.8	20.0	20.7	18.5	14.6	12.5	10.5	20.7	10.5	16.12
13	15.0	11.9	11.8	14.0	15.3	14.8	15.8	17.4	17.9	14.8	15.0	12.3	19.3	11.7	14.35	10.4	8.7	10.0	15.0	17.4	18.5	18.9	18.7	14.9	11.4	10.7	19.8	7.7	14.32	
14	12.2	12.1	12.0	13.6	17.0	16.7	18.5	19.2	17.4	15.9	14.4	14.0	19.2	12.0	15.25	10.1	8.8	9.5	13.5	17.0	18.5	19.6	19.9	19.1	14.8	13.1	11.0	20.1	8.2	14.56
15	13.9	14.0	14.2	15.8	17.3	18.3	17.4	16.1	15.3	16.0	15.0	14.1	19.1	13.9	15.62	7.9	7.3	7.8	14.7	16.7	17.6	19.1	17.9	16.0	14.3	14.2	19.1	7.0	14.04	
16	12.8	12.7	14.0	15.2	15.9	18.6	20.4	20.2	20.1	19.1	15.9	15.1	21.9	12.3	16.67	13.8	13.3	12.8	14.0	16.5	18.6	18.4	17.8	17.1	15.9	15.5	15.4	18.9	12.8	15.76
17	14.4	13.7	15.6	20.8	23.4	24.8	22.6	25.7	23.8	22.8	19.9	19.3	26.1	13.7	20.72	15.0	13.4	14.4	15.4	17.4	20.1	20.4	19.6	19.0	17.8	16.8	16.7	20.7	13.1	17.17
18	18.1	16.9	18.4	20.7	23.1	25.1	26.0	26.8	27.0	24.7	18.7	16.4	27.0	16.4	21.82	16.6	15.9	14.4	15.7	18.4	19.9	18.2	18.0	18.4	17.8	17.2	17.3	20.0	14.1	17.32
19	15.2	15.2	16.5	20.9	24.6	25.9	27.4	26.6	25.5	22.2	20.1	17.1	27.7	14.8	21.43	16.9	17.0	17.3	18.0	17.9	21.6	21.8	21.6	20.3	18.7	18.1	17.8	22.1	16.8	18.92
20	17.4	16.5	17.4	17.8	19.6	20.3	21.5	22.0	22.3	20.4	16.8	17.0	22.4	16.4	19.08	17.4	16.9	16.5	17.0	17.7	18.0	19.0	19.2	18.2	17.9	18.8	18.2	19.2	16.5	17.97
21	15.6	13.9	13.9	15.6	17.6	19.6	19.8	20.1	19.7	19.4	16.5	14.7	20.9	13.7	17.20	18.7	18.4	18.1	18.3	17.4	20.9	21.9	18.6	16.6	15.3	13.3	11.6	22.0	11.6	17.42
22	14.8	13.9	16.2	17.4	18.8	19.0	20.1	21.0	22.4	20.7	16.6	16.3	22.4	13.9	18.10	11.2	9.5	10.6	12.3	15.0	17.6	18.7	20.0	19.4	15.3	13.1	11.6	20.1	9.4	14.52
23	15.3	14.0	15.5	18.8	20.8	21.7	22.1	22.9	21.5	19.6	16.1	14.6	23.4	13.8	18.59	9.8	8.6	8.6	14.0	17.7	20.5	22.7	21.0	17.8	13.5	12.9	23.0	8.6	15.83	
24	13.6	13.0	12.5	11.4	10.5	11.4	14.2	15.6	16.3	15.5	13.9	13.1	16.4	10.4	15.42	12.1	11.8	12.0	15.6	19.0	21.8	23.3	23.4	22.2	18.1	16.8	16.3	23.8	11.8	17.70
25	12.3	11.8	11.5	12.9	14.9	17.6	18.9	20.3	19.7	17.3	11.4	10.2	20.3	10.2	14.88	15.5	15.0	14.4	18.8	20.6	22.1	22.1	21.7	21.3	19.9	19.2	18.3	22.7	14.0	19.08
26	9.1	8.1	11.3	16.7	19.0	20.8	20.8	18.2	18.7	17.0	15.5	15.2	21.4	8.1	15.87	18.4	16.9	16.2	17.5	21.3	23.2	23.4	24.0	22.5	19.1	15.9	16.2	24.2	15.5	19.55
27	14.3	14.5	15.4	16.1	16.6	16.3	17.4	15.0	14.9	14.6	14.3	13.5	17.5	13.5	15.22	16.2	15.6	15.0	15.4	16.5	20.2	21.8	21.1	18.7	15.8	15.5	21.9	14.9	17.41	
28	13.0	12.4	12.5	13.3	15.8	15.0	15.2	15.6	15.9	15.3	15.2	15.2	15.9	12.4	14.14	15.2	14.7	13.7	16.4	16.4	15.1	16.0	15.0	15.6	15.1	14.3	15.7	15.26	28	
29	15.2	15.1	14.9	15.4	16.0	16.6	19.1	17.4	16.3	15.5	19.2	14.9	14.6	16.11	14.1	13.0	14.1	14.3	15.4	16.6	17.1	16.0	13.9	12.4	12.2	17.5	12.2	14.38		
30	15.3	15.2	15.5	16.4	17.8	19.9	20.2	21.6	22.8	20.8	17.7	17.3	23.1	15.2	18.38	11.9	11.2	10.2	10.8	14.1	15.2	16.2	16.6	15.1	13.3	12.5	12.3	16.6	10.0	13.26
31	16.3	15.8	16.4	16.7	20.6	22.5	24.7	22.4	24.2	22.3	17.5	16.3	24.7	15.5	19.64	11.9	11.4	10.2	11.4	13.7	15.1	15.0	14.3	13.6	13.8	12.1	15.3	10.2	12.08	31
32	14.54	14.09	15.11	17.05	18.91	20.21	21.09	21.49	20.99	19.42	16.66	15.32	22.45	13.49	17.91	14.42	13.66	13.81	16.29	18.30	20.14	20.81	21.02	20.02	17.74	15.75	14.81	21.64	12.75	17.24

Registrierungen der Lufttemperatur T

1944

Oslo (Blådorn)  
September IX

$\varphi = 60^{\circ} 35' N$     $\lambda = 10^{\circ} 44' E$     $g = 9.813$     $\Delta G = +1^h$     $H_0 = 94$     $H_0 = 53.6$     $h_r = 2.0$     $h_r = 25.2$     $h_r = 25.6$     $h_r = 1.5$

Oktober X

X	2	4	6	8	10	12	14	16	18	20	22	24	Max	Min	Dies	2	4	6	8	10	12	14	16	18	20	22	24	Max	Min	Dies	X	
1	11.3	10.6	10.1	10.7	11.5	13.5	14.6	12.6	11.7	10.3	9.5	14.7	9.5	11.47	3.9	3.3	3.0	4.5	8.5	10.2	11.1	10.6	8.3	5.4	2.8	2.0	11.2	2.0	6.12	1		
2	8.2	7.3	7.3	12.1	13.6	16.9	17.9	16.5	12.5	12.6	12.5	13.9	7.3	12.97	1.2	0.9	0.5	3.1	6.6	9.9	12.8	12.9	7.2	4.5	3.6	2.7	13.0	0.5	5.49	2		
3	11.9	10.9	10.6	11.1	11.4	10.8	10.4	10.2	8.8	8.4	7.9	12.5	7.9	10.05	2.9	3.6	4.3	4.4	5.3	6.6	6.8	7.7	8.1	7.6	6.8	6.2	8.2	2.7	5.86	3		
4	7.8	7.8	7.6	9.2	10.8	11.2	11.6	12.6	12.1	10.2	9.6	13.7	7.6	10.10	6.2	6.1	5.3	5.3	9.1	11.1	12.6	13.2	12.8	11.5	10.8	10.3	13.2	1.5	7.14	4		
5	9.6	9.6	9.6	10.4	10.9	10.3	10.7	11.0	10.8	10.0	9.9	9.7	9.4	10.21	0.6	0.8	2.9	3.6	5.2	7.5	12.3	14.9	11.5	8.0	5.1	3.6	1.3	13.2	1.5	6.92	5	
6	9.2	9.6	9.2	9.7	10.8	12.7	13.4	13.4	11.7	9.9	8.9	13.5	8.7	11.02	6.9	4.6	2.2	2.8	5.5	8.3	9.9	9.9	8.7	7.3	6.8	7.3	9.9	2.0	6.68	6		
7	8.7	9.6	9.9	11.6	15.9	14.9	15.2	15.1	12.9	11.2	10.7	10.5	8.5	15.8	9.3	9.3	8.4	8.2	12.0	17.2	19.4	20.3	16.2	15.1	9.3	7.0	20.6	7.0	12.47	7		
8	10.5	10.6	11.4	12.2	12.2	12.3	12.9	13.0	12.6	11.8	11.2	10.4	10.4	11.76	6.1	4.8	4.8	6.0	9.4	14.0	17.7	18.0	11.8	10.3	7.9	8.2	18.7	4.0	9.92	8		
9	9.6	8.7	7.8	10.5	13.2	14.9	15.8	15.3	11.7	8.6	8.0	8.1	16.5	8.0	11.02	6.8	4.0	3.0	5.0	6.3	8.9	9.9	11.2	10.3	9.0	8.6	7.5	11.7	3.0	7.54	9	
10	7.7	6.3	5.3	9.4	11.9	11.9	15.8	15.2	11.3	8.4	6.5	5.7	14.1	5.3	9.28	6.6	5.8	4.8	6.9	7.7	8.8	9.7	8.5	8.3	5.9	5.9	9.8	4.7	7.39	10		
11	5.5	6.1	6.7	8.5	12.3	16.6	17.4	16.2	14.5	11.6	10.1	9.4	17.7	5.3	11.24	5.9	6.0	6.5	7.0	7.3	8.1	8.6	8.8	8.9	9.1	9.4	10.3	10.5	5.9	7.99	11	
12	10.1	9.6	8.9	10.2	14.9	15.1	15.9	15.2	14.9	9.8	9.6	15.9	8.7	12.00	10.5	10.5	10.4	10.6	10.7	10.9	11.0	11.5	11.1	10.7	10.2	10.0	11.5	10.0	10.67	12		
13	10.0	10.0	9.5	9.9	11.8	14.3	16.2	17.5	15.2	10.2	8.5	7.9	17.5	7.9	11.75	9.9	9.9	9.9	10.1	10.0	10.3	11.0	10.9	11.0	10.8	10.9	10.4	11.0	9.9	10.42	13	
14	7.5	7.0	8.3	9.3	12.4	15.8	16.0	17.4	14.6	9.3	7.7	6.8	17.4	6.8	11.01	10.0	9.6	8.5	9.0	9.1	10.3	10.6	10.6	10.4	9.5	9.6	9.7	10.6	8.5	9.74	14	
15	7.0	7.8	8.7	10.1	12.0	15.5	15.0	14.1	12.8	11.7	12.4	12.5	15.5	6.8	11.03	10.4	10.3	9.5	9.5	9.7	10.8	11.6	11.0	8.9	7.9	7.6	7.1	11.6	7.1	9.52	15	
16	12.3	11.5	10.8	10.2	10.5	13.8	12.9	11.8	12.7	13.1	13.2	11.1	13.8	10.1	11.99	6.8	6.8	6.8	6.6	6.6	7.2	7.9	6.6	6.5	6.5	6.6	6.6	6.6	6.6	6.6	7.76	16
17	12.2	12.3	12.5	12.6	14.1	16.6	17.7	16.1	15.2	10.5	9.3	12.8	7.9	13.28	7.9	8.2	8.8	9.4	10.7	10.8	10.8	10.6	10.6	10.1	9.7	9.0	11.4	7.9	9.72	17		
18	8.4	7.6	7.4	10.0	10.9	12.6	14.6	14.5	14.2	12.8	12.1	11.2	14.6	7.1	11.36	9.1	8.9	9.0	10.0	9.7	10.4	10.3	9.5	8.8	8.3	8.0	10.6	8.0	9.17	18		
19	10.7	10.7	9.4	12.5	16.8	17.5	17.4	17.6	15.7	15.3	10.5	18.7	9.2	13.35	7.6	6.7	6.7	7.2	8.8	11.4	10.8	8.2	7.4	6.9	7.0	11.5	6.7	7.95	19			
20	11.1	11.0	11.0	10.2	10.0	10.5	11.6	12.7	12.4	11.6	10.7	10.5	12.7	10.0	11.11	7.0	6.2	3.0	3.9	7.7	7.5	8.5	8.2	6.9	7.0	6.8	6.5	8.5	2.5	6.19	20	
21	10.5	10.5	10.5	10.8	11.5	11.8	12.4	12.6	12.2	11.2	11.2	11.9	12.7	10.5	11.42	6.7	6.9	7.1	6.9	7.7	9.5	9.7	8.9	7.7	5.3	3.9	5.1	9.8	3.8	7.12	21	
22	11.4	11.4	11.2	12.0	13.5	14.6	13.1	11.7	11.4	11.2	10.0	14.6	10.0	11.91	5.2	5.2	4.6	4.4	5.8	7.6	7.8	7.8	7.2	6.9	6.9	6.9	7.8	4.4	6.36	22		
23	10.4	10.1	9.9	10.3	11.2	11.7	11.8	12.6	12.8	12.9	12.1	12.3	12.9	11.2	11.51	6.8	6.8	5.6	5.4	5.2	5.2	5.3	5.6	6.0	6.1	6.3	6.9	5.2	5.80	23		
24	12.6	13.4	13.6	13.8	15.6	15.8	15.8	12.8	11.5	11.1	10.7	9.9	13.8	9.9	12.55	6.3	6.3	6.3	6.3	6.3	6.4	6.4	6.6	6.6	6.6	6.6	6.6	6.7	6.3	6.41	24	
25	9.8	9.3	8.4	7.8	8.8	10.7	11.0	11.4	9.5	6.5	5.6	5.4	11.5	5.0	8.68	6.5	6.5	6.6	6.7	7.5	7.5	7.5	7.5	7.4	7.4	7.5	7.5	6.5	7.12	25		
26	5.7	6.5	6.9	7.0	8.7	11.9	10.4	12.3	10.3	7.3	5.8	6.7	12.9	5.3	8.34	7.4	7.4	7.4	7.4	7.6	8.2	8.2	7.6	6.9	6.5	5.2	9.2	5.2	7.27	26		
27	6.5	4.9	2.8	4.3	8.6	10.9	11.9	12.3	10.3	7.0	5.5	12.5	1.8	7.86	5.1	5.2	5.3	5.2	5.5	5.5	5.6	5.6	5.6	5.6	5.6	5.6	5.6	5.1	5.43	27		
28	4.8	5.6	6.1	7.7	10.3	11.2	13.4	12.4	10.9	9.0	6.8	3.3	13.4	3.3	8.46	5.6	5.6	4.9	4.8	4.9	5.2	5.4	5.3	5.2	4.9	4.9	4.9	5.6	4.5	5.10	28	
29	1.9	1.1	0.5	3.3	7.0	9.0	10.2	10.4	10.3	10.0	9.8	9.7	10.4	0.5	6.93	4.1	4.2	4.3	3.7	3.8	3.7	4.0	4.1	4.1	4.1	4.2	4.6	3.7	3.99	29		
30	9.7	10.1	10.0	10.4	10.5	10.9	9.8	8.5	8.2	7.8	6.9	5.3	10.9	5.3	9.01	4.1	4.0	3.9	3.7	4.4	4.9	5.3	5.6	3.5	2.2	0.9	-0.1	5.6	-0.1	3.53	30	
M	9.10	8.92	8.73	9.90	11.55	15.02	13.64	13.60	12.41	10.59	9.69	9.05	14.40	7.95	10.85	6.22	5.92	5.61	6.01	7.07	8.48	9.41	9.54	8.19	7.31	6.68	6.34	9.98	4.66	7.23	N	

November XI

Dezember XII

1	2.3	1.6	1.4	1.4	2.3	3.7	4.3	3.9	3.4	3.0	3.4	3.5	4.4	1.1	2.85	2.6	1.8	0.7	0.6	0.4	0.9	1.3	2.4	3.1	4.0	5.9	6.0	0.4	2.48	1	
2	3.4	3.9	3.6	4.0	4.2	4.3	5.0	5.0	3.7	3.9	3.9	3.6	5.0	3.4	4.04	6.1	6.7	7.2	7.4	7.4	6.5	6.0	4.5	3.6	2.8	2.7	2.6	2.6	2.6	5.39	2
3	3.7	3.6	3.8	4.4	4.6	4.9	5.3	5.3	4.9	4.3	4.2	3.9	5.3	3.5	4.41	2.2	1.6	0.5	0.3	0.7	0.5	0.6	0.6	0.6	0.4	0.4	0.4	0.4	0.4	0.39	3
4	3.0	3.2	3.2	2.8	3.4	3.5	6.6	6.0	4.2	2.2	2.1	2.5	6.6	1.9	3.36	0.7	0.7	0.7	0.7	0.7	0.8	0.8	0.5	0.5	0.5	0.4	0.4	0.4	0.3	0.39	4
5	5.0	8.6	9.8	10.4	10.8	11.2	10.7	10.4	6.1	5.5	5.4	5.3	11.5	2.5	8.87	-0.5	-0.4	0.1	0.4	0.4	0.8	0.8	0.4	0.2	0.4	0.2	0.4	0.2	0.4	0	

## Registrierungen der relativen Feuchte U

Oslo (Blaðadorn)

bawar. I

◎ = 2° 26' N 1°

$10^{\circ} 44' E$        $\lambda = 9$

19  $\Delta G = +1^b$

1944

1

## Registrierungen der relativen Feuchte U

1944

Oslo (Blaadern)

Mai

$$\phi = 22^\circ 26' N$$

$\alpha = 10^{\circ} 44' E$

$$= 9.810 \quad \Delta G$$

$H_b = 94$        $H_b = 95.6$

b<sub>2</sub> = 2

10

2 h

**25.6**       $h_r = 1.5$

Juni VI

Dy	2		4		6		8		10		12		14		16		18		20		22		24		Max		Min		Dies		Dat																																																																				
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99
1	96	51	97	77	53	57	67	64	76	94	87	83	97	89	98	95	92	90	88	86	84	82	80	78	76	74	72	70	68	66	64	62	60	58	56	54	52	50	48	46	44	42	40	38	36	34	32	30	28	26	24	22	20	18	16	14	12	10	8	6	4	2	1																																				
2	95	50	96	76	52	56	66	63	74	93	85	81	95	87	90	88	92	89	86	84	82	80	78	76	74	72	70	68	66	64	62	60	58	56	54	52	50	48	46	44	42	40	38	36	34	32	30	28	26	24	22	20	18	16	14	12	10	8	6	4	2	1																																					
3	94	50	95	75	51	55	65	62	73	92	84	80	94	86	89	87	91	88	85	83	81	79	77	75	73	71	69	67	65	63	61	59	57	55	53	51	49	47	45	43	41	39	37	35	33	31	29	27	25	23	21	19	17	15	13	11	9	7	5	3	1																																						
4	93	50	94	74	50	54	64	61	72	91	83	79	93	85	88	86	90	87	84	82	80	78	76	74	72	70	68	66	64	62	60	58	56	54	52	50	48	46	44	42	40	38	36	34	32	30	28	26	24	22	20	18	16	14	12	10	8	6	4	2	1																																						
5	92	50	93	73	50	53	63	60	71	90	82	78	92	84	87	85	89	86	83	81	79	77	75	73	71	69	67	65	63	61	59	57	55	53	51	49	47	45	43	41	39	37	35	33	31	29	27	25	23	21	19	17	15	13	11	9	7	5	3	1																																							
6	91	50	92	72	50	52	62	59	70	89	81	77	91	83	86	84	88	85	82	80	78	76	74	72	70	68	66	64	62	60	58	56	54	52	50	48	46	44	42	40	38	36	34	32	30	28	26	24	22	20	18	16	14	12	10	8	6	4	2	1																																							
7	90	50	91	71	50	51	61	58	69	88	80	76	90	82	85	83	87	84	81	79	77	75	73	71	69	67	65	63	61	59	57	55	53	51	49	47	45	43	41	39	37	35	33	31	29	27	25	23	21	19	17	15	13	11	9	7	5	3	1																																								
8	89	50	90	70	50	49	59	56	67	87	79	75	89	81	84	82	86	83	80	78	76	74	72	70	68	66	64	62	60	58	56	54	52	50	48	46	44	42	40	38	36	34	32	30	28	26	24	22	20	18	16	14	12	10	8	6	4	2	1																																								
9	88	50	89	69	50	49	59	56	67	86	78	74	88	80	83	81	85	82	79	77	75	73	71	69	67	65	63	61	59	57	55	53	51	49	47	45	43	41	39	37	35	33	31	29	27	25	23	21	19	17	15	13	11	9	7	5	3	1																																									
10	87	50	88	68	50	49	58	55	66	85	77	73	87	79	82	80	84	79	76	74	72	70	68	66	64	62	60	58	56	54	52	50	48	46	44	42	40	38	36	34	32	30	28	26	24	22	20	18	16	14	12	10	8	6	4	2	1																																										
11	86	50	87	67	50	49	57	54	65	84	76	72	86	78	81	79	83	80	77	75	73	71	69	67	65	63	61	59	57	55	53	51	49	47	45	43	41	39	37	35	33	31	29	27	25	23	21	19	17	15	13	11	9	7	5	3	1																																										
12	85	50	86	66	50	49	56	53	64	83	75	71	85	77	80	78	82	79	76	74	72	70	68	66	64	62	60	58	56	54	52	50	48	46	44	42	40	38	36	34	32	30	28	26	24	22	20	18	16	14	12	10	8	6	4	2	1																																										
13	84	50	85	65	50	49	55	52	63	82	74	70	84	76	79	77	81	78	75	73	71	69	67	65	63	61	59	57	55	53	51	49	47	45	43	41	39	37	35	33	31	29	27	25	23	21	19	17	15	13	11	9	7	5	3	1																																											
14	83	50	84	64	50	49	54	51	62	81	73	69	83	75	78	76	80	77	74	72	70	68	66	64	62	60	58	56	54	52	50	48	46	44	42	40	38	36	34	32	30	28	26	24	22	20	18	16	14	12	10	8	6	4	2	1																																											
15	82	50	83	63	50	49	53	50	61	80	72	68	82	74	77	75	81	78	75	73	71	69	67	65	63	61	59	57	55	53	51	49	47	45	43	41	39	37	35	33	31	29	27	25	23	21	19	17	15	13	11	9	7	5	3	1																																											
16	81	50	82	62	50	49	52	49	60	79	71	67	81	73	76	74	79	76	73	71	69	67	65	63	61	59	57	55	53	51	49	47	45	43	41	39	37	35	33	31	29	27	25	23	21	19	17	15	13	11	9	7	5	3	1																																												
17	80	50	81	61	50	49	51	48	59	78	70	66	80	72	75	73	78	75	72	70	68	66	64	62	60	58	56	54	52	50	48	46	44	42	40	38	36	34	32	30	28	26	24	22	20	18	16	14	12	10	8	6	4	2	1																																												
18	79	50	80	60	50	49	48	45	56	77	69	65	79	71	74	72	77	74	71	69	67	65	63	61	59	57	55	53	51	49	47	45	43	41	39	37	35	33	31	29	27	25	23	21	19	17	15	13	11	9	7	5	3	1																																													
19	78	50	79	59	50	49	48	45	55	76	68	64	78	70	73	71	76	73	70	68	66	64	62	60	58	56	54	52	50	48	46	44	42	40	38	36	34	32	30	28	26	24	22	20	18	16	14	12	10	8	6	4	2	1																																													
20	77	50	78	58	50	49	47	44	54	75	67	63	77	69	72	70	75	72	70	68	66	64	62	60	58	56	54	52	50	48	46	44	42	40	38	36	34	32	30	28	26	24	22	20	18	16	14	12	10	8	6	4	2	1																																													
21	76	50	77	57	50	49	46	43	53	74	66	62	76	68	71	69	74	71	69	67	65	63	61	59	57	55	53	51	49	47	45	43	41	39	37	35	33	31	29	27	25	23	21	19	17	15	13	11	9	7	5	3	1																																														
22	75	50	76	56	50	49	45	42	52	73	65	61	75	67	70	68	73	70	68	66	64	62	60	58	56	54	52	50	48	46	44	42	40	38	36	34	32	30	28	26	24	22	20	18	16	14	12	10	8	6	4	2	1																																														
23	74	50	75	55	50	49	44	41	51	72	64	60	74	66	69	67	72	69	67	65	63	61	59	57	55	53	51	49	47	45	43	41	39	37	35	33	31	29	27	25	23	21	19	17	15	13	11	9	7	5	3	1																																															
24	73	50	74	54	50	49	43	40	50	71	63	59	73	65	68	66	71	68	66	64	62	60	58	56	54	52	50	48	46	44	42	40	38	36	34	32	30	28	26	24	22	20	18	16	14	12	10	8	6	4	2	1																																															
25	72	50	73	53	50	49	42	39	49	70	62	58	72	64	67	65	70	67	65	63	61	59	57	55	53	51	49	47	45	43	41	39	37	35	33	31	29	27	25	23	21	19	17	15	13	11	9	7	5	3	1																																																
26	71	50	72	52	50	49	41	38	48	69	61	57	71	63	66	64	69	6																																																																																	

July VIII

## August VIII

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	M
89	90	91	92	93	94	95	96	97	98	99	90	91	92	93	94	95	96	97	98	99	90	91	92	93	94	95	96	97	98	99	88
99	89	91	92	93	94	95	96	97	98	99	90	91	92	93	94	95	96	97	98	99	90	91	92	93	94	95	96	97	98	99	88
98	90	91	92	93	94	95	96	97	98	99	90	91	92	93	94	95	96	97	98	99	90	91	92	93	94	95	96	97	98	99	88
97	98	99	90	91	92	93	94	95	96	97	90	91	92	93	94	95	96	97	98	99	90	91	92	93	94	95	96	97	98	99	88
96	97	98	99	90	91	92	93	94	95	96	90	91	92	93	94	95	96	97	98	99	90	91	92	93	94	95	96	97	98	99	88
95	96	97	98	99	90	91	92	93	94	95	90	91	92	93	94	95	96	97	98	99	90	91	92	93	94	95	96	97	98	99	88
94	95	96	97	98	99	90	91	92	93	94	90	91	92	93	94	95	96	97	98	99	90	91	92	93	94	95	96	97	98	99	88
93	94	95	96	97	98	99	90	91	92	93	90	91	92	93	94	95	96	97	98	99	90	91	92	93	94	95	96	97	98	99	88
92	93	94	95	96	97	98	99	90	91	92	90	91	92	93	94	95	96	97	98	99	90	91	92	93	94	95	96	97	98	99	88
91	92	93	94	95	96	97	98	99	90	91	90	91	92	93	94	95	96	97	98	99	90	91	92	93	94	95	96	97	98	99	88
90	91	92	93	94	95	96	97	98	99	90	91	92	93	94	95	96	97	98	99	90	91	92	93	94	95	96	97	98	99	88	
89	90	91	92	93	94	95	96	97	98	99	90	91	92	93	94	95	96	97	98	99	90	91	92	93	94	95	96	97	98	99	88
88	89	90	91	92	93	94	95	96	97	98	88	89	90	91	92	93	94	95	96	97	88	89	90	91	92	93	94	95	96	97	88

## **Registrierungen der relativen Feuchte U**

Oslo (Skandern)  
September IX

September 18

θ = 3° 35' N

$\lambda = 10^{\circ} 44'E$

AGE 3

1<sup>st</sup>      H<sub>2</sub> 94      H<sub>2</sub> 91

1

10

0

高 2

h

234

1

1.5

Oktober >

November XI

Dezember XI

Registrierungen des Windes D,v

1944

Oslo (Blindern)

Januar I

$\varphi = 60^{\circ} 56' N$

$l = 10^{\circ} 44' E$

$g = 9.819$

$\Delta G = +1^h$

$H_0 = 94$

$H_b = 95.6$

$h_t = 2.0$

$h_a = 25.2$

$h_d = 25.6$

$h_r = 1.5$

Februar II

Dat	2	4	6	8	10	12	14	16	18	20	22	24	2	4	6	8	10	12	14	16	18	20	22	24	Dat			
1	06	0.6	19	1.8	19	3.0	22	2.4	04	1.2	12	1.2	21	4.3	26	5.5	06	3.0	29	1.2	03	0.6	01	0.5	24	0.5		
2	05	1.8	02	1.2	01	1.2	01	0.6	02	2.4	02	0.6	02	1.8	06	1.2	01	0.6	01	1.2	03	0.5	06	0.6	25	0.8		
3	02	0.6	04	1.2	14	0.6	23	1.2	26	4.9	02	1.2	23	5.5	21	1.8	06	1.2	01	1.2	03	0.5	06	0.6	22	2.4		
4	01	0.5	32	6.7	01	7.9	03	3.0	06	0.6	19	1.2	03	1.2	03	2.4	27	2.4	01	0.6	01	0.6	02	0.6	23	1.2		
5	01	5.5	32	5.5	01	7.2	20	0.6	21	1.2	21	0.6	26	0.6	14	0.6	19	4.9	18	4.5	18	9.1	01	2.4	32	0.6		
6	18	8.5	18	4.3	18	7.3	18	3.6	03	5.5	03	8.5	21	8.5	22	7.3	23	7.9	22	9.1	24	6.7	09	1.8	30	0.6		
7	7	4.9	22	5.5	21	3.0	18	2.4	03	20	2.4	29	1.8	28	2.4	23	5.6	21	1.2	06	28	4.3	17	4.9	18	5.5		
8	06	0.6	32	1.2	21	1.2	13	1.2	21	2.1	29	0.6	28	0.6	18	1.8	01	0.6	01	1.2	03	0.5	06	0.6	28	1.1		
9	01	7.3	03	1.8	08	3.0	02	1.2	08	0.6	02	1.2	08	1.2	08	0.6	07	0.6	11	1.8	05	1.0	01	1.1	02	0.9		
10	28	0.6	02	0.6	08	0.0	02	1.8	02	0.6	02	0.6	08	0.6	03	1.2	04	0.6	01	9.0	01	12.0	01	6.7	01	5.5		
11	05	0.6	02	0.6	08	0.6	02	0.6	26	7.3	27	10.3	32	3.0	23	3.0	14	0.5	05	0.6	08	0.6	25	0.6	20	1.2		
12	02	0.8	00	0.0	02	1.2	02	0.6	02	0.6	02	1.2	02	1.2	02	1.2	02	1.2	02	1.2	02	1.2	02	1.2	02	1.2		
13	06	0.6	00	0.0	02	1.2	02	0.6	01	0.6	01	0.6	01	0.6	01	0.6	01	0.6	01	0.6	01	0.6	01	0.6	01	0.6		
14	08	2.4	32	3.6	3.6	10	1.2	06	02	0.6	02	0.6	02	0.6	02	0.6	02	0.6	02	0.6	02	0.6	02	0.6	02	0.6		
15	32	0.6	02	0.6	08	0.6	01	1.2	02	0.6	02	1.2	02	1.2	02	1.2	02	1.2	02	1.2	02	1.2	02	1.2	02	1.2		
16	02	1.2	02	1.2	03	1.8	03	0.6	02	0.6	02	0.6	02	0.6	02	0.6	02	0.6	02	0.6	02	0.6	02	0.6	02	0.6		
17	02	0.6	01	1.8	06	0.6	11	2.0	02	0.6	02	0.6	02	0.6	02	0.6	02	0.6	02	0.6	02	0.6	02	0.6	02	0.6		
18	21	0.6	21	1.2	18	0.6	18	0.6	02	0.6	02	0.6	02	0.6	02	0.6	02	0.6	02	0.6	02	0.6	02	0.6	02	0.6		
19	25	1.2	21	1.2	05	0.6	19	0.6	19	0.6	19	0.6	19	0.6	19	0.6	19	0.6	19	0.6	19	0.6	19	0.6	19	0.6		
20	18	1.2	06	1.2	02	0.6	03	1.2	27	1.2	26	0.6	03	1.2	27	0.6	03	1.2	26	0.6	03	1.2	27	0.6	03	1.2		
21	29	0.6	08	0.6	28	1.2	05	2.4	00	0.0	25	1.2	05	0.6	22	1.8	18	0.6	04	0.6	08	1.8	05	1.2	12	0.6		
22	15	0.6	15	1.8	16	1.2	17	1.2	16	3.6	18	6.7	18	3.0	25	2.4	22	1.8	05	1.2	21	1.2	22	1.8	05	1.2		
23	28	5.5	28	1.2	27	1.8	05	0.6	10	3.0	29	3.6	29	5.5	28	5.5	28	1.8	27	1.2	28	4.3	28	4.9	28	5.5		
24	27	1.8	28	5.5	29	4.9	30	6.1	30	6.1	28	6.7	16	3.0	27	2.4	30	1.2	05	1.2	28	3.6	28	4.3	28	5.5		
25	04	3.6	04	4.9	02	4.3	06	3.6	04	3.0	04	4.3	02	7.9	05	9.1	02	10.9	02	9.7	02	9.7	02	10.9	02	9.7		
26	01	7.9	01	7.3	32	3.6	32	3.0	02	4.3	02	4.5	05	2.4	06	1.8	01	3.6	06	1.8	01	2.2	01	1.2	01	1.2		
27	02	0.6	06	0.6	03	1.2	02	0.6	24	2.4	22	4.9	24	0.6	03	1.2	02	0.6	03	1.2	02	0.6	03	1.2	02	0.6		
28	22	0.6	22	1.2	16	1.8	22	2.4	08	1.2	28	3.6	28	6.7	28	4.9	26	2.4	08	1.2	28	3.6	28	6.7	28	1.2		
29	01	0.6	24	0.6	05	1.2	05	0.6	05	1.2	20	1.2	20	0.6	05	1.2	05	1.2	05	1.2	05	1.2	05	1.2	05	1.2		
30	16	1.8	24	6.6	24	10.3	26	4.3	28	3.0	18	1.8	20	3.0	24	7.0	16	4.9	26	1.2	09	1.8	04	2.4	16	5.5		
31	03	4.9	03	3.6	04	2.4	24	0.6	04	0.6	05	1.2	03	0.6	29	1.0	24	1.0	25	1.7	32	1.3	04	0.6	04	0.6		
		2.41		2.27		2.34		1.75		2.16		2.36		2.38		2.25		2.13		2.15		2.28		2.64		2.18		1.85

März III

April IV

1	17	7.9	16	7.3	17	3.6	18	6.7	19	5.5	28	6.1	19	3.0	23	2.4	22	1.8	03	1.2	20	4.3	20	4.9	20	5.5
2	22	1.2	23	1.2	24	0.6	25	0.6	24	0.6	20	1.8	17	3.6	17	4.3	18	2.4	03	1.2	20	4.3	20	4.9	20	5.5
3	17	1.8	18	1.2	16	1.2	22	1.2	21	3.6	21	4.9	19	1.2	22	1.2	04	3.0	1.2	03	1.2	20	4.3	20	4.9	20
4	18	2.4	18	0.6	22	1.2	06	0.6	20	1.8	21	4.9	18	2.4	22	1.2	04	3.0	1.2	03	1.2	20	4.3	20	4.9	20
5	04	1.8	04	1.2	04	1.2	06	0.6	16	0.6	02	1.2	31	1.2	27	1.8	26	0.6	03	1.2	04	1.2	03	1.2	04	1.2
6	11	0.6	30	1.2	08	1.8	06	1.8	02	4.9	05	2.4	06	1.8	01	3.6	08	1.2	07	1.2	08	1.2	07	1.2	08	1.2
7	07	0.6	07	0.6	03	1.2	05	1.8	02	2.4	22	1.8	27	1.8	28	2.4	05	1.2	03	1.2	04	1.2	03	1.2	04	1.2
8	08	0.6	04	0.6	03	0.6	04	0.6	04	0.6	20	1.2	22	1.8	20	0.6	05	1.2	03	1.2	04	1.2	03	1.2	04	1.2
9	09	0.6	00	0.2	0.6	04	0.6	04	0.6	04	0.6	04	0.6	04	0.6	04	0.6	04	0.6	04	0.6	04	0.6	04	0.6	04
10	10	32	1.2	02	0.6	04	0.6	04	0.6	04	0.6	04	0.6	04	0.6	04	0.6	04	0.6	04	0.6	04	0.6	04	0.6	04
11	28	6.7	27	6.1	26	3.0	08	3.0	05	4.9	18	9.7	22	9.1	18	7.9	17	6.7	18	4.3	19	3.6	20	4.9	20	5.5
12	20	1.8	22	1.8	16	1.2	03	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
13	03	1.2	03	3.6	03	4.9	02	8.5	03	5.5	03	8.5	03	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
14	22	6.1	02	7.9	01	3.0	03	5.5	02	6.1	02	5.5	01	5.												

## Registrierungen des Windes D,v

1944

**Oslo (Blastrand)**

May V

$$\phi = 53^\circ \text{ N}$$

$10^{\circ} 44' E$

$$\Delta G = +1$$

H<sub>0</sub> = 90

H<sub>b</sub> = 93.6

**h<sub>c</sub> = 2.0**

= 23.2      h<sub>4</sub> =

**25.6**       $h_r = 1$

Juni VI

Juli VIII

August VIII

## **Registrierungen des Windes D.v**

1944

**Oslo (Blastrand)**  
**September IX**

$$\phi = 35^\circ 35' N \quad L = 10^\circ 44' E \quad g = 9.819 \quad \Delta G = +1^h \quad H_1 = 94 \quad H_0 = 35.6 \quad h_L = 2.0 \quad h_0 = 35.2 \quad h_0 = 35.6 \quad h_r = 1.$$

Oktober X

D	2	4	6	8	10	12	14	16	18	20	22	24	2	4	6	8	10	12	14	16	18	20	22	24			
1	22	2.4	24	1.2	24	1.8	21	3.0	22	1.8	20	1.2	25	1.2	32	2.4	01	1.8	29	1.2	29	0.6	06	0.6	07	1.2	
2	03	1.2	32	1.2	01	0.6	03	1.2	20	0.6	16	1.2	21	1.8	29	1.8	05	3.0	02	3.0	04	4.3	01	3.6	02	1.8	
3	03	3.6	03	3.6	04	4.9	04	6.7	06	8.5	02	8.5	02	8.5	01	7.9	01	9.1	02	6.7	02	6.1	02	4.3	02	4.3	
4	32	2.4	16	1.2	03	0.6	02	2.4	15	1.2	21	1.2	19	1.2	10	1.2	23	1.8	07	1.2	04	1.8	02	4.9	03	3.6	
5	03	2.4	03	3.0	02	4.9	03	4.9	05	4.9	04	4.9	04	4.9	05	6.1	01	5.5	02	4.9	02	4.0	02	4.3	02	4.9	
6	03	4.5	02	3.6	02	3.6	04	3.0	05	3.6	06	2.4	01	1.2	23	0.6	23	1.2	19	0.6	03	1.2	02	3.6	00	0.0	
7	32	1.8	01	3.0	03	0.6	03	1.2	08	2.4	08	1.8	09	1.8	05	2.4	01	2.4	02	3.0	01	4.9	02	3.2	01	4.9	
8	02	7.3	08	7.9	06	4.9	09	3.6	08	5.8	08	4.9	13	3.6	20	4.3	02	1.8	21	7.3	18	7.5	15	4.7	02	3.2	
9	17	4.3	17	4.3	21	2.4	16	1.2	15	1.2	16	2.4	16	1.8	16	1.8	24	1.8	01	6.7	32	7.9	22	2.1	01	9.0	
10	32	4.9	27	0.6	1.8	01	1.8	02	2.4	21	1.8	28	5.0	18	2.4	16	1.8	28	1.2	30	1.2	01	1.8	18	2.0	01	5.5
11	01	2.2	01	1.2	02	1.8	01	0.6	24	0.6	20	2.4	01	3.0	21	2.4	26	1.2	05	1.8	24	3.2	1.2	32	5.5	02	4.0
12	32	1.8	32	0.6	02	1.8	20	1.2	08	0.6	21	1.8	19	1.2	19	0.6	19	1.2	02	1.8	01	1.2	15	2.4	15	3.6	12
13	32	2.4	01	1.8	02	1.8	06	0.6	04	1.2	07	1.8	15	1.2	20	1.8	20	1.2	06	0.6	32	1.8	01	2.4	15	3.6	16
14	32	3.6	32	1.8	02	1.8	06	20	3.6	19	1.8	21	2.4	17	2.4	03	0.6	24	0.2	2.4	17	4.9	16	3.0	15	4.9	
15	32	2.4	02	2.4	07	1.2	03	0.6	16	1.2	18	4.3	18	3.6	16	3.6	21	0.6	08	0.6	17	1.8	18	3.0	01	2.4	
16	15	4.3	17	3.6	17	1.8	08	1.8	06	1.2	14	1.2	16	1.2	03	2.4	08	4.3	16	3.3	16	3.6	02	4.0	05	3.6	21
17	14	2.3	16	3.1	15	2.3	16	2.4	16	3.4	19	3.5	18	2.8	21	2.1	19	1.8	01	1.2	32	1.6	01	6.7	17	4.9	15
18	13	2.0	03	1.1	31	0.9	30	0.8	29	0.6	32	0.6	22	1.2	21	0.6	22	0.8	03	1.1	03	0.8	32	1.3	13	6.1	14
19	01	1.4	01	1.0	02	0.9	28	1.1	32	1.1	09	2.4	08	2.4	04	3.0	05	2.4	08	2.1	02	4.0	2.4	14	12	0.6	19
20	20	02	3.4	02	3.5	01	4.4	04	5.7	04	6.0	04	4.1	15	2.6	32	1.9	08	1.2	02	1.7	06	1.8	06	2.1	11	0.6
21	32	2.4	04	2.2	04	1.6	06	1.1	04	2.9	06	3.4	05	2.8	03	2.7	32	4.0	01	3.8	32	3.6	05	2.4	03	3.0	05
22	01	4.0	02	3.9	04	4.2	08	3.1	06	4.0	08	3.2	08	3.0	09	4.3	07	3.6	06	2.4	05	3.0	03	2.4	06	1.2	06
23	04	3.6	04	3.0	07	3.0	07	2.4	08	1.8	08	2.4	08	2.4	06	1.2	07	3.6	05	5.5	04	6.7	03	5.5	04	6.7	03
24	08	5.5	12	4.9	16	1.8	15	1.2	16	3.0	20	2.4	17	3.0	16	3.6	15	3.0	14	2.4	16	3.0	02	4.3	04	4.3	05
25	07	1.8	07	1.2	03	1.2	03	3.6	04	4.3	04	3.6	04	4.3	02	4.9	32	3.6	05	0.6	27	1.2	04	5.0	06	0.6	00
26	04	0.6	00	0.0	0.0	20	1.8	22	2.4	22	1.8	21	2.4	18	2.4	25	2.4	22	4.3	18	5.5	16	1.2	15	1.8	20	3.0
27	16	3.6	19	1.2	02	1.2	06	22	3.0	17	3.6	16	5.5	16	4.3	15	4.9	14	1.8	16	3.0	09	3.6	00	3.0	4.9	16
28	01	2.4	02	2.4	02	3.0	32	1.8	17	1.2	17	1.8	24	1.8	21	1.8	26	1.8	28	4.3	30	2.4	4.9	04	4.9	04	6.1
29	32	0.6	02	0.6	02	1.2	03	1.2	09	1.2	17	1.8	18	6.7	10	7.3	18	6.1	17	5.5	15	02	6.7	02	4.9	01	6.1
30	15	1.8	16	0.6	16	0.6	21	1.2	22	1.8	26	3.6	27	8.5	24	6.7	27	5.5	20	2.4	24	3.0	32	5.5	32	3.6	02
M	2.86	2.34	2.11	2.16	2.56	2.60	3.24	2.99	3.07	2.77	2.88	3.03	3.12	3.01	2.86	2.64	2.85	3.38	3.19	3.57	3.22	3.19	3.12	3.28	3.01		

November XI

Dezember XII

Registrierungen des Niederschlags R

1944

Ostal (Blinde)  $\varphi = 59^{\circ} 56' N$   $z = 10^{\circ} 44' E$   $g = 9.819$   $\Delta G = +1^{\circ}$   $H_s = 94$   $H_e = 95.6$   $h_s = 2.0$   $h_e = 25.6$   $h_r = 1.3$

D	Januar I												Dauer in Stunden	April IV												D					
	2	4	6	8	10	12	14	16	18	20	22	24		2	4	6	8	10	12	14	16	18	20	22	24						
1	-	1.6	0.6	-	-	-	-	-	0.0	-	-	-	2.2	1.5	-	-	0.1	0.3	0.2	0.6	1.0	-	-	0.2	0.0	2.3	4.0	11			
5	-	-	-	-	-	-	-	-	0.0	1.1	1.4	0.8	0.1	3.4	5.0	-	0.1	0.2	0.1	-	-	-	-	0.1	-	0.2	0.5	12			
9	0.1	-	0.1	-	-	-	-	0.3	0.2	0.1	0.2	0.7	1.2	4.4	0.5	-	0.4	0.4	0.8	0.1	-	-	-	-	0.1	-	0.4	1.5	16		
13	-	0.7	0.9	0.1	-	-	-	-	-	-	-	-	-	7.9	4.5	-	0.3	-	-	-	-	3.9	6.8	0.3	-	-	11.0	4.5	17		
14	2.5	4.2	1.1	0.1	-	-	-	-	-	-	-	-	-	0.2	0.5	-	0.3	-	-	-	-	-	-	-	0.1	0.5	22				
19	-	0.0	0.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.1	0.5	26				
21	-	-	0.7	1.1	0.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.1	0.5	27				
22	-	-	-	-	1.6	0.5	0.2	0.4	4.4	2.0	-	-	-	2.2	3.0	-	0.0	-	-	-	-	-	-	-	0.1	0.5	28				
24	0.2	0.1	-	-	-	-	-	-	0.1	0.5	1.1	1.0	-	14.3	9.0	-	-	-	-	-	-	-	-	0.0	0.3	0.5	29				
25	0.4	0.1	-	-	-	-	-	-	-	-	-	-	-	0.3	1.0	-	-	-	-	-	-	-	-	-	0.3	0.5	30				
26	-	-	-	0.4	1.7	-	-	-	-	-	-	-	-	-	2.1	2.0	-	-	-	-	-	-	-	-	-	-	20.5				
31	-	-	-	-	-	-	-	-	-	-	-	-	-	3.2	6.7	3.5	1.8	4.3	3.8	3.5	4.6	3.3	2.1	2.6	2.3	41.7	49.0				
Februar II												Mai V												0.7 1.5 1							
1	-	-	-	-	-	-	-	-	0.7	0.4	0.1	-	1.2	1.5	0.0	-	-	0.1	0.6	2.4	2.1	0.2	-	-	-	4.9	5.0	2			
4	-	-	0.5	-	0.4	0.3	0.1	-	-	-	-	-	1.3	2.5	0.9	3.3	2.7	2.6	5.6	4.0	2.0	0.7	0.8	0.2	-	6.5	10.0	3			
7	-	-	1.5	2.2	2.1	-	-	-	-	-	-	-	5.8	5.0	-	-	-	0.1	-	-	-	-	-	-	-	1.2	3.5	14			
14	-	0.0	0.1	-	-	-	-	-	-	-	-	-	0.1	0.5	-	-	-	-	-	-	-	-	-	-	-	4.7	8.3	16			
15	-	0.4	1.5	0.7	0.9	0.8	0.3	-	-	-	-	-	4.6	8.5	-	-	-	0.0	-	-	-	-	-	-	-	1.3	0.5	17			
27	-	0.4	3.0	3.5	3.0	1.2	0.6	0.1	0.7	0.5	0.1	0.0	13.1	18.5	-	-	-	0.1	0.0	1.8	0.1	-	-	-	0.9	-	2.3	0.5	27		
-	0.4	3.0	3.5	3.0	1.2	0.6	0.1	0.7	0.5	0.1	0.0	13.1	18.5	-	-	-	-	-	-	-	-	-	-	-	0.9	0.5	30				
März III												Juni VI												0.1 0.5 1							
1	-	-	0.0	0.1	-	-	0.8	0.3	-	-	-	-	1.2	1.5	4.2	5.4	5.5	1.2	-	0.1	-	3.3	0.8	4.5	0.2	0.3	0.8	0.1	10.1	5.0	2
3	-	0.1	-	0.0	-	-	0.0	-	-	-	-	-	0.1	0.5	-	-	-	0.2	-	0.2	-	0.8	-	1.8	1.5	3.6	4.6	12.3			
10	-	0.4	0.1	-	1.9	0.4	-	-	0.1	0.2	0.9	0.1	-	5.6	5.5	-	1.4	1.2	4.3	0.5	-	0.6	0.2	0.8	-	8.5	7.0	4			
19	0.1	0.1	3.0	1.9	0.4	-	0.2	0.9	0.1	-	-	-	1.1	2.5	-	-	1.1	4.3	0.5	-	0.9	0.6	0.2	-	0.4	4.0	5.5	6			
25	-	-	-	-	0.1	-	-	-	-	-	-	-	0.3	0.5	-	-	0.3	0.5	0.4	0.7	1.9	0.5	-	-	0.2	3.5	6.3	7.5	7		
26	-	-	-	-	-	-	-	-	-	-	-	-	0.1	0.5	-	-	0.6	0.4	0.4	0.7	1.9	0.5	-	-	0.2	3.5	6.3	7.5	8		
30	0.4	0.3	0.1	0.1	-	-	-	-	-	-	-	-	0.9	3.5	-	-	0.6	0.9	0.6	0.7	2.3	2.6	2.4	-	0.3	0.5	1.0	1.0	11		
0.5	0.9	3.2	2.1	0.5	0.2	1.9	0.4	-	0.3	-	0.1	10.1	16.0	12.5	10.6	16.8	3.8	2.2	9.5	7.5	12.8	4.0	2.4	3.5	12.0	102.4	77.0				

## **Registrierungen des Niederschlags R**

1944

Ostic (Blaauw)  $\phi = 59^{\circ} 56' N$

$\lambda = 10^{\circ} 44' E$

g = 9.819

$$\Delta G = -$$

H.

94 H<sub>0</sub> = 95.1

1

$\tau = 2.0$        $h_0 = 25$

h<sub>0</sub> = 25.6

$h_r = 1.5$

1944 Abweichungen der Monatsmittel des Luftdrucks vom Mittelwert 1901–1930,  $\Delta P$

Station	$\varphi$	2	I	II	III	IV	V	VI	VII	VIII	IX	X	XI	XII	An
Dombås	62° 4'	9° 7'	-6.8	3.0	-1.8	1.7	0.8	-3.5	1.4	3.4	-1.1	-0.1	-3.5	1.7	-0.4
Oslo (Blindern)	59° 56'	10° 44'	-7.4	2.1	-2.6	2.9	0.0	-3.0	1.5	4.5	-1.1	0.5	-4.6	2.4	-0.4
Fjærø	59° 2'	10° 32'	-7.2	2.0	-2.7	3.2	-0.1	-2.9	1.0	4.7	-1.5	0.2	-5.5	2.4	-0.6
Oskey	58° 4'	8° 3'	-5.1	2.9	-1.3	3.8	0.3	-3.8	0.1	4.7	-2.0	-0.9	-6.6	2.1	-0.5
Skudenes II	59° 9'	5° 15'	-4.3	4.3	1.1	3.7	1.5	-4.8	-0.4	3.5	-2.6	-1.4	-6.6	1.6	-0.4
Ullensvang	60° 19'	6° 40'	-5.6	3.9	0.0	3.1	1.4	-4.4	0.3	3.7	-2.1	-0.7	-5.4	1.6	-0.3
Bergen (Fredriksberg)	59° 24'	5° 19'	-4.8	4.5	1.1	3.4	1.9	-4.1	0.3	4.3	-1.8	-0.6	-5.4	2.3	-0.1
Lærdal	61° 6'	7° 29'	-6.7	3.6	-0.7	2.7	1.5	-4.0	0.4	3.8	-1.8	-0.7	-4.6	1.5	-0.4
Kinn	61° 6'	4° 48'	-6.0	4.3	0.8	2.9	1.5	-3.9	0.8	3.9	-1.9	-1.1	-5.7	1.7	-0.2
Osna	62° 52'	6° 33'	-7.1	4.5	-0.1	2.2	1.9	-4.3	1.3	3.0	-1.4	-1.3	-4.6	1.6	-0.4
Trondheim (Voll)	60° 25'	10° 27'	-7.1	3.4	-1.5	2.5	2.0	-3.8	2.1	3.8	-0.6	-0.4	-2.5	1.5	0.0
Bremnesund	60° 28'	12° 12'	-9.2	1.8	-2.8	1.6	0.8	-2.9	2.3	2.5	-0.3	-1.2	-1.0	1.4	-0.6
Rest	60° 30'	12° 4'	-9.0	1.2	-2.0	2.1	0.1	-1.8	3.6	0.9	0.5	-1.7	0.5	1.4	-0.4
Tromsø	60° 39'	18° 57'	-8.8	0.3	-0.9	0.7	0.3	-0.2	4.2	-0.2	1.4	-1.0	3.3	2.3	0.1
Vadsø	60° 22'	31° 6'	-10.8	-1.3	0.6	-3.2	-0.2	1.2	3.4	-1.2	3.2				
Karasjok	69° 28'	25° 31'	-9.8	-0.4	-0.1	-1.1	0.6	1.3	4.2	-1.2	3.2				

1944 Abweichungen der Monatsmittel der Lufttemperatur vom Mittelwert 1901–1930,  $\Delta T$

Station	$\varphi$	2	I	II	III	IV	V	VI	VII	VIII	IX	X	XI	XII	An
Nord	62° 34'	11° 23'	1.7	2.5	0.8	-1.3	-2.6	-0.7	2.1	2.5	0.9	2.9	1.0	4.9	1.2
Eikerdal	61° 41'	12° 1'	0.2	2.2	-0.1	-0.8	-1.7	-1.5	1.1	2.2	1.0	2.6	1.8	5.4	1.1
Dombås	61° 41'	9° 7'	-1.7	1.3	-0.3	-1.0	-2.4	-1.2	1.0	2.1	0.5	2.1	0.1	3.7	0.6
Vinstre	59° 4'	9° 45'	-1.2	2.9	-0.6	-1.3	-1.6	-1.7	0.9	1.5	0.5	1.6	0.4	3.3	0.4
Vollen i Slidre	61° 36'	9° 45'	-1.2	2.9	0.8	-0.4	-1.0	-1.3	1.3	2.2	0.1	1.3	-1.3	4.4	0.9
Lillehammer	61° 6'	10° 29'	0.5	2.1	-0.4	-1.6	-1.5	-1.9	0.9	2.0	0.6	1.9	1.1	4.2	0.6
Yngsbygd Hedmark	60° 49'	11° 11'	1.5	2.4	-0.6	-1.7	-1.5	-2.2	0.6	1.8	-0.2	1.7	0.9	3.8	0.6
Mjøsa	60° 49'	11° 11'	1.5	2.4	-0.2	-0.7	-1.2	-1.9	1.5	2.5	0.6	-0.1	1.5	5.1	0.7
Oslo (Blindern)	60° 37'	12° 1'	1.1	1.4	-0.2	-0.7	-1.2	-1.9	0.8	2.1	0.1	2.3	1.1	3.3	1.0
Kesbyen	60° 56'	10° 44'	2.5	2.0	0.8	-0.2	-1.2	-1.5	0.6	1.9	0.4	2.0	-0.2	5.4	1.0
Dagali	60° 23'	8° 26'	2.6	0.1	0.2	-0.2	-1.2	-1.2	1.8	2.8	-0.3	0.8	-1.3	1.9	0.6
Svane	59° 46'	9° 35'	2.6	1.2	-0.6	-0.1	-0.5	-1.2	1.2	2.8	0.7	1.7	-0.1	4.2	1.1
Ås	59° 40'	10° 46'	1.8	1.3	-0.1	-0.5	-1.1	-1.5	1.1	2.6	0.1	1.6	0.6	3.2	0.7
Fjærø	59° 2'	10° 32'	3.0	1.5	0.8	0.1	-1.1	-1.3	1.0	2.5	0.3	1.4	0.2	2.1	0.9
Gvarv	59° 24'	9° 10'	0.7	0.7	-0.1	-0.5	-0.4	-1.0	0.8	2.2	0.9	1.9	0.2	3.2	0.6
Dalen i Telemark	59° 27'	8° 0'	2.9	2.0	0.2	-0.3	-0.8	-1.6	0.2	2.7	0.3	1.3	-0.1	2.6	0.8
Lynge	58° 58'	9° 7'	2.9	1.5	0.6	0.1	-0.3	-0.9	0.8	1.9	0.0	1.1	0.0	2.1	0.8
Ryfylkefjord	58° 40'	7° 48'	1.5	0.4	-0.2	-0.5	-0.4	-1.2	0.3	2.3	0.2	0.8	-0.5	1.5	0.3
Oskey	58° 4'	8° 3'	2.6	1.0	0.2	-0.2	-0.6	-0.7	0.9	2.1	0.6	1.2	-0.3	1.3	0.7
Lister	58° 6'	6° 34'	2.6	0.5	0.4	0.0	-0.9	-0.5	1.2	1.8	0.1	0.6	-0.1	0.7	0.6
Tonstad	58° 40'	6° 43'	1.2	-0.6	-0.4	0.1	-0.3	-1.0	1.3	2.2	0.2	1.5	-0.4	1.3	0.5
Klepp	58° 48'	5° 38'	1.8	-0.2	-0.4	0.5	-0.3	-0.3	1.6	1.8	0.3	0.9	-0.5	0.8	0.5
Sauda	59° 39'	6° 22'	1.4	-0.2	-1.1	0.0	-1.0	-0.5	1.4	2.2	0.4	1.4	-0.1	1.5	0.5
Skudenes II	59° 9'	5° 15'	1.7	0.0	-0.2	0.5	-0.4	-0.3	1.5	1.1	0.2	0.8	-0.7	0.3	0.4
Ullensvang	60° 19'	6° 40'	1.3	0.0	-0.9	-0.3	-1.2	-1.4	0.7	1.5	-0.4	0.9	-0.3	1.3	0.1
Silird	60° 37'	7° 25'	1.1	-0.8	-1.0	-0.5	-2.1	-1.4	1.1	2.1	-0.7	0.5	-1.6	0.9	-0.2
Bergen (Fredriksberg)	60° 24'	5° 19'	1.8	0.2	-0.5	0.3	-0.6	-0.3	1.8	1.1	0.5	1.5	0.3	0.9	0.5
Lærdal	61° 6'	7° 29'	1.5	-0.7	-1.7	-1.2	-1.7	-0.7	0.7	0.7	0.1	2.0	0.0	2.1	0.1
Kinn	61° 34'	4° 48'	1.7	0.8	0.0	-0.3	-1.4	-0.6	0.8	0.0	0.5	1.7	0.4	1.2	0.0
Opstryn	61° 56'	7° 13'	1.0	-0.7	-2.3	-1.6	-3.1	-1.4	1.2	1.5	0.9	2.6	0.2	1.7	0.0
Osna	62° 52'	6° 33'	0.8	0.2	-0.6	-0.6	-0.1	0.5	-0.2	-0.1	-0.3	1.5	-0.1	0.6	0.0
Sundal	62° 53'	9° 7'	1.2	0.1	-1.2	-1.7	-3.1	-0.5	0.9	0.8	0.2	2.2	0.1	2.4	0.1
Sula Pyr	62° 51'	8° 28'	1.4	1.1	0.1	-0.6	-0.8	0.8	0.6	0.2	0.3	1.6	0.1	1.3	0.5
Trondheim (Voll)	62° 50'	10° 27'	2.3	1.7	-0.1	-1.9	-1.9	-0.1	1.3	0.4	1.0	2.8	0.5	3.5	0.8
Sulstua	62° 40'	12° 1'	2.3	2.5	0.1	-0.9	-2.7	-0.5	1.6	0.7	0.7	2.9	0.5	4.1	1.0
Hordaland	62° 28'	13° 36'	0.8	2.8	-0.2	-1.6	-2.8	-1.6	0.9	0.2	0.1	2.2	0.2	4.2	0.4
Bremnesund	62° 48'	10° 33'	1.3	1.4	0.0	-1.0	-1.2	0.4	-0.4	-0.6	0.1	2.0	0.3	2.1	0.3
Myken	62° 46'	12° 29'	1.2	1.8	-0.4	-1.1	-1.3	0.8	0.1	-0.8	-0.1	2.3	1.1	2.6	0.6
Bods	62° 17'	14° 26'	0.3	2.2	-0.1	-2.1	-1.2	0.5	0.2	-0.8	1.1	3.0	1.0	3.5	0.7
Offørsey	62° 20'	15° 38'	0.4	2.2	0.2	-1.4	-0.7	1.0	0.6	-1.3	0.8	2.9	1.1	3.2	0.8
Skravør Pyr	62° 25'	11° 53'	0.5	1.5	-0.3	-0.9	-0.3	0.8	-0.3	-0.9	-0.2	1.9	1.0	1.8	0.4
Eggen	62° 18'	13° 41'	0.9	2.7	0.0	-1.6	-0.4	0.9	-0.3	-1.1	0.8	3.0	1.3	3.1	0.8
Andenes	62° 19'	16° 7'	0.9	2.6	0.3	-1.5	-0.4	0.6	0.1	-0.6	1.0	2.8	1.3	3.0	0.8
Tromsø	62° 39'	18° 57'	0.9	3.0	0.6	-1.2	-0.2	1.1	-0.1	-1.0	1.5	3.6	1.6	3.3	1.1
Dividalen	62° 47'	19° 44'	2.8	4.8	0.9	-1.1	-0.4	-0.1	-0.4	0.0	0.5	4.8	2.9	5.7	1.8
Alta (Elvebakken)	62° 58'	23° 22'	2.0	3.8	0.4	-1.1	-0.2	0.8	0.1	-0.2	1.1	1.1	7.7	5.2	9.5
Galten	62° 45'	22° 44'	1.6	2.1	0.8	-0.4	-0.4	0.4	-0.9	-1.3	1.5	3.1			
Ingsøy	62° 43'	24° 9'	1.7	3.9	1.0	-1.7	-0.1	0.1	-0.1	-1.7	1.5	3.1			
Kistrand	62° 40'	23° 13'	2.1	2.3	0.7	-1.3	-0.2	-0.3	-1.8	-1.2	0.9	1.4			
Sletnes Pyr	62° 51'	28° 14'	2.1	1.9	0.6	-0.8	0.6	0.8	-1.6	-0.3	1.3				
Tana	62° 27'	28° 16'	1.8	3.9	1.0	-1.7	-0.1	0.1	-0.1	-1.7	1.5				
Vadsø	62° 22'	31° 6'	1.7	1.7	1.6	-1.1	-0.2	0.1	-1.7	-0.3	1.3				
Karbjukt	62° 40'	30° 29'	1.3	3.5	0.9	-1.9	-0.5	0.3	2.5	-0.6	0.8				
Karasjok	62° 28'	25° 31'	1.2	4.1	1.3	-2.3	-0.4	0.0	-0.6	-0.4	0.8				
Sivertsværfjord	62° 45'	23° 33'	1.2	4.1	1.0	-2.4	-0.4	-0.4	-0.3	0.7	0.7				

1944 See-Temperatur  $T_s$

Station	$\varphi$	2	I	II	III	IV	V	VI	VII	VIII	IX	X	XI	XII	An





<tbl\_r cells="

# Extenso-Tabelle

1944

**Oslo (Blindern)**

$\phi = 59^{\circ} 56' N$   $l = 10^{\circ} 44' E$

$g = 9.819$

$\Delta G = +1^{\circ}$

**Januar I**

$H_a = 94$   $H_b = 95.6$

$h_a = 2.0$   $h_b = 25.2$   $h_d = 25.6$   $h_r = 1.5$

Datum	Luftdruck P			Lufttemperatur T						Relative Feuchte U			Richtung und Stärke des Windes D,F			>	Bewölkung und Wetter N,w			Niederschlag R	Schnellhöhe H <sub>s</sub>	Witterungsverlauf W			
	8	14	19	8	14	19	Max	Min	8	14	19	8	14	19	14	8	14	19							
1	76.8	73.7	79.8	-2.2	0.8	-1.2	3.1	-5.7	95	68	63	22	1	22	1	32	1	4	7	3	3	2.1	5	* = n, o = n, - = n, - = n, - = n, p (-) = - n, - = n, - = n, - = n, - = n, p	
2	85.5	77.5	72.5	-5.0	-2.0	-2.2	0.2	-5.8	81	89	95	02	1	32	1	00	0	4	8	10	10	0.0	5	* = n, - = n, - = n, - = n, - = n, p	
3	73.6	77.0	79.2	-4.5	-0.6	-2.5	0.1	-5.9	77	49	54	24	1	26	1	03	1	6	6	1	10	10	0.0	5	* = n, - = n, - = n, p
4	96.4	90.0	03.1	-7.4	-4.9	-3.1	-2.1	-9.5	64	62	58	04	2	30	0	32	2	5	0	10	10	2	5	* = n, - = n, - = n, - = n, - = n, p	
5	10.9	06.8	99.5	-5.8	-4.7	-0.3	-0.3	-7.4	68	77	96	03	0	30	0	18	2	4	10	10	10	10	5	* = n, - = n, - = n, - = n, - = n, p	
6	76.2	77.6	78.2	4.6	5.6	3.6	6.7	-u.4	86	50	46	18	2	24	2	24	4	9	7	1	1	0	0.0	2	* = n, - = n, o = a, - = o p
7	81.1	87.2	92.2	1.2	2.0	-2.5	3.8	-2.9	51	58	65	25	2	30	1	20	1	6	10	10	10	5	2	* = n, - = n, o = a, - = o p	
8	91.4	84.4	76.9	-5.7	-3.1	-2.5	-2.1	-7.3	73	72	98	14	1	30	0	32	1	4	10	10	10	5	2	* = n, - = n, a, - = p	
9	74.8	76.1	79.3	-8.8	-7.2	-10.7	-2.5	-11.9	84	73	86	02	2	02	1	00	0	6	10	8	4	4	4.9	9	* = n, - = n, - = o a, - = o o p
10	85.9	89.6	93.0	-13.1	-11.0	-14.8	-9.1	-16.4	84	80	89	02	1	30	0	02	1	4	1	0	0	1	8	* = n, - = o a, p	
11	97.4	99.7	02.4	-15.0	0.6	-5.0	1.1	-17.6	95	49	68	31	1	32	2	02	1	8	10	1	1	1	8	* = n, - = o a, - = o p	
12	06.8	08.4	09.6	-9.7	-8.2	-11.1	-4.7	-12.0	82	81	86	08	1	38	1	00	0	3	1	9	10	1	8	8	* = n, - = n, - = o a, p
13	09.8	07.1	01.8	-7.4	-4.3	-0.6	-0.6	-13.1	95	97	98	16	1	33	1	13	2	3	10	10	10	10	1.7	9	* = n, - = n, - = o a, - = o o p
14	90.0	95.1	02.0	-1.1	-0.9	0.7	0.7	-4.2	97	94	86	00	0	34	1	24	2	3	9	10	4	4	13.0	20	* = n, - = n, - = o a, - = o o p
15	10.0	14.2	16.0	-3.3	-0.5	-1.8	1.1	-4.4	97	96	98	32	1	33	1	06	1	4	9	10	6	1	20	* = n, - = n, - = (E) a, p, - = 19	
16	19.2	19.8	18.7	-1.6	0.0	-2.4	0.7	-3.4	91	90	94	03	2	00	0	03	0	4	7	6	6	4	20	* = n, - = n, - = n, - = o a, - = o o p	
17	16.8	14.4	10.2	-4.6	-2.1	0.0	0.9	-5.6	97	99	94	14	1	00	0	00	0	2	10	10	10	10	20	* = n, - = n, - = n, - = o a, p	
18	07.2	07.4	06.0	-1.7	-1.4	-1.3	0.5	-1.7	99	98	98	00	0	00	0	00	0	1	10	10	10	10	19	* = n, - = n, p	
19	03.9	04.6	05.6	1.8	2.4	1.3	2.6	-2.5	99	99	99	00	0	00	0	00	0	1	10	10	10	10	18	* = n, - = n, a, p	
20	06.5	05.8	04.1	-5.0	-5.1	-7.0	2.6	-7.4	96	98	95	00	0	06	1	00	0	0	10	10	10	10	15	* = n, - = n, a, p, V 19	
21	90.8	88.0	88.8	-2.2	0.6	-2.8	1.4	-7.5	90	98	98	04	1	00	0	22	1	4	10	10	0	0	2.5	16	* = n, - = n, - = n, - = n, - = n, p
22	83.1	72.4	72.0	-0.4	3.8	2.8	4.4	-4.5	97	95	91	01	1	16	1	26	1	4	10	10	2	1	0.1	14	* = n, - = n, - = n, - = o a, - = o o p
23	68.6	58.7	57.3	1.3	2.5	1.1	3.1	-0.4	96	94	96	00	0	00	0	28	3	1	4	10	10	1	1.4	12	* = n, - = n, - = n, a, p
24	68.2	81.5	85.2	1.9	2.2	-3.4	3.0	-3.4	62	48	63	30	5	16	2	32	1	8	9	10	10	10	15.6	10	* = n, - = n, - = n, - = o a, p
25	77.1	72.1	70.3	-2.8	-3.6	-3.0	-2.1	-7.9	65	85	88	10	3	02	4	04	6	4	10	10	10	10	10	* = n, - = n, - = n, - = n, - = n, p	
26	81.1	88.7	93.9	-1.4	-0.4	-1.4	1.9	-3.2	81	67	75	02	4	02	1	03	1	8	10	9	0	0	3.9	12	* = n, - = n, - = o a, - = o o p
27	86.5	79.0	75.1	-1.7	3.0	1.0	3.1	-6.0	98	94	97	23	1	17	2	24	1	5	10	10	2	1	0.3	12	* = n, - = n, - = n, - = o a, - = n, - = o o p
28	80.4	87.8	95.2	0.4	6.7	2.0	6.9	-0.2	88	47	48	24	1	28	4	28	2	9	3	10	10	10	0.2	10	* = n, - = n, - = o a, - = o o p
29	01.5	97.7	91.8	-3.0	1.4	0.3	3.0	-4.4	81	81	96	06	1	00	0	04	2	4	9	10	10	10	8	* = n, - = n, - = n, - = o a, p	
30	95.1	95.6	98.4	6.1	9.6	3.4	9.9	-0.6	58	46	59	26	2	20	1	20	1	6	4	4	4	4	8	* = n, - = n, - = o a, (-) = o o p	
31	04.6	00.2	95.5	-1.0	1.5	1.1	3.9	-1.4	84	82	98	00	0	00	0	00	0	5	10	10	10	10	0.6	9	* = n, - = n, - = o a, - = o p
M	92.0	91.9	92.0	-3.1	-0.6	-2.0	1.3	-6.0	84	78	83	1.3	1	00	1	1.2	1.2	4.6	8.1	7.3	5.4	47	10		

**Februar II**

1	95.1	90.7	83.7	-2.4	3.0	3.2	3.4	-3.5	97	86	98	00	0	00	0	16	1	4	10	10	10	10	2.0	12	* = n, a, - = o p		
2	82.9	85.7	86.3	2.1	7.2	0.8	7.2	-0.5	91	43	68	00	1	06	1	04	1	8	10	3	3	1	1.1	7	* = n, - = n, - = o p		
3	75.2	71.2	68.4	-0.5	0.4	0.0	1.0	-1.5	98	99	99	18	1	00	0	00	0	2	10	10	10	10	7	* = n, - = n, - = o p			
4	88.2	74.7	83.2	-0.6	2.2	-1.7	2.6	-1.5	98	88	76	14	1	32	4	32	1	6	10	10	7	10	1.8	13	* = n, - = n, - = o p		
5	97.5	92.6	06.6	1.6	1.4	-1.4	2.7	-1.5	55	43	46	32	3	31	4	32	3	9	7	10	0	1	0.7	10	* = n, - = n, - = o p		
6	12.2	09.0	04.7	-8.0	-3.0	-3.6	-1.0	-8.7	68	68	71	32	1	00	0	00	0	5	8	10	10	10	10	4.9	10	* = n, - = o a, - = o p	
7	87.0	75.9	71.2	2.8	4.4	3.5	5.2	-4.6	98	98	68	17	2	16	3	17	3	5	10	10	10	10	2.1	21	* = n, - = n, - = o a, - = o p		
8	69.4	79.6	84.1	1.4	3.7	-0.3	6.0	-0.5	68	44	46	27	2	32	4	30	2	9	9	10	10	6	5	5	5	* = n, - = n, - = o a, - = o p	
9	85.8	83.6	82.8	-4.6	2.0	-1.9	2.7	-5.6	64	51	53	04	1	31	1	01	2	9	10	7	10	1	5	5	5	* = n, - = n, - = o a, - = o p	
10	88.5	95.4	97.2	-3.0	2.2	1.4	2.9	-3.5	60	55	58	32	4	01	3	02	3	9	6	8	8	1	5	5	5	* = n, - = n, - = o a, - = o p	
11	01.2	01.6	02.3	1.8	3.0	0.9	3.6	-0.6	58	58	71	31	3	32	3	03	2	9	10	10	10	10	5	5	5	5	* = n, - = n, - = o a, - = o p
12	11.9	13.8	15.5	-6.2	-0.6	-4.8	2.0	-6.5	76	75	86	00	0	00	0	11	1	04	2	6	3	1	1	1.1	7	* = n, - = n, - = o a, - = o p	
13	18.9	18.2	16.7	-8.9	-2.2	-3.4	-1.5	-10.1	97	81	81	00	0	00	0	12	1	04	2	6	9	8	10</				

# Extenso-Tabelle

1944

**Oslo (Blindern)**

$\varphi = 59^{\circ} 56' N$

$\lambda = 10^{\circ} 44' E$

$g = 9.819$

$\Delta G = +1^{\circ}$

**März III**

$H_s = 94$

$H_b = 95.6$

$h_t = 2.0$

$h_a = 25.2$

$h_d = 25.6$

$h_r = 1.5$

Datum	Luftdruck P			Lufttemperatur T						Relative Feuchte U		Richtung und Stärke des Windes D,F			Sicht V			Bewölkung und Wetter N,w			Niederschlag R	Schneehöhe E	Witterungsverlauf W		
	8	14	19	8	14	19	Max	Min	8	14	19	8	14	19	14	8	14	19							
1	71.5	70.1	71.1	-1.7	-0.9	-2.8	2.8	-3.0	99	94	94	16	3	28	2	22	1	5	10	-	10	3	0.1	5	-
2	72.5	72.1	73.0	-7.2	1.7	-1.1	2.4	-8.4	85	59	90	00	0	18	1	19	2	8	7	-	1	3	1.4	9	-
3	74.9	76.8	79.5	-3.5	-0.4	-2.0	2.1	-4.4	98	76	68	00	0	00	0	26	1	5	10	-	10	5	0.2	9	-
4	87.5	92.8	96.1	-3.4	2.0	-1.3	2.9	-4.3	62	41	43	00	0	00	0	28	1	8	10	-	10	4	0.0	8	-
5	07.5	09.8	12.3	-7.7	2.8	-1.5	3.1	-8.5	65	47	59	00	0	00	0	00	0	9	8	-	8	3	0.0	8	-
6	18.6	21.0	23.6	-6.4	4.0	0.0	4.0	-7.9	93	62	72	06	1	19	1	03	2	4	9	1	8	1	1	7	-
7	28.1	28.8	28.1	-5.0	0.8	-1.6	3.0	-5.5	00	84	84	04	1	19	1	03	2	3	10	1	9	1	0	7	-
8	27.8	26.3	24.1	-6.0	5.5	1.2	6.9	-6.6	91	54	68	00	0	00	0	03	1	4	10	1	9	1	0	6	-
9	17.6	12.7	07.3	-0.6	5.0	1.9	5.4	-1.2	88	56	86	03	1	21	1	18	2	5	10	1	10	10	0.3	5	-
10	97.7	95.5	88.7	-1.2	7.6	4.8	8.0	-1.6	00	43	51	00	0	24	2	22	2	9	10	1	9	8	0.3	5	-
11	76.5	78.7	85.2	-1.4	4.8	4.9	5.6	-0.9	55	47	54	08	1	02	5	01	5	9	9	1	4	1	5	4	-
12	87.7	80.7	79.4	-1.3	2.4	1.0	5.0	-1.8	78	72	78	04	1	20	1	00	0	9	10	1	10	9	0.0	0	-
13	67.6	70.6	70.6	-2.0	-1.4	0.9	1.7	-3.6	85	84	57	03	2	02	4	04	2	8	9	1	9	9	0.0	0	-
14	79.5	81.0	84.0	-0.8	3.4	0.5	4.9	-2.5	57	48	50	02	2	02	3	02	2	9	3	1	3	2	0.0	0	-
15	91.7	94.4	96.9	-2.0	4.6	0.9	5.8	-4.4	67	37	46	16	1	32	2	08	1	9	0	1	3	2	0.0	0	-
16	00.1	00.8	01.8	-2.1	1.5	-0.9	3.9	-6.3	66	63	70	07	1	12	2	03	1	8	10	1	4	1	3	0	-
17	04.0	04.2	05.5	-5.0	1.8	1.6	2.7	-7.5	87	79	85	00	0	00	0	00	0	9	10	1	10	10	0.0	0	-
18	99.3	95.8	97.0	-0.5	5.4	5.3	0.9	-0.9	00	71	56	00	0	00	0	00	0	9	10	1	8	7	0.0	0	-
19	83.2	79.8	81.8	0.4	5.9	3.2	6.4	0.0	97	56	42	00	0	26	2	28	3	9	10	1	4	1	6.3	6	-
20	88.2	89.2	89.2	0.7	4.2	2.0	4.9	-0.5	46	36	40	30	3	32	5	32	2	9	1	1	2	4	0.0	0	-
21	95.8	97.1	99.9	-1.7	2.4	0.0	2.4	-3.0	48	40	45	32	5	02	6	02	3	9	0	1	5	1	1	0	-
22	03.7	03.4	03.9	-2.6	1.8	0.1	2.0	-4.6	60	43	48	02	3	07	2	00	0	9	1	1	7	10	0.0	0	-
23	98.8	94.2	94.6	-1.5	3.4	4.6	5.9	-3.0	72	62	62	19	1	19	2	03	4	9	10	1	10	9	0.0	0	-
24	05.3	10.6	14.5	-1.2	3.2	0.6	4.9	-1.1	53	47	49	02	2	04	3	32	1	9	9	1	4	1	1	0	-
25	16.6	15.0	12.4	-3.0	0.4	0.2	0.9	-5.6	69	92	94	00	0	00	0	00	0	3	10	1	10	10	0.0	0	-
26	09.4	09.9	12.4	-1.1	6.5	3.8	8.1	-2.1	89	62	72	00	0	16	1	09	1	5	10	1	2	9	1.2	1	-
27	15.8	12.7	08.7	-0.8	1.4	1.8	4.1	-1.0	92	91	90	15	2	16	1	17	1	5	10	1	10	10	0.1	0	-
28	97.6	94.0	93.8	-2.7	6.0	2.4	6.7	-0.5	74	43	66	02	1	04	2	06	2	8	9	1	9	9	0.0	0	-
29	97.6	96.3	95.2	-3.6	-0.4	-1.5	2.7	-4.9	70	55	69	02	2	00	0	08	2	8	8	1	10	9	0.1	0	-
30	95.3	94.3	93.6	-3.9	-1.4	-2.1	-0.6	-5.9	68	56	64	16	2	16	2	14	2	8	10	1	10	10	1.5	3	-
31	95.5	96.2	97.6	-3.9	0.6	-0.3	1.9	-8.5	64	50	53	02	1	00	0	10	1	8	1	1	4	10	0.0	0	-
M	97.2	96.8	97.3	-2.2	2.7	0.9	4.2	-3.8	77	60	65	1.2		1.6	1.5	7.1	7.8	6.9	6.1	11	3				

# April IV

1	04.0	05.0	06.1	-4.4	1.6	-0.2	3.1	-7.7	74	46	46	30	0	19	1	00	0	8	0	-	1	2	0	0	-	
2	09.2	08.2	08.1	-4.8	4.4	2.4	5.9	-8.2	87	55	54	00	1	20	0	05	1	7	10	-	2	8	0	0	-	
3	09.3	08.8	08.0	-1.9	4.1	3.3	5.3	-3.7	95	55	50	08	1	20	0	05	1	8	0	-	9	8	0	0	-	
4	09.2	08.2	07.2	-0.8	2.4	1.8	3.5	-3.0	62	58	58	03	2	11	2	04	1	8	0	-	9	8	0	0	-	
5	05.7	04.6	05.1	0.0	3.3	2.2	4.2	-0.6	65	53	51	05	2	06	1	01	1	7	10	-	8	7	0	0	-	
6	10.0	10.4	10.0	0.3	5.4	4.6	6.8	-2.6	57	46	41	05	1	18	1	00	0	9	0	-	1	4	0	0	-	
7	08.9	07.4	07.1	-0.4	8.9	8.3	10.8	-3.7	87	51	48	00	2	20	2	24	2	8	8	-	4	1	7	0	-	
8	11.3	10.1	08.1	3.2	6.8	4.0	8.6	-1.2	66	63	74	04	2	20	1	16	2	8	10	-	10	1	0	0	-	
9	04.4	04.2	03.6	2.1	6.2	5.6	7.1	-0.9	86	66	72	00	0	18	1	00	0	5	10	-	10	10	0	0	-	
10	04.2	02.8	00.9	2.2	10.9	9.8	12.6	-0.7	87	49	43	30	0	16	1	00	0	8	10	-	3	4	0	0	-	
11	97.6	95.6	94.2	2.4	4.4	3.8	10.2	0.7	84	98	00	00	0	00	20	1	02	1	2	12	-	10	10	0.3	0	-
12	98.7	93.0	94.2	3.9	4.1	3.2	4.2	0.8	88	78	75	03	2	08	1	02	1	8	10	-	10	10	2.1	0	-	
13	07.6	07.7	06.8	1.1	4.8	5.9	7.7	-0.6	78	68	62	18	1	17	1	17	1	8	10	-	9	9	0.0	0	-	
14	05.2	04.1	03.0	2.6	6.0	5.8	6.9	-0.3	86	77	84	21	2	16	2	16	2	5	10	-	10	10	0.0	0	-	
15	99.6	96.0	94.4	2.4	6.7	5.5	7.0	-1.5	98	78	83	00	0	00	0	00	0	6	10	-	10	10	0.0	0	-	
16	92.0	90.7	90.0	5.1	7.7	6.4	7.9																			

# Extenso-Tabelle

1944

**Oslo (Blindern)**

$\varphi = 59^{\circ} 56' N$

$\lambda = 10^{\circ} 44' E$

$g = 9.819$

$\Delta G = +1^h$

**MaI V**

$H_a = 94$

$H_b = 95.6$

$h_a = 2.0$

$h_b = 25.2$

$h_d = 25.6$

$h_r = 1.5$

Datum	Luftdruck P			Lufttemperatur T						Relative Feuchte U			Richtung und Stärke des Windes D,F			Bewölkung und Wetter N,w			Niederschlag R	Schneehöhe E	Witterungsverlauf W		
	8	14	19	8	14	19	Max	Min	8	14	19	8	14	19	8	14	19						
1	95.0	91.2	92.2	5.0	14.6	10.5	15.2	4.4	99	57	40	00	0	16	2	26	3	8	10	9 -	8 -	0.6	
2	88.3	80.1	76.2	2.6	3.2	4.2	10.8	1.1	85	96	95	16	1	05	1	04	1	5	10	10 -	10 -	0.2	
3	71.7	74.1	79.3	3.6	2.9	3.1	4.8	2.5	92	93	89	04	2	02	4	02	4	6	10	10 -	10 -	5.1	
4	90.2	91.9	92.4	3.3	6.1	5.0	6.6	1.0	55	45	42	03	4	02	3	32	2	10	9	9 -	8 -	6.4	
5	95.6	93.3	94.8	2.4	4.8	3.6	5.2	-1.1	51	53	53	04	2	04	4	04	3	9	4	10	10 -	9 -	
6	03.5	06.1	09.0	3.9	7.8	7.9	9.3	-0.8	48	33	29	04	2	32	4	02	2	10	3	2	1	-	
7	16.6	15.7	15.1	5.8	11.7	12.1	13.5	-1.6	55	29	23	16	1	15	1	00	0	9	0	1	1	0	
8	17.6	15.5	13.8	7.0	15.4	13.8	16.2	-0.5	55	25	29	00	0	10	1	22	1	9	2	3	3	9 -	
9	13.6	10.7	09.6	8.5	16.1	12.8	17.4	0.9	60	22	33	02	1	16	1	00	0	8	5	7	9 -		
10	05.4	02.6	01.4	7.0	14.8	14.2	15.7	4.5	91	54	57	16	1	16	2	18	1	7	10	10 -	9 -		
11	02.0	01.8	03.6	10.0	17.8	14.8	18.5	3.0	64	47	45	16	1	16	2	26	1	9	8	7	9 -	0.0	
12	08.0	08.2	09.4	11.8	18.7	12.1	19.0	3.5	61	52	78	14	1	16	3	20	2	9	0	1	1	10	
13	08.9	06.6	04.1	8.7	16.2	15.5	17.8	5.7	97	61	56	00	0	16	2	16	2	7	10	7	9 -		
14	00.9	99.6	00.0	12.4	15.1	6.0	16.7	6.0	78	61	88	12	1	29	2	32	1	8	10	10	10 -		
15	02.2	05.6	00.1	5.8	7.7	6.6	8.7	4.4	84	81	91	04	3	04	4	04	7	9	10	10 -	10 -	2.5	
16	11.4	12.9	13.2	5.9	8.2	8.1	8.8	5.5	00	85	88	00	0	04	2	04	2	9	10	10 -	10 -	21.4	
17	14.4	13.3	11.9	7.2	10.8	13.2	15.2	6.3	87	78	72	03	2	02	2	02	1	9	10	10 -	10 -	1.4	
18	12.1	09.5	07.9	12.6	18.5	17.4	18.9	10.3	59	38	46	02	2	02	2	03	1	10	6	6	5	0.1	
19	06.4	01.7	98.0	14.6	18.5	17.9	19.8	9.6	56	47	47	16	1	20	1	16	1	9	4	4	2		
20	03.0	01.5	00.3	8.0	10.8	9.3	17.9	4.8	52	43	42	01	4	01	3	02	2	10	5	6	2		
21	93.9	90.9	89.2	4.8	8.2	5.0	9.8	2.6	65	71	86	02	2	06	2	27	1	9	10	7	9 -	0.0	
22	92.2	94.6	97.6	6.5	9.3	9.6	10.4	3.2	63	41	47	32	4	07	5	04	2	9	8	9	9 -	0.8	
23	00.9	00.1	00.0	7.6	10.9	9.2	11.6	3.5	53	33	36	32	4	32	5	32	2	9	7	8	8 -	0.0	
24	93.9	94.6	96.7	5.8	9.4	9.8	11.2	1.4	63	48	50	24	1	24	1	32	3	8	10	9	10 -	0.0	
25	97.8	94.7	93.2	7.6	11.5	8.0	11.9	1.0	48	37	49	28	1	16	2	16	2	9	1	10	10 -		
26	98.6	00.8	03.9	8.3	15.7	14.7	16.5	4.8	70	48	62	00	0	20	2	16	1	9	10	8	7		
27	09.5	10.8	12.0	10.0	11.1	13.0	15.1	5.6	78	97	91	00	0	17	2	00	0	4	10	10 -	10 -	0.0	
28	18.9	19.0	14.3	14.3	18.3	16.1	19.5	8.0	53	40	53	26	2	16	2	19	1	9	3	9	9 -	0.4	
29	16.7	14.3	12.1	11.0	15.6	16.1	17.4	9.6	91	81	77	00	0	00	0	00	0	6	10	10 -	10 -	0.4	
30	10.8	07.4	04.9	14.5	17.6	15.7	18.6	10.5	66	46	57	02	3	02	1	30	2	9	6	9	8 +	1.7	
31	06.7	04.5	03.5	11.7	15.3	13.1	15.9	7.8	58	43	48	30	1	32	2	02	2	10	8	6	4 -	0.8	
M	03.4	02.3	02.0	8.0	12.3	10.9	13.9	4.2	69	54	57	1.5		2.4	1.7	8.4	7.0	7.6	7.7	42			

**Juni VI**

	04.8	05.2	01.0	6.8	12.0	12.8	14.6	6.4	74	60	57	03	2	16	1	05	2	10	10	10	5 -	0.1
1	00.1	99.0	98.0	11.6	10.9	10.4	14.5	7.4	65	91	91	07	1	24	1	16	1	10	7	10	10 -	0.1
2	97.9	98.3	98.3	8.3	9.5	10.5	11.1	7.4	86	78	76	00	0	16	1	15	1	9	10	10 -	7 -	10.3
3	00.0	99.9	98.6	9.8	10.4	8.2	12.3	7.7	88	80	89	00	0	17	2	04	2	9	10	10 -	10 -	0.1
4	90.8	90.9	91.4	10.0	14.3	12.4	14.8	7.8	96	71	69	08	1	15	2	15	2	8	10	9	7 -	20.6
5	95.4	93.9	94.7	10.5	14.1	12.6	14.9	9.2	88	69	76	02	2	04	2	04	3	7	10	10 -	10 -	3.7
6	94.3	96.5	95.7	10.4	12.4	12.1	15.6	9.4	92	87	91	04	2	03	3	02	2	7	10	10 -	10 -	8.4
7	92.2	91.9	90.6	11.3	12.8	12.9	15.8	11.2	95	89	88	08	1	16	1	16	2	1	6	10	9 -	5.5
8	88.9	86.1	83.9	11.3	17.8	16.0	18.8	5.5	79	52	52	10	0	24	1	00	0	8	1	6 -	8 -	4.1
9	80.2	83.4	85.9	10.0	10.8	8.8	16.4	8.8	92	83	85	00	0	32	2	03	3	7	10	10 -	10 -	2.5
10	90.3	90.8	91.0	7.4	14.3	12.6	15.6	6.2	77	58	72	05	3	16	2	16	3	10	9	4	8 -	1.1
11	91.2	90.8	91.5	10.1	9.8	10.4	12.8	9.5	92	94	96	16	2	09	1	00	0	5	10	10 -	9 -	0.4
12	98.0	97.9	97.8	15.0	17.0	13.6	17.5	9.2	67	55	61	18	2	15	5	15	2	9	3	8(?)	7 -	11.1
13	85.0	89.2	90.4	9.5	9.2	12.6	13.8	7.4	92	89	77	03	3	20	2	19	1	10	10	10 -	9 +	18.7
14	92.2	92.0	93.1	12.2	16.4	12.9	16.4	9.5	77	62	84	17	1	18	1	00	0	9	7	9(?)	7 -	6.1
15	94.7	95.7	98.2	14.0	17.0	13.4	17.3	7.2	63	52	58	16	1	15	2	15	2	10	9	7 -	0.8	
16	06.3	06.7	07.7	12.7	17.8	16.1	19.3	8.9	67	53	57	03	3	02	3	02	1	9	9	9 -	7 -	
17	10.3	09.1	09.0	16.1	21.6	19.5	22.8	8.4	60	37	46	18	1	16	2	16	2	9	0	3 -	2 -	0.0
18	11.7	10.6	09.8	17.6	23.8	21.6	24.7	8.4	60	36	38	00	0	16	2	15	2	9	0	1	1 -	
19	09.6	07.3	05.5	16.7	22.0	18.1	22.5	9.9	77	49	60	16	1	16	2	16	2</					

# Extenso-Tabelle

1944

**Oslo (Blindern)**

$\varphi = 59^{\circ} 56' N$   $l = 10^{\circ} 44' E$   $g = 9.819$   $\Delta G = +1^{\circ}$

**Juli VII**

$H_0 = 94$

$H_0 = 95.6$

$h_0 = 2.0$

$h_0 = 25.2$

$h_0 = 25.6$

$h_0 = 1.5$

Datum	Luftdruck P			Lufttemperatur T						Relative Feuchte U			Richtung und Stärke des Windes D,F			> Sonne	Bewölkung und Wetter N,w			Niederschlag R	Schnellhöhe E	Witterungsverlauf W	
	8	14	19	8	14	19	Max	Min	8	14	19	8	14	19	14	8	14	19					
1	03.2	03.2	03.2	16.0	18.0	16.0	19.9	13.4	81	86	85	01	1	01	1	01	1	7	10	9	10	0.1	
2	05.3	06.4	06.0	15.0	17.5	17.2	19.8	14.8	95	79	78	16	1	19	1	19	1	9	10	10	9	17.1	
3	07.0	05.8	04.6	15.0	21.8	21.0	22.6	13.1	90	65	65	00	0	19	1	19	1	8	10	3	4	0.1	
4	03.6	01.6	09.9	20.0	25.4	24.4	26.8	16.0	69	53	50	00	0	18	1	18	1	9	6	7	3	0.1	
5	00.6	00.2	09.4	20.8	27.2	24.9	27.9	13.1	68	49	52	00	0	20	1	15	1	9	1	2	1	1	
6	02.6	02.1	02.4	20.6	27.3	23.4	27.3	13.6	72	55	70	20	1	16	3	15	2	8	0	1	5	1	
7	04.7	03.3	02.5	17.8	25.8	23.8	27.0	15.0	93	65	63	00	0	18	1	15	2	7	10	1	0	0.1	
8	05.1	01.9	00.6	19.9	26.0	25.2	28.0	12.9	74	52	50	17	1	15	2	16	2	6	1	3	5	1	
9	97.9	94.2	90.9	22.4	29.3	27.4	30.6	16.0	73	55	55	00	0	18	1	00	0	7	3	7	9	1	
10	87.4	87.3	87.6	19.0	20.4	20.0	27.4	18.2	95	81	84	15	2	15	2	15	3	7	10	0	9	12.2	
11	87.9	88.8	89.4	17.4	19.8	17.7	20.8	14.6	66	57	61	19	2	16	3	17	3	9	1	4	1	0.9	
12	87.9	87.2	88.1	16.0	13.8	15.1	18.9	12.4	85	91	85	15	2	00	0	32	1	8	10	10	5	0.1	
13	92.6	91.2	90.4	14.0	15.8	15.8	19.3	11.4	76	75	65	04	2	31	2	15	1	9	6	7	8	9.6	
14	92.4	93.4	94.4	13.6	18.5	16.3	19.7	11.5	91	58	65	00	0	22	1	18	2	10	10	10	10	7.5	
15	97.3	98.3	98.6	15.8	17.4	15.7	19.4	13.4	86	74	88	16	2	18	3	15	3	10	10	10	10	0.0	
16	00.3	00.7	01.6	15.2	20.4	19.6	22.4	11.9	83	69	70	05	1	00	0	18	1	9	9	8	7	0.5	
17	06.5	06.6	05.5	20.8	22.6	25.2	28.7	13.0	64	66	47	06	1	00	0	00	0	10	1	7	4	0.0	
18	07.8	05.6	04.4	20.7	26.0	25.7	27.3	10.8	61	49	44	04	2	19	1	00	0	9	2	3	4	0.5	
19	04.3	01.5	00.7	20.9	27.4	25.8	27.8	14.5	66	47	61	16	1	20	1	16	2	9	9	10	10	0.0	
20	01.9	01.2	09.2	19.8	21.5	20.2	24.0	11.2	62	60	60	04	2	12	2	12	1	8	9	10	10	0.0	
21	01.8	99.5	98.0	15.6	19.8	20.0	21.7	13.3	59	50	50	03	2	07	2	07	1	9	6	7	7	2	
22	98.3	97.5	96.5	17.4	20.1	21.6	22.7	13.6	68	61	54	07	3	32	3	32	1	9	8	8	9	0.0	
23	98.9	97.7	97.8	18.8	22.1	19.6	25.8	13.5	63	51	63	04	1	10	1	00	0	9	2	8	8	0.0	
24	00.2	00.6	00.0	11.4	14.2	16.2	19.8	11.3	67	66	64	03	4	04	2	00	0	9	10	1	1		
25	06.9	07.2	07.2	12.9	18.9	18.4	20.8	11.3	58	48	46	03	3	24	1	24	1	9	4	5	6	0.0	
26	09.9	08.4	07.5	16.7	20.8	17.7	21.8	8.2	35	49	71	00	0	23	1	14	2	9	3	10	9	0.0	
27	06.8	05.9	05.5	16.1	17.4	14.6	17.8	14.3	81	74	91	14	2	15	3	04	2	8	10	10	10	19.7	
28	01.6	02.1	02.3	12.5	15.0	15.8	15.8	12.0	95	95	97	04	3	02	2	08	2	5	10	10	10	15.1	
29	03.3	03.8	03.9	15.4	16.6	17.5	19.8	14.5	95	94	82	03	2	04	2	10	2	6	10	10	9	12.5	
30	06.6	06.9	06.5	16.4	20.2	22.3	23.4	15.2	88	75	60	08	2	11	2	00	0	8	10	9	8	0.0	
31	09.6	09.2	08.7	16.7	24.7	23.8	24.8	15.1	91	58	54	00	0	28	3	00	0	9	10	8	R	0.0	
M	01.2	00.6	00.1	17.1	21.1	20.2	23.2	13.2	77	65	65	1.4		1.6		1.3	8.4	6.5	7.0	5.7	9.6		

**August VIII**

1	11.6	10.9	10.0	19.8	21.3	25.6	27.0	13.7	74	81	49	00	0	30	1	00	0	8	0	7	1	6.7		
2	11.8	11.1	10.7	21.4	26.6	25.0	27.0	15.4	69	52	62	03	2	05	3	00	0	8	7	1	1	0.0		
3	14.8	14.5	13.6	20.3	24.9	25.5	26.0	15.5	56	56	59	11	1	24	1	24	1	9	2	2	1			
4	16.9	16.6	15.8	19.8	25.3	22.3	25.7	13.3	77	50	53	16	1	18	1	15	2	9	0	1	1			
5	15.5	13.1	11.7	17.9	25.9	23.1	26.3	12.5	88	61	66	14	1	19	1	16	2	9	0	1	1			
6	11.7	10.3	09.0	19.3	24.6	21.9	26.0	14.5	79	68	71	00	0	14	1	12	2	8	4	1	3	9		
7	08.4	07.0	05.1	16.7	22.8	20.0	24.0	16.5	90	67	75	15	1	18	1	16	3	8	10	1	8	0.1		
8	03.8	02.1	00.3	16.4	25.0	20.0	25.0	15.5	88	54	70	22	1	22	2	16	3	8	10	1	6	0.0		
9	97.0	95.6	93.7	16.2	19.6	19.0	22.0	14.7	95	80	80	10	1	18	1	15	2	7	10	1	10	6.0		
10	91.8	91.0	91.3	15.4	20.5	18.3	21.8	11.4	91	69	71	16	1	19	3	20	1	8	10	1	5	0.0		
11	94.5	93.8	92.7	17.1	19.8	20.5	21.6	11.4	81	82	77	16	2	16	5	18	5	8	9	1	10	0.2		
12	95.1	94.3	95.3	17.1	20.0	14.7	21.6	12.5	77	50	65	22	1	18	2	28	9	9	7	1	1	10.1		
13	99.3	98.3	96.6	15.0	18.9	16.3	20.2	7.4	58	51	52	27	4	19	3	28	3	10	2	1	1	0.0		
14	99.9	97.7	90.7	00.9	13.3	19.6	20.6	7.8	78	64	64	00	0	28	5	30	3	10	3	7	3	0.0		
15	06.6	06.4	05.4	14.7	19.1	15.6	19.1	6.2	57	49	58	08	1	20	2	19	2	10	3	1	9	0.0		
16	03.4	02.3	00.6	14.0	18.4	16.4	19.4	12.4	98	69	75	19	1	16	4	16	3	9	10	1	9	0.3		
17	96.7	94.3	92.9	15.4	20.4	18.4	20.8	12.5	88	71	80	16	1	19	1	17	4	9	8	1	8	0.1		
18	95.5	96.2	95.6	15.7	18.2	18.2	19.9	13.4	95	82	85	00	0	17	4	16	3							

# Extenso-Tabelle

1944

**Oslo (Blindern)**

$\varphi = 59^{\circ} 56' N$   $l = 10^{\circ} 44' E$

$g = 9.819$

$\Delta G = +1^h$

**September IX**

$H_a = 94$

$H_b = 95.6$

$h_t = 2.0$

$h_a = 25.2$

$h_b = 25.6$

$h_t = 1.5$

Datum	Luftdruck P					Lufttemperatur T					Relative Feuchte U			Richtung und Stärke des Windes D,F			Sicht V			Bewölkung und Wetter N,w			Niederschlag R	Schneehöhe h <sub>s</sub>	Witterungsverlauf W	
	8	14	19	8	14	19	Max	Min	8	14	19	8	14	19	14	8	14	19								
1	79.6	82.2	86.3	10.7	14.6	11.4	14.7	9.8	95	71	92	22	2	00	0	29	1	10	=	10	-	10	•	26.4		
2	97.8	99.0	97.9	12.1	17.9	12.6	18.8	7.3	88	57	84	00	0	19	1	04	2	9	3	=	10	-	10	-	2.1	
3	92.9	89.2	87.3	11.1	10.4	8.7	13.5	8.7	92	92	90	04	4	J2	5	02	5	6	10	•	10	-	10	•	10.5	
4	90.2	92.7	93.1	9.2	11.6	11.4	13.8	7.2	89	74	79	02	2	16	1	00	0	8	9	=	10	-	10	-	22.4	
5	89.9	88.8	88.7	10.4	10.7	10.2	11.6	9.1	86	90	86	02	2	02	3	02	2	6	10	=	10	-	10	-	0.0	
6	85.8	87.9	90.7	9.7	13.4	12.9	13.7	9.0	91	78	80	03	1	18	1	00	0	8	10	•	10	-	9	-	4.2	
7	96.9	97.1	96.0	11.6	15.2	12.4	15.7	8.3	91	71	71	00	0	19	2	32	1	8	8	=	10	-	10	-	0.2	
8	82.5	76.8	83.0	12.2	12.9	12.2	13.1	10.2	90	95	79	08	2	15	2	20	4	7	10	=	10	-	10	-	17.8	
9	91.5	92.5	94.5	10.5	15.8	10.2	16.2	7.8	80	58	89	00	0	16	1	05	4	9	2	=	4	-	10	-	6.5	
10	03.7	05.6	06.5	9.4	13.8	9.7	14.2	5.0	62	53	62	02	1	17	1	00	0	9	2	=	8	-	5	-	24.6	
11	08.7	11.3	13.3	8.5	17.4	13.2	17.7	5.2	89	51	74	00	0	20	1	00	0	9	6	=	3	-	9	-		
12	20.6	21.2	21.0	10.2	15.9	11.2	15.9	8.7	83	60	81	00	0	21	1	00	0	9	2	=	9	-	6	-	0.0	
13	21.2	20.3	19.2	9.9	16.2	12.8	17.3	8.8	88	65	78	00	0	00	0	00	0	8	9	=	3	-	4	-	0.0	
14	19.3	18.3	17.3	9.3	16.0	11.8	17.2	6.4	93	62	78	00	0	24	2	00	0	9	9	=	5	-	1	-		
15	17.3	15.3	14.3	10.1	15.0	12.2	15.5	7.3	93	64	83	00	0	18	2	00	0	8	10	=	9	-	10	-	0.0	
16	13.5	11.4	08.8	10.2	12.9	12.5	13.9	10.0	81	79	91	08	1	16	1	00	0	7	10	=	10	-	10	-	0.0	
17	09.2	09.4	10.6	12.5	16.6	14.4	17.6	11.7	76	78	87	13	1	16	1	00	0	8	8	=	7	-	7	-	3.1	
18	15.6	15.9	16.8	10.3	14.6	13.2	14.7	7.0	94	82	91	00	0	00	0	00	0	9	9	=	10	-	10	-	4.0	
19	18.6	17.9	16.6	12.5	17.4	14.2	18.7	9.5	88	67	78	00	0	07	1	04	1	8	1	=	7	-	7	-	2.4	
20	13.9	12.0	12.0	10.2	11.6	11.8	14.4	9.5	88	92	94	03	3	03	1	07	1	5	10	=	9	-	8	-	0.5	
21	15.8	16.5	16.3	10.8	12.4	11.8	12.7	10.2	95	88	89	00	0	04	1	01	1	5	10	=	10	-	5	-	5.2	
22	14.5	12.1	10.4	11.2	14.6	11.5	14.8	10.7	94	67	70	07	1	08	3	08	2	8	10	=	9	-	10	-	0.0	
23	04.6	01.8	99.8	10.3	11.8	12.9	13.2	9.4	86	85	80	07	1	08	1	10	2	6	10	=	10	-	10	-	0.0	
24	92.6	92.8	92.6	12.8	13.8	11.3	13.9	11.1	96	68	81	15	1	16	2	17	1	8	10	=	10	-	10	-	16.0	
25	93.4	91.3	86.1	7.8	11.0	7.9	11.7	6.9	95	79	85	06	1	04	2	04	1	8	10	=	8	-	7	-	11.5	
26	74.9	76.3	78.4	7.0	10.4	8.4	12.8	4.8	95	70	65	18	1	26	3	22	3	8	10	=	10	-	3	-	1.0	
27	78.0	79.4	81.9	4.3	11.9	9.8	12.7	2.2	94	61	76	00	0	16	3	16	2	9	4	=	7	-	9	-	0.5	
28	90.3	94.2	97.3	7.7	13.4	9.2	13.7	4.5	86	53	53	02	1	27	2	25	2	9	3	=	8	-	8	-		
29	00.5	96.3	95.7	5.3	10.2	9.9	10.7	0.1	91	95	96	02	1	16	5	18	2	5	9	=	10	-	10	-		
30	84.9	85.2	89.2	10.4	9.8	8.1	11.2	8.0	99	78	74	24	1	26	4	22	2	8	10	=	10	-	10	-	29.8	
M	00.6	00.4	00.6	9.9	13.6	11.3	14.5	7.8	90	73	82	0.9		1.8	1.3	7.8	7.9	8.6	8.3						189	

**Oktober X**

1	95.1	95.6	96.9	4.3	11.1	6.2	11.7	-2.0	76	53	76	00	0	16	2	28	2	9	1	=	7	-	1	-	0.0		
2	01.2	01.4	01.2	3.1	12.8	5.0	13.3	-0.5	87	56	83	-3	1	18	1	16	1	8	1	=	1	-	0	-			
3	03.9	00.9	02.4	4.4	6.8	7.8	8.5	2.3	94	89	87	19	1	03	2	05	2	8	10	=	10	-	10	-	1.6		
4	08.8	09.8	11.2	5.3	12.6	5.7	13.5	4.5	87	49	82	21	2	04	1	01	1	8	8	=	1	-	1	-			
5	09.8	08.7	09.7	3.6	12.5	7.6	13.9	0.2	00	56	78	00	0	01	0	01	0	9	10	=	7	-	2	-			
6	14.3	09.8	05.4	2.8	9.9	7.5	9.9	1.5	91	68	91	01	JU	2	20	1	30	0	8	10	=	10	-	9	-		
7	02.1	00.3	99.9	8.2	19.4	13.4	20.1	6.8	91	56	63	16	1	16	1	28	2	9	8	=	2	-	2	-			
8	97.7	97.8	03.6	6.0	17.7	11.1	18.0	4.2	95	52	55	04	1	30	2	01	2	10	6	=	2	-	1	-			
9	05.5	05.9	06.0	5.0	9.9	9.6	11.7	2.3	82	82	94	03	1	24	1	18	2	6	9	=	6	-	6	-			
10	06.9	05.4	03.0	6.9	9.8	8.6	12.2	6.3	85	77	72	08	1	03	2	03	2	7	2	=	2	-	10	-			
11	99.3	99.1	99.1	7.0	8.6	9.0	9.0	5.7	95	94	97	03	2	20	3	34	1	5	10	=	10	-	10	-	19.0		
12	98.1	98.6	00.4	10.6	11.0	10.8	11.5	9.0	95	95	95	16	2	16	2	16	1	4	10	=	10	-	10	-	5.9		
13	97.7	94.9	92.7	10.1	11.0	10.8	11.0	9.6	95	89	92	13	1	13	2	16	2	6	10	=	10	-	10	-	2.2		
14	95.6	92.4	90.0	9.0	10.6	10.0	10.8	10.8	82	96	79	86	15	2	12	2	14	3	8	10	=	10	-	10	-	7.5	
15	90.8	93.4	94.4	9.5	11.6	8.3	11.7	8.2	89	75	88	18	3	18	4	11	1	9	8	=	9	-	6	-	4.4		
16	94.4	93.2	91.4	6.8	8.6	8.5	8.7	6.3	96	90																	

**Extenso-Tabelle**

**Oslo (Blindern)**

**1944**

Datum	November XI										December XII										Witterungsverlauf W						
	Luftdruck P			Lufttemperatur T				Relative Feuchte U			Richtung und Stärke des Windes D.F				Bewölkung und Wetter N,w			Niederschlag R			Schnethöhe h <sub>s</sub>						
	8	14	19	8	14	19	Max	Min	8	14	19	8	14	19	14	8	14	19	8	14	19						
1	94.3	94.3	95.9	1.4	4.3	2.6	4.4	3.8	69	56	76	02	5	02	6	01	5	6	6	10	10	10	3.5	3.2	3.2	3.2	
2	99.7	99.4	98.6	4.0	5.0	3.3	5.4	2.5	79	77	79	03	5	04	4	02	9	10	10	10	10	10	0.2	0.2	0.2	0.2	
3	89.9	85.0	82.8	4.4	5.3	4.4	5.6	5.3	84	91	83	03	4	04	3	03	2	7	10	10	10	10	0.1	0.1	0.1	0.1	
4	79.9	82.2	84.2	2.8	6.6	2.8	6.9	2.8	95	72	84	21	1	22	2	00	0	8	10	10	10	10	1.0	1.0	1.0	1.0	
5	72.4	70.1	72.7	10.4	10.7	6.6	11.6	1.7	88	86	91	15	4	20	7	20	4	6	10	10	10	10	3.2	3.2	3.2	3.2	
6	83.4	83.6	82.4	3.9	7.6	5.6	8.1	3.3	78	63	75	16	2	16	4	17	3	8	5	7	6	6	4.1	4.1	4.1	4.1	
7	78.0	76.9	78.4	1.9	3.3	3.0	6.0	0.4	94	89	91	00	0	03	3	33	0	5	10	10	10	10	0.2	0.2	0.2	0.2	
8	81.3	80.5	79.0	0.9	0.6	0.4	3.7	0.4	87	94	95	02	4	01	1	00	0	4	10	10	10	10	1.2	1.2	1.2	1.2	
9	79.0	83.6	89.0	1.2	2.0	1.2	2.3	0.3	93	91	91	04	2	02	2	02	0	6	10	10	10	10	4.6	4.6	4.6	4.6	
10	98.6	92.4	04.6	-2.4	-0.5	-1.6	1.9	-2.5	91	90	93	07	1	00	0	00	0	5	10	10	10	10	0.1	0.1	0.1	0.1	
11	08.4	09.2	07.9	-3.1	4.2	4.3	4.9	-4.7	95	74	69	04	2	02	3	02	5	8	3	10	10	10	1	1	1	1	
12	06.6	06.5	04.6	1.6	2.4	3.2	4.8	0.6	85	90	90	02	6	02	6	04	6	6	10	10	10	10	4.8	4.8	4.8	4.8	
13	02.3	04.3	07.1	5.6	5.6	4.8	5.9	3.2	86	90	87	03	6	04	4	04	6	6	10	10	10	10	5.4	5.4	5.4	5.4	
14	06.4	04.9	04.1	2.0	0.4	0.3	5.0	-0.5	91	92	90	03	5	03	6	03	6	6	10	10	10	10	3.7	3.7	3.7	3.7	
15	07.3	08.8	11.8	1.6	2.4	0.0	2.7	-0.2	89	78	84	03	5	05	7	04	6	6	10	10	10	10	8.0	8.0	8.0	8.0	
16	14.6	15.7	16.8	-0.2	-0.4	-0.8	0.2	-1.3	72	67	67	02	6	02	5	02	3	9	10	10	10	10	0.5	0.5	0.5	0.5	
17	17.0	15.9	14.2	-1.2	-1.1	-1.7	-0.5	-0.5	76	69	81	02	6	06	2	07	4	6	10	10	10	10	0.9	0.9	0.9	0.9	
18	07.0	00.8	98.6	-2.3	-1.2	-0.8	-0.8	-2.8	91	88	91	06	2	02	2	07	4	5	10	10	10	10	0.9	0.9	0.9	0.9	
19	96.5	91.0	84.5	0.5	0.9	1.5	1.5	-1.1	91	95	93	04	2	04	2	02	5	4	10	10	10	10	2.2	2.2	2.2	2.2	
20	76.6	76.4	74.7	1.3	1.8	1.4	3.1	0.8	98	97	94	00	0	00	0	00	0	4	10	10	10	10	12.2	12.2	12.2	12.2	
21	84.6	90.2	94.8	-0.5	3.2	-0.2	3.6	-1.4	74	61	67	03	2	28	4	00	0	9	5	10	10	10	10	0.5	0.5	0.5	0.5
22	97.7	97.2	96.4	-6.2	-3.5	-5.9	-0.1	-7.0	81	79	85	06	1	00	1	04	2	2	10	10	10	10	0.0	0.0	0.0	0.0	
23	89.0	84.1	80.4	-4.6	-1.3	0.4	0.7	-8.2	87	91	97	02	2	06	1	00	0	5	10	10	10	10	0.0	0.0	0.0	0.0	
24	74.5	74.5	74.5	1.1	0.9	0.2	1.7	0.0	90	90	90	00	0	00	0	00	0	2	10	10	10	10	9.7	9.7	9.7	9.7	
25	71.4	71.6	73.5	-0.4	0.4	-5.4	0.7	-5.7	91	84	92	32	2	00	0	32	1	6	9	10	10	10	10	0.7	0.7	0.7	0.7
26	82.5	86.5	91.3	-6.1	-5.3	-5.4	-4.6	-7.0	95	94	95	15	1	10	1	00	0	4	9	10	10	10	10	19	19	19	19
27	03.9	07.9	10.3	-5.6	-4.4	-8.2	-2.7	-8.9	87	84	90	04	1	00	1	00	0	3	10	10	10	10	0.0	0.0	0.0	0.0	
28	10.6	05.2	00.2	-8.0	-1.2	1.9	2.3	-11.7	93	95	95	03	2	07	1	15	3	4	10	10	10	10	0.0	0.0	0.0	0.0	
29	97.7	99.9	01.5	1.4	1.7	-1.0	2.2	1.0	97	99	99	04	22	1	20	1	20	1	3	10	10	10	10	6.1	6.1	6.1	6.1
30	02.1	02.0	02.4	2.8	3.2	3.0	3.4	0.8	90	90	90	22	1	20	1	20	1	3	10	10	10	10	0.7	0.7	0.7	0.7	
M	93.8	93.7	93.9	0.3	1.8	0.7	3.0	-1.4	88	84	88	2.5	2	2.6	2.2	5.4	8.3	7.7	7.4	7.4	7.4	72					

**Dezember XII**

1	05.1	02.6	99.4	0.6	1.3	3.4	3.5	0.3	03	00	00	0	02	1	00	0	3	10	10	10	10	10	3.5	3.5	3.5	3.5
2	82.1	79.4	79.8	7.4	6.0	3.4	7.8	3.3	97	89	81	16	5	16	5	17	4	8	10	10	10	10	9.7	9.7	9.7	9.7
3	83.2	81.8	79.1	0.3	0.6	0.4	3.9	0.1	95	97	99	03	1	00	0	00	0	2	10	10	10	10	2.3	2.3	2.3	2.3
4	74.1	76.6	78.2	0.7	0.5	0.2	1.3	-0.1	93	94	90	04	2	02	2	02	1	6	10	10	10	10	8.9	8.9	8.9	8.9
5	77.9	77.5	78.1	0.4	0.8	0.4	1.0	-1.2	89	88	90	04	2	02	2	02	1	6	10	10	10	10	3	3	3	3
6	79.6	82.5	82.9	0.8	0.9	1.1	2.0	0.0	97	92	95	18	2	04	1	05	1	5	10	10	10	10	5.7	5.7	5.7	5.7
7	80.6	79.3	78.5	1.4	1.2	1.1	2.2	0.3	92	91	95	08	3	06	3	08	3	5	10	10	10	10	1.4	1.4	1.4	1.4
8	77.5	77.0	77.7	2.4	3.0	1.4	3.2	1.0	91	87	91	08	3	04	4	04	5	6	10	10	10	10	7.6	7.6	7.6	7.6
9	84.0	84.5	83.0	2.2	1.8	0.8	2.9	-2.9	90	92	89	03	2	01	2	02	3	6	10	10	10	10	7.5	7.5	7.5	7.5
10	82.9	83.5	85.0	-0.5	0.8	1.4	1.5	-1.0	87	94	92	00	0	10	1	16	2	5	10	10	10	10	0.0	0.0	0.0	0.0
11	90.1	92.4	92.7	0.6	2.2	1.8	2.7	-0.4	95	89	85	05	1	06	2	06	2	2	10	10	10	10	12.2	12.2	12.2	12.2
12	92.0	93.6	96.9	-3.0	-2.7	-6.2	2.0	-6.4	87	85	89	02	1	00	0	00	0	1	10	10	10	10	2.2	2.2	2.2	2.2
13	09.8	13.7	17.1	-9.6	-7.2	-7.8	-6.0	-10.2	90	89	91	00	0	00	0	00	0	3	10	10						

# Extenso-Tabelle

1944

**Bergen (Fredrikberg)**

$\varphi = 60^\circ 24' N$   $\lambda = 5^\circ 19' E$

$g = 9.819$

$\Delta G = +1^h$

**Januar I**

$H_a = 43$

$H_b = 44.4$

$h_t = 1.8$

$h_a = 10.7$

$h_d = 10.3$

$h_r = 1.3$

Datum	Luftdruck P			Lufttemperatur T						Relative Feuchte U			Richtung und Stärke des Windes D,F			> Sicht	Bewölkung und Wetter N,w			Niederschlag R	Schneehöhe E	Witterungsverlauf W		
	8	14	19	8	14	19	Max	Min	8	14	19	8	14	19	14	8	14	19						
1	88.9	91.9	92.3	2.6	3.4	2.4	5.0	-0.3	85	77	82	30	1	32	1	10	2	8	5+	8-	9-	13.8	12	* n, * a, p
2	86.5	82.0	93.3	3.4	6.3	4.3	6.6	-1.9	90	98	95	12	3	26	3	28	3	7	10+	10-	7+	3.9	11	* - n, a, p
3	86.7	88.4	87.9	1.2	-0.2	-0.9	9.0	-1.3	77	85	97	32	1	00	0	10	2	9	10+	6(+)	10+	13.7	2	* + Δ - n, * Δ - a, * - p
4	86.9	12.9	17.0	-1.2	-0.8	-2.9	0.0	-3.1	60	63	84	02	3	00	0	20	0	8	0	1-	0-	3.9	6	* - n, * - a, * - p
5	15.0	07.4	99.9	0.4	1.5	6.4	6.4	-3.9	75	96	96	12	4	12	5	16	5	5	10+	10+	10+	0.0	6	* = n, * + a, * + a, * - p
6	88.3	90.9	93.2	6.1	5.2	3.8	8.0	3.0	74	70	72	28	4	28	4	28	4	8	1	7-	6(0)	54.8	19	* - n, * - a, * Δ - p
7	94.3	96.1	92.5	2.6	1.3	0.7	4.3	0.5	65	83	98	28	3	12	3	32	2	9	8	9-	10+	1.0	0	Δ - n, * - a, * - p
8	94.8	88.1	86.3	0.2	0.6	-1.9	1.5	-2.2	98	67	77	14	3	02	3	32	2	9	10+	9-	0	14	* - n, * + a, * - p	
9	78.6	76.4	80.0	-3.1	-1.6	-1.1	-1.0	-4.5	94	82	76	00	0	12	2	30	1	6	4	9-	9-	8.6	21	* = n, * a, p
10	90.2	96.6	02.9	-3.8	-3.4	-3.9	-0.8	-4.9	87	91	94	00	0	12	2	12	1	3	3-	10+	9+	0.4	19	* - n, * - a, * - p
11	10.6	11.7	12.2	-1.1	-0.2	-1.6	-0.2	-4.1	94	92	92	26	0	10	2	10	2	6	9+	5-	5-	5.2	24	* - n, * - a, * - p
12	12.3	11.3	09.5	-4.4	-1.7	1.9	2.4	-3.4	94	93	96	00	0	30	1	14	4	3	1-	10-	10+	1.3	23	- - n, - a, * - p
13	05.1	98.5	92.6	4.8	7.1	5.6	7.4	1.2	85	91	94	14	5	12	4	14	4	9	10-	10+	10+	7.6	11	* - n, * - a, * - p
14	99.3	06.5	09.4	5.1	6.2	5.3	6.3	3.2	91	83	97	16	4	28	2	14	3	3	9-	9-	10-	24.1	0	* - n, * a, p
15	21.0	25.7	26.5	8.6	7.9	6.9	9.0	5.0	92	91	93	28	2	16	3	14	3	6	10-	9+	1-	13.3	13	* - n, * - a, * - p
16	26.5	25.2	24.2	5.6	6.0	5.8	7.0	5.0	90	67	87	14	3	14	4	14	5	9	9-	1-	10+	0.2	0	* - n, * - a, * - p
17	23.6	18.7	15.8	5.3	5.9	6.3	7.1	4.8	91	96	97	12	3	14	4	14	5	4	9-	10+	10+	3.0	0	* - n, * - a, * - p
18	13.6	10.8	08.6	7.1	7.2	7.2	7.6	6.2	97	91	82	14	4	16	5	14	5	7	10-	9+	10-	6.8	0	* - n, * a, - p
19	10.2	12.0	12.6	6.6	6.1	4.3	7.6	4.2	88	90	91	30	1	14	2	12	2	7	8-	7-	2-	11.4	0	* - n, * a, * - p
20	11.0	08.5	04.0	4.8	5.4	5.4	5.4	3.3	91	76	76	12	4	14	5	14	6	8	8-	8-	10-	0.0	0	* - n, a, p
21	91.3	93.4	94.0	5.3	4.6	3.0	6.6	1.0	79	94	93	14	3	18	3	18	3	8	10-	8-	9+	11.2	0	* - n, * - a, * - p
22	77.2	75.4	75.1	4.5	7.5	5.2	8.0	2.3	92	85	82	16	7	18	5	18	6	8	10+	10+	9+	27.1	0	* - n, * - a, * - p
23	69.8	67.3	67.1	0.6	3.3	3.5	6.7	0.5	97	91	78	10	1	12	5	02	2	8	10+	5-	10-	26.4	0	* - n, * a, * - p
24	90.4	92.2	88.6	1.5	1.5	1.6	3.8	0.5	68	85	75	32	3	12	2	14	3	7	8-	8-	7-	1.8	0	* - n, * a, * - p
25	69.1	67.3	72.6	3.7	4.8	3.5	5.6	1.5	50	51	72	08	3	06	5	22	1	10	8-	10-	10-	0.0	0	* - n, a, * - p
26	92.7	99.5	99.2	2.1	3.7	2.4	4.0	1.3	96	77	81	32	3	30	1	12	3	9	10+	7-	10-	0.1	0	* - n, - a, * - a, * - p
27	88.1	83.9	87.5	7.2	7.0	5.8	7.8	1.5	88	66	74	16	3	26	2	24	4	8	10-	10-	6-	5.9	0	* - n, * - a, * - p
28	91.1	01.1	06.3	5.4	4.6	3.8	6.4	3.5	91	75	76	32	3	30	3	00	0	8	9+	9-	9-	6.2	0	* - n, * - a, * - p
29	05.2	02.2	4.7	7.8	7.9	8.4	2.7	0.7	97	94	93	14	4	16	3	26	3	5	10-	10-	10-	2.7	0	* - n, * - a, * - p
30	07.1	09.9	11.2	6.4	7.5	6.2	8.3	5.6	90	88	93	30	2	28	3	00	0	6	10-	10-	10-	13.0	0	* - n, * a, * - a, * - p
31	07.4	03.1	03.8	6.9	6.9	7.9	8.2	5.6	97	94	92	14	5	14	6	16	3	4	10-	10+	10-	2.0	0	* - n, * - a, * - a, * - p
M	98.5	90.6	99.3	3.2	4.2	3.4	5.4	1.1	86	83	86	2.7	3	3.0	3.0	7.1	8.0	8.2	8.0	280	5			

**Februar II**

1	00.2	90.8	85.5	6.7	6.6	7.3	8.8	6.3	94	90	97	16	3	14	6	14	4	4	10+	10+	10+	10.4	1	* - n, a, * - p
2	96.1	95.6	89.6	3.8	4.2	3.9	8.2	3.3	92	87	87	32	1	16	2	14	4	5	9-	9-	10+	25.8	0	* - n, * - a, * - p
3	78.8	74.8	76.9	6.6	5.8	3.6	7.5	2.4	94	91	91	16	4	16	4	28	5	5	9+	9+	10+	8.2	0	* - n, * - a, * - p
4	79.6	89.2	96.9	-1.9	1.2	2.0	2.0	-2.2	88	64	78	10	2	32	3	02	2	10	2-	1-	1-	18.0	0	* - n, * - a, * - p
5	11.6	16.1	19.0	0.6	1.0	0.2	1.3	-0.2	70	73	83	02	3	32	3	02	2	10	2-	1-	1-	18.0	0	* - n, * - a, * - p
6	17.9	12.4	06.7	0.4	1.5	1.7	1.8	-0.6	68	71	94	12	1	12	5	12	6	9	9-	10-	10-	0.0	0	* - n, * - a, * - p
7	87.0	77.9	76.7	7.8	5.6	3.8	8.1	-1.6	93	78	88	16	5	24	5	24	5	7	10+	10+	10+	23.8	0	* - n, * - a, * - p
8	90.2	95.1	97.4	2.3	-0.3	-0.7	4.4	-1.1	82	93	91	30	6	32	2	30	3	9	10+	10+	9+	12.1	0	* - n, * - a, * - p
9	96.2	88.8	80.7	-1.4	0.7	0.5	1.9	-1.7	88	74	74	10	1	12	3	04	4	8	8-	8-	8-	5.4	0	* - n, * - a, * - p
10	00.3	06.7	10.0	-0.9	1.8	1.1	1.8	-1.4	59	56	65	32	2	32	3	32	1	10	0	0	1	2.8	4	* - n, * - a, * - p
11	12.2	11.6	11.4	0.5	2.4	2.0	2.8	-0.3	90	90	92	00	0	24	1	00	0	7	9-	9-	10-	2.0	0	* - n, * - a, * - p
12	15.1	18.6	20.4	0.9	3.7	3.0	4.0	-0.1	93	73	84	12	1	12	3	12	3	7	8-	10-	10-	0.0	0	* - n, * - a, * - p
13	21.9	19.8	18.2	1.8	1.8	1.0	3.2	1.0	83	60	60	12	1	16	3	14	3	9	10-	10-	10-	0.0	0	* - n, * - a, * - p
14	18.7	22.5	23.1	2.1	3.5	2.9	3.8	0.2	84	61	62	14	4	14	3	12	3	7	9-	9-	9-	0.0	0	* - n, * - a, * - p
15	23.9	21.5	18.9	1.9	2.5	3.1	3.2	1.5	73	65	68	12	5	14	5	14	5	9	10-	3-	10-	0.0		

**Extenso-Tabelle**

**1944**

**Bergen (Fredrikberg)**

$\varphi = 60^{\circ} 24' N$

$\lambda = 5^{\circ} 19' E$

$g = 9.819$

$\Delta G = +1^{\circ}$

**März III**

$H_a = 43$

$H_b = 44.4$

$h_c = 1.8$

$h_d = 10.7$

$h_e = 10.3$

$h_f = 1.3$

Datum	Luftdruck P			Lufttemperatur T					Relative Feuchte U			Richtung und Stärke des Windes D.F.			> Süd			Bewölkung und Wetter N.w			Niederschlag $\alpha$	Schneehöhe h <sub>s</sub>	Witterungsverlauf W	
	8	14	19	8	14	19	Max	Min	8	14	19	8	14	19	14	8	14	19						
1	79.0	78.4	78.7	-1.4	-0.9	-0.7	0.9	-2.1	88	83	88	10	2	16	1	00	0	8	10	9 8	9 9	18.0	11	8 - n, 8 8 - a, 8 - p
2	74.5	74.2	78.8	-0.8	3.1	1.0	3.6	-1.7	92	67	73	14	4	12	2	24	1	8	9 8	9 -	9 -	6.3	16	8 8 - a, 8 8 - a, 8 - p
3	87.2	91.0	95.9	1.7	1.2	0.5	2.6	-0.6	85	82	90	30	4	30	4	32	4	9	9 (8)	5 8	1 -	0.5	13	8 8 - n, 8 8 - a, 8 - p
4	99.1	92.2	96.7	-1.8	0.7	-1.2	1.8	-3.0	77	65	74	52	2	32	1	02	2	10	1 -	2	6	0.0	10	8 8 - n, 8 8 - a, 8 - p
5	15.9	19.6	21.4	-1.4	2.0	1.2	2.0	-2.9	79	67	85	00	0	12	2	12	3	9	9 -	10	10 8	10 -	8	8 - n, 8 8 - a, 8 - p
6	27.1	29.3	30.2	2.4	5.5	4.2	6.6	-1.1	98	81	90	10	1	30	2	28	2	9	9 -	4 8	1 -	2.0	0	8 8 - n, 8 8 - a, 8 - p
7	34.8	36.2	35.8	0.4	5.9	3.4	6.0	-0.5	94	72	91	00	0	24	1	28	1	7	9 8	9 -	7 -	0.0	0	8 8 - n, 8 8 - a, 8 - p
8	35.9	34.9	34.3	0.0	4.1	3.2	4.7	-0.6	92	73	91	00	0	30	1	30	3	9	9 -	9 8	9 -	9 -	0	8 8 - n, 8 8 - a, 8 - p
9	26.7	22.1	16.3	2.8	3.8	3.7	4.1	-2.2	92	96	97	10	1	14	3	14	3	6	10	10 8	10 -	10	0	8 8 - n, 8 8 - a, 8 - p
10	10.1	06.3	98.0	4.0	5.2	5.5	7.1	3.6	94	86	93	30	1	26	2	28	3	8	9 -	9 (8)	10 -	13.8	0	8 8 - n, 8 8 - a, 8 - p
11	89.4	95.1	99.1	1.2	4.2	4.2	5.7	0.3	91	77	84	30	4	30	3	30	3	10	9 8	2	1 -	5.2	1	8 8 - n, 8 8 - a, 8 - p
12	95.8	89.0	85.8	1.0	3.8	1.9	4.4	0.4	97	92	96	12	3	30	0	12	2	4	10 8	10 -	10 -	1.7	0	8 8 - n, 8 8 - a, 8 - p
13	73.5	76.3	79.1	0.7	3.2	1.9	3.7	0.5	87	67	70	32	3	32	2	32	2	9	9 -	4 8	1 -	13.2	0	8 8 - n, 8 8 - a, 8 - p
14	90.0	92.1	94.8	1.1	3.5	2.7	5.1	0.1	68	86	88	02	2	32	2	32	2	8	9 8	1 -	1 -	0.0	0	8 8 - n, 8 8 - a, 8 - p
15	02.2	03.8	04.1	0.6	5.9	2.4	5.4	0.1	82	60	77	28	1	32	1	30	0	10	1 -	9	9 -	0.0	0	8 8 - n, 8 8 - a, 8 - p
16	03.2	05.4	07.3	2.1	3.9	3.4	4.0	0.9	83	85	91	12	4	10	3	06	2	6	10	10 8	10 -	0.3	0	8 8 - n, 8 8 - a, 8 - p
17	09.7	10.7	11.2	4.2	7.2	5.7	7.6	3.2	92	91	94	30	1	30	1	12	2	7	10	10 -	10 -	0.8	0	8 8 - n, 8 8 - a, 8 - p
18	04.2	07.8	05.5	4.2	4.5	4.4	6.1	3.3	98	79	83	30	3	10	2	14	4	7	7	9 8	10 -	23.8	0	8 8 - n, 8 8 - a, 8 - p
19	91.6	92.3	94.6	3.8	2.6	0.5	5.7	-0.4	79	81	96	30	4	30	2	32	2	7	7	10 8	9 -	22.7	0	8 8 - n, 8 8 - a, 8 - p
20	02.5	02.5	03.2	-0.3	1.9	0.0	2.5	-0.5	94	72	78	30	4	30	3	30	4	8	9 *	10 (8)	8 -	9.0	8	8 8 - n, 8 8 - a, 8 - p
21	09.7	10.7	11.0	-1.1	3.6	1.2	3.7	-1.7	71	54	57	32	1	32	2	02	2	9	1	9 -	1 -	1.1	7	8 8 - n, 8 8 - a, 8 - p
22	12.5	11.8	11.7	-0.3	4.5	1.7	4.5	-2.1	55	44	56	02	3	24	1	18	2	10	1 -	1	9 -	0	0	8 8 - n, 8 8 - a, 8 - p
23	06.9	13.7	05.3	-0.1	2.5	3.7	4.1	-1.6	92	98	88	12	4	10	3	02	4	4	10	10 -	9 -	0.4	0	8 8 - n, 8 8 - a, 8 - p
24	13.4	15.8	18.4	1.9	7.4	5.5	8.4	1.6	97	70	73	14	1	30	1	14	2	9	7	7	7 -	7.5	0	8 8 - n, 8 8 - a, 8 - p
25	22.5	20.1	19.0	3.3	3.9	4.7	5.6	2.4	76	92	95	14	4	12	4	10	4	6	10	10 -	10 -	0.0	0	8 8 - n, 8 8 - a, 8 - p
26	15.9	17.1	19.0	5.3	9.4	6.0	9.6	4.3	85	78	88	14	1	32	3	30	1	8	9 8	1 -	1 -	4.6	0	8 8 - n, 8 8 - a, 8 - p
27	20.8	19.5	16.5	3.7	6.2	5.4	6.4	0.5	85	86	91	12	3	16	4	24	1	8	9 8	10 -	9 -	0.1	0	8 8 - n, 8 8 - a, 8 - p
28	08.1	05.4	02.5	2.9	4.4	2.2	5.7	1.4	91	74	82	30	2	30	4	32	2	9	9 8	9 -	1 -	2.8	0	8 8 - n, 8 8 - a, 8 - p
29	01.5	00.9	99.8	0.2	4.9	2.8	5.7	-1.3	85	61	73	00	0	00	0	00	0	8	8 1	8 -	7 -	0.6	0	8 8 - n, 8 8 - a, 8 - p
30	97.6	97.2	97.3	-0.6	2.5	0.5	3.3	-1.3	60	45	46	02	3	32	3	02	2	10	1 -	1	1 -	0.0	0	8 8 - n, 8 8 - a, 8 - p
31	99.7	02.4	04.4	-2.3	3.4	1.3	3.6	-4.2	72	47	55	00	0	30	1	26	2	9	0 -	1	1 -	0	0	8 8 - n, 8 8 - a, 8 - p
M	05.1	05.6	05.9	1.2	4.0	2.7	4.8	0.1	85	75	82	22	2	21	2.1	8.1	7.3	7.3	6.4	134	2	0	0	0

**April IV**

1	11.0	12.6	13.8	-1.1	3.4	0.4	3.7	-3.0	67	61	69	10	2	16	2	00	0	8	9 -	8 -	10 -	6.2	7	8 8 - n, 8 8 - a, 8 - p
2	13.9	13.9	13.4	-0.2	4.1	2.6	5.3	-0.5	96	86	87	10	2	12	2	12	2	0	8	9 -	1 -	0.1	0	8 8 - n, 8 8 - a, 8 - p
3	10.9	10.4	09.7	0.9	5.7	4.5	6.8	-1.1	77	42	44	00	0	04	2	10	0	8	9 -	1 -	0 -	0	0	8 8 - n, 8 8 - a, 8 - p
4	09.1	08.9	09.3	2.1	8.9	4.9	6.0	-0.7	65	45	44	00	0	30	1	02	1	9	1 -	10 8	9 -	0	0	8 8 - n, 8 8 - a, 8 - p
5	09.5	10.0	10.8	0.2	6.6	5.1	8.7	-1.2	77	52	57	00	0	32	1	30	1	9	4 -	0 -	1 -	0	0	8 8 - n, 8 8 - a, 8 - p
6	15.6	16.3	16.3	1.1	5.9	4.8	6.7	-0.9	75	57	82	00	0	16	5	16	3	8	0 -	9 -	9 -	0	0	8 8 - n, 8 8 - a, 8 - p
7	15.1	15.9	15.8	4.4	6.8	5.1	7.5	2.3	94	82	85	14	3	20	4	16	2	8	8 -	8 -	9 -	2.4	0	8 8 - n, 8 8 - a, 8 - p
8	14.3	13.2	11.2	3.3	6.3	6.2	7.0	2.5	92	75	83	12	4	16	5	16	4	7	10 -	9 -	9 -	1.6	0	8 8 - n, 8 8 - a, 8 - p
9	07.4	06.5	06.0	7.7	14.6	11.0	14.9	4.4	47	34	39	12	2	16	3	30	1	9	10 -	8 -	7 -	0.0	0	8 8 - n, 8 8 - a, 8 - p
10	06.5	06.3	05.7	7.5	12.3	13.7	4.8	4.8	73	48	73	00	0	28	1	28	1	9	10 -	9 -	10 -	0.0	0	8 8 - n, 8 8 - a, 8 - p
11	05.9	04.7	04.5	5.2	6.2	4.9	7.7	4.9	92	96	95	12	2	10	2	18	1	6	10 -	10 -	9 -	6.3	3	8 8 - n, 8 8 - a, 8 - p
12	05.7	07.4	08.2	6.2	10.4	7.																		

# Extenso-Tabelle

1944

**Bergen (Fredriksberg)**

$\varphi = 60^\circ 24' N$

$\lambda = 5^\circ 19' E$

$g = 9.819$

$\Delta G = + 1^h$

**Mai V**

$H_s = 43$

$H_b = 44.4$

$h_t = 1.8$

$h_a = 10.7$

$h_d = 10.3$

$h_r = 1.3$

Datum	Luftdruck P			Lufttemperatur T					Relative Feuchte U			Richtung und Stärke des Windes D,F			> Sicht			Bewölkung und Wetter N.w			Niederschlag R	Schnellhöhe	Witterungsverlauf W		
	8	14	19	8	14	19	Max	Min	8	14	19	8	14	19	14	8	14	19							
1	02.7	05.4	04.4	7.8	8.7	7.1	9.6	6.2	97	66	65	26	1	28	3	26	2	8	10 -	9 -	10 -	28.2		$\text{F} = \text{E}^\circ \text{n}, \text{F}^\circ = \text{O}^\circ \text{s}, -\text{O}^\circ \text{p}$	
2	05.0	02.7	08.1	6.1	8.1	7.6	8.4	3.1	93	96	96	12	5	14	3	16	3	5	10 -	10 -	10 -	8.1		$\text{E}^\circ = \text{O}^\circ \text{n}, \text{E}^\circ = \text{O}^\circ \text{s}, -\text{O}^\circ \text{p}$	
3	06.3	04.2	09.3	5.4	7.0	6.5	7.8	4.1	78	70	72	30	5	30	4	32	4	9	10 -	9 -	9 -	16.0		$\text{O}^\circ = \text{E}^\circ \text{n}, \text{O}^\circ = \text{O}^\circ \text{s}, \text{O}^\circ = \text{p}$	
4	09.0	09.0	07.4	6.4	10.8	8.6	11.4	3.1	59	49	48	42	3	30	1	18	2	10	1	4	7 -	7 -	0.1		$\text{O}^\circ = \text{O}^\circ \text{n}, \text{O}^\circ = \text{O}^\circ \text{s}, \text{O}^\circ = \text{p}$
5	07.8	06.9	01.0	5.4	7.9	5.9	9.3	2.5	59	44	41	18	1	02	4	02	3	10	9 -	1	0 -	0.0		$\text{O}^\circ = \text{O}^\circ \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
6	11.2	14.6	17.4	5.5	9.2	7.4	9.2	1.7	48	47	48	00	0	26	3	30	1	9	0 -	1 -	1 -			$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
7	22.8	22.7	23.5	7.1	10.6	7.8	10.9	1.0	56	55	52	00	0	18	3	16	2	9	10 -	1 -	1 -			$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
8	24.3	23.2	22.9	7.4	10.1	8.0	11.4	3.3	68	61	68	12	3	18	4	16	3	9	10 -	0 -	9 -			$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
9	20.2	19.2	17.8	9.9	9.2	9.0	10.7	6.4	59	73	90	14	3	18	4	16	3	7	1 -	10 -	9 -			$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
10	13.6	13.1	11.5	7.5	10.4	9.8	12.2	7.1	96	82	84	18	3	26	1	14	2	7	9 -	9 -	9 -	1.9		$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
11	10.0	12.8	13.6	7.6	9.8	9.9	10.6	6.0	94	87	86	14	4	16	3	14	2	6	10 -	10 -	9 -	2.0		$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
12	12.6	15.8	13.8	10.8	12.2	11.7	12.5	9.8	85	84	82	16	4	14	4	16	4	6	10 -	9 -	10 -	0.1		$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
13	10.8	10.5	11.0	11.4	11.0	8.5	14.1	8.5	86	84	97	16	3	14	3	30	2	6	10 -	10 -	10 -	22.9		$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
14	15.7	16.1	15.1	4.6	6.2	5.4	8.7	4.1	78	72	78	30	4	30	4	28	3	10	9 (i)	6 (i)	9 -	10.6		$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
15	11.5	10.2	10.3	6.2	10.9	10.7	11.8	3.7	74	53	55	32	3	32	4	32	2	9	9 -	9 -	9 -	1.6		$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
16	17.0	20.9	21.3	9.8	9.5	8.2	10.8	6.7	77	76	82	14	2	26	2	30	1	9	7 -	10 -	10 -	2.3		$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
17	20.0	17.8	17.2	9.2	17.6	16.8	19.2	6.3	88	55	55	00	0	02	1	04	3	9	3 -	6 -	1 -	0.1		$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
18	17.1	15.0	13.7	13.8	20.4	18.1	21.2	8.6	74	53	48	00	0	30	2	02	3	9	0 -	1 -	1 -			$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
19	12.0	09.6	07.0	14.3	15.5	18.5	19.8	9.8	65	60	63	00	0	26	2	28	1	9	1 -	2 -	1 -			$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
20	07.1	07.7	07.0	11.3	15.1	10.6	15.8	8.9	49	49	63	02	3	26	2	28	1	9	9 -	10 -	10 -			$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
21	03.0	02.7	02.6	5.2	7.6	4.7	10.6	3.9	94	71	77	00	0	28	3	30	4	9	9 (i)	9 (i)	9 -	1.7		$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
22	05.0	06.2	09.9	7.0	8.6	7.2	9.0	1.8	77	59	63	30	3	30	4	30	4	9	7 -	7 -	7 -	2.8		$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
23	12.0	12.3	12.2	6.7	9.7	6.4	10.2	3.3	64	59	67	32	2	28	3	30	2	9	1 -	5 -	10 -			$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
24	07.5	06.9	09.5	4.7	9.7	7.3	10.2	3.5	85	65	63	30	4	30	3	30	3	9	4 -	1 -	1 -	2.3		$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
25	05.7	01.6	00.6	6.3	8.6	5.8	9.0	2.3	72	55	81	00	0	22	1	22	1	8	10 -	10 -	10 -			$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
26	05.5	10.2	11.1	7.6	10.9	11.9	12.8	4.8	94	86	56	10	2	18	3	16	3	7	10 -	9 -	9 -	0.8		$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
27	11.1	18.2	22.0	10.7	12.7	10.8	13.5	10.0	97	82	81	16	5	18	2	14	3	8	10 -	9 -	9 -	9.5		$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
28	26.2	26.7	24.2	12.4	11.9	10.9	14.4	9.4	72	85	91	14	2	18	3	14	3	7	9 -	10 -	10 -	2.7		$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
29	23.3	22.6	21.5	10.0	10.5	11.0	11.5	9.6	96	97	93	14	2	00	0	30	2	6	10 -	10 -	9 -	26.2		$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
30	20.7	19.2	18.0	9.4	12.2	10.9	12.8	7.6	96	77	72	30	2	28	3	30	4	9	9 -	9 -	9 -	7.6		$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
31	16.6	15.1	13.6	9.0	12.7	10.2	13.4	7.0	81	67	71	32	2	32	2	28	2	9	9 -	6 -	7 -			$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$	
M	10.5	11.1	11.0	8.3	10.9	9.4	12.0	5.6	78	68	71	2.3		2.7		2.5	8.2	7.4	6.9	7.1	148				

**Juni VI**

1	09.6	08.0	06.4	8.1	12.6	12.3	13.9	5.5	82	71	67	32	1	26	3	28	1	9	9 -	9 -	3 -			$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$
2	05.5	05.2	04.6	8.9	13.0	10.9	13.1	6.7	84	73	77	14	1	26	2	26	2	9	9 -	9 -	9 -	0.0		$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$
3	05.1	06.6	06.6	8.9	12.4	9.6	13.1	8.2	86	65	64	30	2	30	1	30	2	10	9 -	1	4 -	11.2		$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$
4	00.4	95.3	92.2	9.0	12.1	11.8	13.0	5.9	78	82	88	00	0	16	5	14	4	7	10 -	10 -	10 -	0.0		$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$
5	90.2	90.6	90.3	11.3	12.7	14.8	9.5	9.5	82	73	71	14	5	16	4	14	5	9	2 -	10 -	9 -			$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$
6	96.2	99.6	00.7	10.2	16.6	17.7	18.9	9.0	96	68	57	00	0	30	1	00	0	9	10 -	9 -	2 -	13.1		$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$
7	99.3	99.4	00.6	12.9	18.7	17.9	20.0	10.1	71	56	54	26	1	06	2	06	2	9	9 -	7 -	2 -	0.1		$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$
8	96.9	96.5	96.0	14.0	14.5	12.8	18.8	12.2	74	79	88	00	0	20	1	00	0	8	7 -	9 -	10 -			$\text{O}^\circ = \text{n}, \text{O}^\circ = \text{a}, \text{O}^\circ = \text{p}$
9	94.2	93.1	92.8	9.9	12.9	10.7	14.9	9.5	94	82	85	14	2	18	3	18</td								

# Extenso-Tabelle

1944

Bergen (Frederiksberg)

$\phi = 60^{\circ} 24' N$

$\lambda = 5^{\circ} 19' E$

$g = 9.819$

$\Delta G = +1^{\circ}$

Juli VII

$H_a = 43$

$H_b = 44.4$

$h_t = 1.8$

$h_a = 10.7$

$h_d = 10.3$

$h_r = 1.3$

Datum	Luftdruck P			Lufttemperatur T						Relative Feuchte U			Richtung und Stärke des Windes D,F			Sicht	Bewölkung und Wetter N,w			Niederschlag R	Schneehöhe h <sub>s</sub>	Witterungsverlauf W		
	8	14	19	8	14	19	Max	Min	8	14	19	8	14	19	14	8	14	19						
1	07.4	07.5	07.5	13.0	16.5	15.2	17.1	11.9	94	86	96	00	0	28	1	24	1	8	10 -	9 -	9 -	4.2		• n, -° - a, p
2	09.6	11.7	11.4	15.9	13.7	14.6	16.6	13.1	92	94	92	00	0	18	3	30	3	6	10 -	10 -	7 -	1.4		-° - n, - a, p
3	10.7	10.3	10.3	15.8	21.9	19.2	22.7	12.9	86	66	77	00	0	26	2	20	0	9	0 -	6 -	9 -	2.3		- n, - o a, - o p
4	06.9	05.0	03.4	18.1	25.7	25.5	26.9	15.2	94	59	50	00	0	28	1	14	3	9	4 -	4 -	5 -	0.0		° - n, - o a, p
5	04.9	05.1	04.7	20.6	27.7	26.1	28.2	16.4	70	53	54	00	0	20	2	20	0	9	8 -	4 -	9 -			° - n, - o a, p
6	09.8	11.5	12.4	15.3	20.4	19.7	26.8	14.8	94	66	66	00	0	18	3	18	2	9	10 -	5 -	3 -	6.0		- n, -° - a, p
7	11.5	09.2	08.4	15.4	25.0	25.2	26.7	13.5	86	62	61	25	1	38	1	00	0	9	2 -	1 -	0 -	1.1		- o a, a, -° o p
8	36.5	08.0	07.9	20.2	22.1	20.6	26.2	16.2	71	74	77	00	0	14	2	24	2	9	1 -	8 -	9 -	2.9		- c n, t° - o a, - o p
9	02.1	99.9	96.5	18.0	18.2	17.2	21.0	16.2	92	91	94	00	0	20	1	20	1	7	9 -	10 -	10 -	0.0		- n, - o a, - ° p
10	92.6	94.9	94.2	16.3	16.7	17.3	19.5	14.8	96	91	83	16	2	26	1	28	1	8	10 -	9 -	1 -	17.7		• ~ n, a, o 19
11	94.7	95.9	97.0	13.3	13.6	13.4	17.8	13.0	94	90	96	30	3	28	2	28	2	8	10 -	10 -	10 -	1.6		- n, - a, p
12	97.7	98.3	98.3	10.8	13.6	13.6	15.7	10.3	90	84	83	00	0	30	3	50	4	9	9 -	9 -	9 -	10.0		° - n, -° - o a, -° o p
13	99.0	98.4	97.7	13.7	16.5	15.1	19.2	12.5	90	83	88	30	1	30	2	26	1	9	9 -	9 -	9 -	2.9		o a, p
14	96.4	99.9	01.2	12.7	11.8	11.3	15.6	11.5	91	94	93	14	2	28	2	14	2	6	9 -	10 -	10 -	9.9		• n, a, - p
15	02.5	02.7	03.1	12.2	16.0	14.2	17.2	10.1	91	78	92	14	3	14	4	18	3	9	10 -	9 -	10 -	7.1		° - o - n, t° - o a, - ° - o p
16	08.0	10.7	12.0	13.9	16.1	16.0	18.1	11.9	84	82	79	00	0	26	1	30	2	9	9 -	9 -	4 -	5.6		t° - o n, - a, - o p
17	16.5	16.4	15.7	13.0	18.8	16.0	19.5	11.7	91	81	87	30	1	28	2	28	2	9	10 -	9 -	9 -			- o ° - n, - o - o a, - ° o p
18	14.5	13.5	13.3	13.4	18.9	17.5	21.3	12.8	97	86	86	00	0	26	2	26	1	9	9 -	1 -	1 -	0.0		° - o ° - n, - a, - o ° a, - o ° p
19	12.4	11.5	10.4	14.0	18.4	17.8	19.6	13.3	97	90	82	00	0	26	2	26	1	7	10 -	8 -	0 -	0.1		° - o ° - o - n, - o - o a, - o - o p
20	08.8	07.3	05.4	14.2	20.5	19.6	22.4	12.9	93	76	67	00	0	28	2	30	3	9	10 -	9 -	0 -			- o - n - n, - o - o a, - o - o p
21	05.5	05.1	04.3	14.6	21.0	21.5	22.9	12.3	90	78	70	00	0	26	2	20	1	9	10 -	1 -	1 -			- o - n, - o - o a, - o - o p
22	05.3	05.8	05.5	14.8	19.4	18.2	21.2	13.7	91	86	86	00	0	26	1	00	0	9	1 -	1 -	2 -			- o ° - n, - o - o a, - o - o p
23	05.9	05.8	05.7	14.0	19.3	16.5	19.8	12.6	96	81	82	00	0	28	1	26	1	8	10 -	9 -	0 -			- o - o - n, - o - o a, - o - o p
24	07.2	06.8	10.2	12.4	16.1	12.6	16.9	9.9	85	62	70	04	2	30	4	32	4	10	7 -	1 -	1 -			- o - o - n, - o - o a, o p
25	13.8	14.8	14.8	11.7	16.3	14.1	17.5	8.3	78	67	66	02	1	26	2	30	2	10	1 -	1 -	0 -			o, n, a, p
26	13.4	12.9	10.7	12.3	14.8	14.3	16.7	8.6	86	59	67	00	0	18	3	18	2	9	10 -	10 -	9 -			o - o - n, - o - o a, - o - o p
27	04.5	03.2	03.6	15.8	22.0	20.2	22.7	11.6	77	56	78	00	0	10	3	14	1	7	9 -	10 -	9 -	0.1		- o ° - n, - o - o a, - o - o p
28	05.4	06.2	06.6	15.3	16.8	15.8	20.5	14.8	92	85	92	18	1	30	1	00	0	7	10 -	10 -	10 -	1.9		- o - o - n, - o - o a, - o - o p
29	08.3	09.1	09.7	16.7	18.2	17.0	18.8	14.5	85	84	84	12	1	26	1	30	1	7	9 -	9 -	1 -	4.8		- o - o - n, - o - o a, - o - o p
30	12.7	13.2	13.8	14.6	21.0	17.6	21.2	13.6	90	73	82	30	1	26	2	30	3	9	10 -	1 -	9 -	0.1		- o - o - n, - o - o a, - o - o p
31	16.1	16.6	16.8	13.8	21.4	19.4	22.3	13.0	96	79	77	00	0	24	1	26	1	9	10 -	1 -	0 -			o - o - n, - o - o a, - o - o p
M	06.8	07.1	06.8	14.7	18.7	17.5	20.6	12.9	89	77	79	0.6		1.9		1.6	8.4	7.8	6.5	5.4	77			

August VIII

1	18.8	18.9	18.3	14.1	21.3	18.6	22.5	13.5	97	77	79	00	0	26	1	26	1	9	10 -	1 -	1 -			- o - o - n, - o - o a, - o - o p
2	18.6	18.0	17.4	12.3	22.0	19.5	21.9	11.6	97	77	75	00	0	28	1	28	1	8	10 -	1 -	1 -			- o - o - n, - o - o a, - o - o p
3	20.1	20.7	20.9	13.5	20.6	17.9	21.4	12.1	94	74	91	00	0	28	1	25	1	9	1 -	0 -	0 -			- o - o - n, - o - o a, - o - o p
4	24.1	25.1	25.1	13.3	18.8	16.8	19.4	12.8	96	77	76	00	0	26	2	26	1	9	10 -	0 -	0 -			- o - o - n, - o - o a, - o - o p
5	24.1	22.1	21.1	14.1	21.4	17.1	21.3	11.6	86	72	93	30	1	28	2	26	1	9	0 -	1 -	0 -			- o - o - n, - o - o a, - o - o p
6	20.0	18.0	16.8	13.1	19.9	17.8	20.2	12.6	94	75	81	30	1	28	3	26	2	9	10 -	1 -	1 -			- o - o - n, - o - o a, - o - o p
7	14.8	13.9	12.6	13.0	20.4	16.6	21.1	12.0	96	75	86	00	0	26	2	24	2	9	0 -	0 -	1 -			- o - o - n, - o - o a, - o - o p
8	10.3	08.8	06.7	13.6	15.5	15.7	16.6	12.9	90	86	85	00	0	30	1	32	1	8	10 -	9 -	1 -			- o - o - n, - o - o a, - o - o p
9	03.3	01.9	00.6	15.0	17.4	17.0	18.7	12.4	91	87	88	02	1	18	4	20	1	7	7 -	10 -	9 -	0.0		- o - o - n, - o - o a, - o - o p
10	98.7	00.0	00.3	15.4	16.8	16.2	17.6	12.7	85	76	83	18	2	20	2	20	3	10	9 -	9 -	9 -	0.0		- o - o - n, - o - o a, - o - o p
11	96.9	99.8	00.3	16.8	16.0	14.1	15.9	13.9	94	91	93	19	4	18	1	00	0	6	10 -	10 -	9 -	22.3		- o - o - n, - o - o a, - o - o p
12	02.6	03.2	05.1	14.1	13.6	12.2	15.8	12.0	86	87	90	22	3	20	2	26	2	8	8 -	9 -	9 -	22.6		- o - o - n, - o - o a, - o - o p
13	07.3	07.8	06.5																					

# Extenso-Tabelle

1944

Bergen (Fredriksberg)

$\varphi = 60^\circ 24' N$

$\lambda = 5^\circ 19' E$

$g = 9.819$

$\Delta G = +1^\circ$

September IX

$H_s = 43$

$H_b = 44.4$

$h_t = 1.8$

$h_a = 10.7$

$h_d = 10.3$

$h_r = 1.3$

Datum	Luftdruck P			Lufttemperatur T						Relative Feuchte U			Richtung und Stärke des Windes D,F			>	Bewölkung und Wetter N,w			Niederschlag R	Schneehöhe h <sub>s</sub>	Witterungsverlauf W	
	8	14	19	8	14	19	Max	Min	8	14	19	8	14	19	14	8	14	19					
1	87.5	91.7	95.1	11.0	14.1	13.6	14.6	10.4	94	92	84	00	0	26	1	26	1	9	10 -	9 -	9 -	20.4	
2	93.0	93.4	92.3	11.5	16.5	15.1	17.7	9.5	92	74	84	00	0	26	1	32	1	9	9 -	9 -	10 -	0.6	
3	96.8	96.7	95.0	12.4	14.8	12.2	15.4	11.7	91	75	91	00	0	26	1	00	0	9	10 -	9 -	9 -	0.9	
4	94.3	96.4	97.1	11.6	13.2	12.5	14.0	10.6	87	82	84	10	2	18	3	14	3	9	8 -	9 -	9 -	3.8	
5	93.0	93.2	92.5	12.1	14.9	13.5	16.0	9.4	78	72	73	30	3	30	1	30	1	9	9 -	9 -	9 -	0.6	
6	92.0	96.5	00.3	9.9	14.2	10.5	16.0	8.1	90	76	77	00	0	28	4	30	3	10	1 -	4	8 -		
7	05.4	04.1	02.5	9.5	13.1	11.3	14.4	7.4	90	68	81	14	1	28	2	30	2	10	9 -	9 -	9 -	0.5	
8	88.8	87.6	90.1	8.9	11.6	10.8	13.5	8.9	94	90	94	32	2	00	0	15	2	8	10 -	10 -	10 -	4.5	
9	97.6	00.9	04.6	9.4	11.3	9.8	11.8	9.2	93	77	76	32	4	30	4	30	4	9	10 -	9 -	2 -	7.8	
10	13.6	15.2	15.2	8.2	9.7	9.5	9.8	6.8	84	88	94	00	0	16	1	00	0	7	10 -	10 -	10 -	0.6	
11	20.1	22.6	24.4	10.2	12.9	11.4	13.4	9.2	96	74	84	00	0	30	2	00	0	9	9 -	7 -	1 -	8.5	
12	28.0	25.6	27.9	8.8	15.5	12.4	16.4	6.9	96	67	78	00	0	30	2	28	1	10	9 -	9 -	1 -	3.1	
13	26.6	25.4	24.7	8.5	16.4	15.2	16.9	6.9	94	67	78	00	0	18	3	23	1	9	0 -	1 -	9 -	0.1	
14	22.3	20.8	19.1	13.2	16.5	15.3	17.2	10.9	77	59	61	12	3	14	3	16	2	9	1 -	9 -	7 -		
15	15.0	12.5	11.8	14.5	14.0	15.9	16.0	12.4	64	77	73	14	3	14	4	16	5	7	10 -	10 -	10 -		
16	09.0	09.6	10.2	15.4	14.7	13.1	16.7	13.1	87	92	93	14	4	16	3	16	4	8	10 -	10 -	10 -	8.5	
17	15.3	19.4	21.0	12.8	14.0	11.7	14.2	11.0	97	81	94	26	1	24	1	10	2	8	10 -	10 -	10 -	8.8	
18	22.4	22.7	25.1	12.8	15.7	14.1	16.7	11.5	85	79	88	10	3	18	2	14	3	9	9 -	9 -	9 -	4.4	
19	22.8	21.5	20.1	11.1	18.8	14.1	19.1	10.1	96	68	85	00	0	14	3	00	0	9	6 -	2 -	9 -	0.1	
20	16.2	14.9	15.6	12.0	16.2	15.5	17.0	11.2	91	68	86	00	0	22	3	14	1	8	10 -	9 -	9 -		
21	18.6	20.1	19.3	13.6	15.1	13.4	15.3	12.2	78	73	79	14	3	15	3	00	0	8	10 -	10 -	7 -		
22	14.1	10.6	08.7	11.6	19.1	16.6	19.8	8.9	90	56	57	00	0	12	3	10	3	7	8 -	9 -	10 -	0.1	
23	01.8	99.6	99.2	14.4	12.8	11.0	16.8	10.9	65	85	97	12	3	14	3	30	1	6	10 -	10 -	10 -	0.1	
24	00.7	01.4	01.3	9.7	11.5	10.7	11.9	9.4	96	78	90	00	0	30	2	28	2	8	9 -	10 -	9 -	27.4	
25	00.1	97.9	93.6	9.5	11.0	9.8	11.4	8.8	90	85	84	32	1	00	0	16	3	9	9(+) -	10 -	10 -	1.1	
26	84.1	85.8	83.9	9.9	8.5	6.8	10.7	6.5	85	85	92	28	2	26	2	16	2	8	8 -	9 -	10 -	10.7	
27	82.4	83.4	89.0	7.6	7.7	5.8	10.3	9.0	92	88	94	16	3	18	3	14	1	3	8 -	10 -	9 -	17.9	
28	01.7	05.1	06.3	6.4	9.2	6.7	9.3	5.7	92	78	84	32	1	26	2	14	2	9	9 -	6 -	3 -	31.8	
29	96.6	95.1	93.2	10.0	12.1	11.6	12.6	6.6	94	97	96	14	5	14	5	22	4	4	10 -	10 -	10 -	16.3	
30	97.9	01.3	02.6	7.9	8.7	7.0	11.7	6.7	87	83	82	30	1	27	2	29	2	9	9 -	9 -	5(+) -	49.2	
M	05.7	06.1	06.3	10.8	13.5	11.8	14.6	9.2	88	78	84	1.5	2	2.3	1	1.9	8.2	8.3	8.5	8.1	228		

## Oktober X

1	03.3	05.0	06.8	4.8	9.5	6.8	9.5	4.5	92	76	93	10	1	26	1	14	1	10	9 -	9 -	9 -	8.1	
2	11.0	09.7	05.9	6.1	8.0	7.3	8.9	5.9	92	82	75	00	0	14	3	14	4	9	9 -	9 -	2 -	17.2	
3	99.6	01.5	04.4	8.5	13.4	9.6	13.5	6.9	86	66	74	12	3	00	0	30	2	10	9 -	9 -	2 -	6.7	
4	14.2	17.0	18.1	7.5	13.6	9.2	13.9	6.9	86	00	0	0	0	0	0	0	0	10	5 -	1 -	4 -	0.1	
5	19.3	21.3	21.4	8.6	8.4	9.1	9.7	7.1	88	98	99	00	0	12	3	10	2	3	2 -	10 -	10 -		
6	21.5	20.8	18.7	9.6	10.5	9.1	10.8	8.8	99	97	97	10	1	16	2	10	2	4	10 -	10 -	10 -	7.3	
7	14.5	12.6	11.7	10.0	11.4	10.7	11.6	9.1	99	99	99	10	1	10	1	26	1	4	10 -	10 -	10 -	2.2	
8	08.7	10.6	12.1	10.3	11.7	8.3	11.7	8.1	99	70	82	30	2	30	3	32	2	9	10 -	3 -	1 -	6.7	
9	12.0	11.8	11.7	4.9	12.6	7.9	12.6	4.4	92	61	85	00	0	23	2	00	0	9	9 -	9 -	1 -	0.2	
10	09.2	07.3	05.2	9.2	13.2	9.5	13.2	6.4	78	62	77	14	2	12	2	00	0	9	9 -	1 -	9 -		
11	02.0	01.4	00.6	8.4	9.9	9.9	10.5	8.1	96	93	92	00	0	26	1	16	4	5	10 -	10 -	10 -	6.5	
12	94.5	96.3	96.8	12.6	13.2	12.6	13.6	9.6	73	67	74	12	4	14	6	14	5	4	10 -	9 -	10 -	3.5	
13	92.7	90.9	93.8	14.5	11.0	8.9	13.5	8.9	89	93	92	14	3	14	3	12	4	4	10 -	10 -	10 -	0.2	
14	90.4	86.6	84.2	11.4	13.6	11.1	14.3	8.2	80	57	81	10	2	22	10	4	2	9	10 -	9 -	10 -	20.9	
15	92.9	95.4	96.1	9.8	8.4	7.7	12.5	7.7	81	87	86	16	3	14	4	13	4	9	9 -	9 -	9 -	10.7	
16	96.0	94.5	93.4	8.4	13.3	8.9	13.3	6.4	82	71	75	14	3	12	2	00	0	8	4 -	1 -	0 -	14.9	
17	83.0	77.7	75.4	9.3	10.2	10.1	11.5	7.1	85	92	91	00	0	14	4	15	4	8	10 -	10 -	9 -	1.2	
18	67.7	70.3	73.9	7.9	8.8	9.2	10.4	7.9	94	94	92	12	4	12	3	15	3	6	10 -	10 -	4(+) -	15.2	
19	82.5	89.2	95.8	8.4	8.4	7																	

# Extenso-Tabelle

1944

Bergen (Fredriksberg)

$\phi = 60^{\circ} 24' N$

$\lambda = 5^{\circ} 19' E$

$g = 9.819$

$\Delta G = +1^{\circ}$

November XI

$H_a = 43$

$H_b = 44.4$

$h_t = 1.8$

$h_a = 10.7$

$h_b = 10.3$

$h_r = 1.3$

Datum	Luftdruck P				Lufttemperatur T						Relative Feuchte U			Richtung und Stärke des Windes D,F			> Sicht			Bewölkung und Wetter N,w			Niederschlag K	Schnellhöhe h <sub>s</sub>	Witterungsverlauf W
	8	14	19	8	14	19	Max	Min	8	14	19	8	14	19	14	8	14	19							
1	06.6	06.8	06.5	4.4	6.7	4.6	6.7	2.5	90	68	66	29	2	31	3	31	2	10	1 -	0	0		12.8		
2	04.6	03.7	02.4	2.7	10.3	4.5	10.3	2.3	76	72	77	14	1	00	0	00	0	5	1 -	0	0		15.2		
3	95.3	91.6	88.6	2.4	6.6	6.1	6.6	1.5	79	67	73	00	0	14	3	16	3	7	1 -	9 -	10 -		9.8		
4	86.4	87.2	83.5	3.3	4.4	5.3	6.1	1.9	92	99	87	10	3	12	3	14	5	8	4 -	3(i)	9 -				
5	75.8	74.8	77.1	8.1	6.0	4.7	10.9	4.7	73	91	88	16	3	14	2	18	2	7	10 -	9 +	9 +				
6	84.7	85.1	85.0	3.7	5.8	5.0	6.9	2.6	90	81	81	24	3	12	3	17	4	7	9 △	9 △	5 △		9.2		
7	81.1	82.3	85.7	2.1	6.4	3.9	6.4	1.7	93	65	63	00	0	00	0	00	0	10	1 -	1	0		6.7		
8	90.8	89.0	87.7	- 0.1	5.4	2.7	5.4	- 0.2	88	74	82	14	2	14	1	12	1	4	1 -	8 -	2 -				
9	87.5	90.1	96.0	1.0	1.1	0.5	2.8	- 0.2	88	91	26	1	10	2	28	1	6	10 +	10 -	0 -		0.0			
10	08.9	12.2	14.1	1.8	5.7	2.9	5.7	- 0.3	90	84	87	00	0	00	0	00	0	10	9 -	1	0 -		1.9		
11	18.4	19.4	17.9	3.4	5.1	2.4	5.1	1.0	82	73	76	32	1	30	1	00	0	10	0	0	0				
12	11.9	11.0	10.8	3.2	7.3	5.7	7.9	0.0	68	61	66	00	0	00	0	25	1	10	3 -	7	1 -				
13	02.5	04.2	06.5	4.3	11.3	9.4	12.4	3.7	57	56	57	02	4	28	3	02	5	9	9 -	10 -	10 -		0.0		
14	09.5	06.9	08.1	7.5	7.0	4.9	9.4	4.8	55	56	25	02	4	02	4	02	4	9	9 -	10 -	10 -				
15	10.9	12.2	13.5	5.4	7.0	5.7	7.0	4.3	54	53	22	05	4	02	4	02	4	9	9 -	10 -	10 -				
16	17.2	19.0	19.6	3.9	4.5	2.4	5.8	2.2	54	59	62	30	2	18	1	00	0	7	1 -	1	9 -				
17	19.5	17.3	11.9	2.3	3.1	1.8	3.1	0.5	60	57	59	19	1	28	1	28	1	9	10 -	0	1				
18	97.7	97.4	98.1	4.7	4.2	4.4	5.1	0.1	62	64	75	10	3	06	2	26	2	8	10 -	9 -	10 -		1.4		
19	94.1	88.4	84.4	6.7	4.8	5.3	7.1	4.1	73	93	91	14	2	00	0	02	3	6	10 +	10 -	10 -		0.1		
20	82.4	82.7	85.3	4.0	5.6	3.8	5.6	3.5	96	87	90	30	2	28	1	32	2	9	10 -	9 -	12.1				
21	98.7	04.5	06.7	3.7	2.3	1.0	5.0	0.8	82	88	96	30	4	32	2	32	1	6	1 -	7	1 -		0.7		
22	05.0	00.0	96.3	0.7	3.1	2.4	3.1	0.2	78	72	63	14	1	10	1	12	3	4	8 -	1 -	1 -		0		
23	81.8	78.8	78.0	5.0	7.3	6.9	8.0	2.1	76	76	93	14	2	06	2	26	1	9	10 +	10 -	10 -		0.1		
24	77.8	77.6	77.9	5.2	5.7	4.4	7.6	4.4	86	87	91	15	4	20	3	16	5	8	9 -	9 +	9 +		4.4		
25	75.9	77.2	80.4	3.5	4.4	4.9	4.9	2.2	94	87	75	13	4	12	4	00	0	8	9 +	9 +	8 -		10.0		
26	89.5	94.4	98.7	2.8	3.5	2.0	4.9	- 1.7	87	79	79	30	3	30	2	32	1	10	5	1	0		0.9		
27	11.4	14.0	14.2	- 0.6	2.4	2.1	2.4	- 1.4	74	76	79	14	1	30	1	12	3	6	1 -	9 -	9 -				
28	02.3	94.7	90.4	5.9	7.1	8.0	8.0	1.8	74	76	79	14	6	14	6	14	5	9	10 +	10 -	10 -		0.0		
29	00.1	00.8	00.9	6.2	5.8	6.8	8.5	5.1	90	93	94	13	4	13	5	14	5	7	9 -	9 +	10 +		10.9		
30	03.5	05.8	07.1	7.7	6.9	6.9	7.9	6.7	96	97	84	16	4	20	3	20	1	4	9 +	10 +	7(4)		11.1		
M	97.7	97.6	97.7	3.9	5.6	4.4	6.6	2.1	80	76	77	2.3	2	2.2	2	2.2	2	7.7	6.3	6.3	5.2	107	0		

Dezember XII

1	04.3	01.4	95.5	7.0	7.7	7.4	8.4	5.8	97	97	97	13	4	14	5	14	5	5	10 +	10 +	10 +	9.9			
2	78.4	81.1	84.9	6.0	3.5	3.2	9.1	3.2	94	96	93	00	2	08	1	10	1	7	10 +	9 +	9 +	33.4			
3	86.7	86.0	84.5	0.9	1.8	0.8	3.9	- 0.1	99	98	98	08	2	08	1	10	1	8	8 +	8 +	9 +	19.8			
4	79.7	79.7	79.7	- 0.4	0.4	0.7	0.8	- 1.4	96	95	88	00	0	00	0	14	1	2	4 -	8 =	10 =	10.6	1		
5	80.0	81.2	81.8	2.7	1.1	0.1	3.1	0.0	66	72	82	28	1	14	2	00	0	5	9 -	1 -	3	1	1		
6	80.6	83.2	82.0	2.4	2.5	3.3	3.7	0.0	85	94	77	00	0	14	4	15	3	8	9 +	9 +	9(1)	0.0	1		
7	77.9	78.4	78.4	3.3	4.4	3.9	6.4	2.5	83	75	77	14	2	08	1	14	2	7	9 +	9 +	8 +	2.4	0		
8	80.7	81.3	80.0	3.6	3.5	6.2	6.9	2.6	76	76	84	08	1	08	2	07	5	7	9 +	10 +	10 -	0.1			
9	89.3	86.8	86.8	4.3	4.5	3.8	6.9	3.1	74	78	79	32	1	00	0	26	1	6	10 +	9 -	10 -	2.4			
10	83.1	83.2	85.5	2.4	3.3	3.8	4.0	1.9	95	86	77	14	4	14	5	13	3	9	10 +	9 -	1 -	1.5			
11	88.0	90.3	92.0	4.5	4.8	6.0	6.2	3.7	72	75	76	12	4	12	1	06	4	5	10 +	10 +	10 +	1.3			
12	97.8	01.2	04.7	1.8	1.4	- 0.4	6.1	- 0.5	67	77	95	16	2	00	0	00	0	4	4 +	1 -	1 -				
13	15.5	18.1	20.7	- 1.1	0.5	- 0.4	1.0	- 1.2	96	92	93	00	0	00	0	00	0	5	7 +	0 -	0 -				
14	24.2	23.9	22.4	2.3	3.5	4.0	4.5	- 2.2	70	65	86	12	2	12	3	12	3	9	2 +	7 -	4 -				
15	17.8	16.3	15.6	3.6	2.9	0.3	4.7	0.3	64	62	89	12	1	08	2	06	4	9	4 -	2 -	3 -				
16	13.8	12.4	10.4	- 3.0	- 0.6	- 1.0	0.9	-																	

# Extenso-Tabelle

1944

## Trondheim (Voll)

$\varphi = 63^\circ 25' N$   $\lambda = 10^\circ 27' E$   $g = 9.821$   $\Delta G = +1^h$

Januar I

$H_a = 127$   $H_b = 133.0$   $h_t = 2.0$   $h_s =$   $h_d = 11.2$   $h_r = 1.3$

Datum	Luftdruck P			Lufttemperatur T					Relative Feuchte U			Richtung und Stärke des Windes D,F			Sicht	Bewölkung und Wetter N,w			Niederschlag Z	Schneehöhe H <sub>s</sub>	Witterungsverlauf W			
	8	14	19	8	14	19	Max	Min	8	14	19	8	14	19		14	8	14	19					
1	68.6	70.4	76.0	0.0	-1.0	-2.8	0.5		93	95	90	32	3	32	1	00	0	10	10	2	11.0	20	* n,a ** n,a, * a,p	
2	74.3	69.6	65.8	-2.6	-2.2	-3.4	-1.5		93	94	90	00	08	1	06	0	10	10	10	10	4.6	25		
3	69.4	73.5	80.8	-5.4	-9.0	-10.0	-3.4		91	75	82	08	1	00	0	08	1	10	10	10	6.6	50	* n, * a	
4	91.5	95.3	90.2	-10.2	-1.8	0.0	0.0		86	93	91	16	3	00	0	24	1	10	10	10	0.2	30	* a,p + p	
5	99.2	84.5	76.4	-1.4	-1.8	3.0	3.0		86	68	80	20	4	16	2	20	4	4	10	10	3.2	35		
6	61.8	59.5	63.0	1.8	2.4	2.6	3.0		97	86	85	20	5	20	4	24	5	10	4	10	23.0	15	* n,a,p	
7	77.7	83.7	82.9	-1.0	-1.4	-2.0	2.6		80	87	86	00	0	20	1	24	1	5	10	8	7.0	15	* p	
8	79.7	76.3	72.5	-5.0	-4.4	-4.4	-2.0		90	90	76	20	5	16	2	20	5	5	10	8	7.6	20	* + n, * a, * p	
9	69.5	72.2	74.0	-11.2	-8.4	-12.0	-4.4		75	75	60	0	08	1	00	0	0	0	0	0	0	2.4	20	o a
10	79.3	81.3	82.4	-16.2	-14.4	-5.6	7.5		83	74	93	16	1	00	0	16	4	1	4	5	10.4	20	c a, * p	
11	89.1	92.9	96.5	0.4	0.0	-1.6	0.7		64	63	91	20	2	16	3	24	3	6	8	5	3.2	20	* n, * a, * p	
12	99.8	92.4	91.4	-2.2	-2.8	-4.0	-1.6		73	91	90	24	3	00	0	30	0	10	7	2	2.0	25	* n, * a	
13	95.9	93.6	85.3	-4.8	-2.4	0.4	0.5		71	70	68	00	0	08	1	04	4	10	9	4	0.5	25		
14	81.6	86.5	92.1	2.2	2.6	1.8	2.6		90	83	90	20	5	16	3	20	3	10	6	0	2.4	25	* n, * p	
15	95.8	90.0	91.6	5.6	6.4	6.2	7.5		90	70	73	16	4	20	7	20	7	10	7	0	10.4	15	* n, * p	
16	97.8	88.3	86.3	4.4	6.0	4.0	6.2		53	88	90	24	5	20	1	20	1	10	9	10	1.8	10	* \ n, ** p	
17	97.0	96.0	90.8	4.8	4.4	0.4	5.5		71	70	82	24	3	08	1	00	0	8	8	0	2.0	5	* n	
18	97.9	96.7	93.2	4.2	3.8	4.4	4.7		86	84	73	20	4	16	1	00	0	5	6	0	0.5	5	o a	
19	94.5	96.3	97.1	4.0	3.0	1.0	4.4		95	80	73	24	4	16	2	00	0	6	** 4	0	0.7	5	* n	
20	96.5	95.9	92.5	2.4	3.2	-0.4	3.3		60	52	62	16	3	16	3	16	1	0	0	0	0	0	o a	
21	76.3	75.7	75.1	2.2	2.4	1.2	2.5		58	57	57	16	4	16	4	16	4	9	7	0	0.14			
22	70.8	61.4	56.9	1.6	2.0	4.2	4.2		65	90	65	20	4	20	6	16	5	10	7	2	0.0	3	** n, * a,p	
23	58.5	57.6	57.3	0.2	2.4	0.8	4.2		65	60	64	00	0	16	1	16	2	0	1	0	1.0	1.0		
24	70.7	75.7	75.7	-0.2	-0.4	-1.4	0.8		90	78	83	24	4	24	4	24	3	10	7	10	0.1	3	** n, * a	
25	70.2	69.5	68.2	-1.2	-0.6	-2.0	-0.6		57	56	56	00	0	16	3	16	1	10	9	10	0.4	3		
26	77.4	85.1	85.7	-1.8	0.0	-0.4	0.3		80	73	74	24	4	24	2	20	3	10	** 4	1	0.0	3	** - n, ** a	
27	70.0	64.0	64.2	2.4	3.4	2.4	3.9		66	60	85	16	5	16	4	20	3	10	10	10	0.2	3	** n, * a, * p	
28	72.0	80.5	86.3	0.8	0.4	0.8	2.4		92	92	91	24	3	20	4	24	3	10	4	10	7.4	3	** n, * a, * p	
29	91.5	84.3	76.7	0.8	2.4	2.4	2.9		88	70	86	24	4	24	3	20	5	5	10	10	10	4.4	6	* n, * a, * p
30	85.5	88.7	94.3	1.0	1.0	0.6	2.4		83	85	71	24	7	24	6	24	6	10	9	5	5.8	3	** \ n, * a,p	
31	94.7	87.7	83.2	0.2	0.4	1.2	1.2		70	93	93	16	1	00	0	20	3	9	10	10	0.8	3	** n, * a, * p	
M	83.0	83.0	82.7	-0.8	-0.1	-0.4	1.6		80	77	80	24	2	20	2.3	2.5	2.5	7.5	6.8	5.0	109	13		

Februar II

1	82.7	77.5	69.0	2.2	4.4	5.4	5.4		84	70	66	16	2	16	2	16	4	8	10	10	8.6	10	* n * n, * a,p	
2	76.9	80.6	79.9	2.0	0.6	0.0	5.4		84	90	90	24	5	24	3	32	4	9	6	*	1.6			
3	65.3	62.1	60.6	-0.2	0.6	0.8	1.5		70	94	80	00	0	12	1	04	1	10	*	9	3	0.8		* n,a
4	69.6	75.6	85.0	-0.4	0.5	0.2	0.8		90	93	91	16	2	24	1	24	1	10	*	5	10	2.2		* n,a,p
5	94.6	99.3	93.1	-2.0	-2.2	-2.4	0.2		88	90	90	28	2	24	2	16	2	5	4	8	4.6	10	* n, * a,p	
6	90.7	95.0	88.9	0.0	1.0	1.2	1.2		80	67	62	16	4	16	3	16	4	10	10	10	3.3	15	** n	
7	68.2	58.6	51.4	3.4	5.4	4.4	5.5		71	61	56	20	5	16	6	16	6	10	1	8	1.2	7	** n, o a	
8	63.7	74.3	76.2	2.0	-0.8	-2.0	-4.4		92	85	85	20	5	24	4	16	4	10	*	10	10	11.0	3	** n, * a, * p
9	79.7	79.9	81.3	-1.2	-2.0	-2.6	-1.1		91	87	90	20	5	16	3	28	3	8	7	2	6.0	10	* n, * a, * p	
10	89.7	93.2	96.8	-3.4	1.6	0.8	1.6		86	89	90	26	4	16	2	24	1	9	10	10	0.0	12	** n, * a,p	
11	96.9	97.7	99.2	0.0	-0.2	-0.2	0.8		93	94	94	24	1	24	1	00	0	10	*	10	10	0.6	13	* n, * a, ** p
12	93.1	95.6	97.6	0.4	1.2	1.0	1.3		92	92	92	24	2	30	0	00	0	10	*	10	10	0.3	15	** n, * a, * p
13	10.5	10.8	17.3	0.6	2.4	1.0	2.7		91	74	70	09	1	16	3	16	1	10	*	0	0	2.2	15	o a,p
14	97.4	11.5	13.0	-5.8	-1.8	-2.4	-1.5		67	61	64	00	0	00	0	00	0	0	0	0	0	0	15	o a,p
15	11.6	88.9	64.6	-6.6	-2.2	-4.0	-2.2		75	74	66	08	1	00	0	12	1	0	2	0	0	0	15	o a,p
16	93.1	93.8	95.3	1.4	1.8	1.4	1.9		62	60	60	16	7	20	2	16	4	0	0	3	15	o a,p		
17	14.2	17.5	17.9	-0.4	1.6	1.4	1.9		71	67	66	16	2	20	2	16	1	8	9	4	15	15	o a,p	
18	19.7	19.3	20.0	-2.8	1.8	0.0	1.9		72	64	63	16	1	12	2	16	2	0	1	0	15	15	o a,p	
19	19.9	18.8	18.5	-7.8	-3.2	-5.4	0.0		76	70	67	16	1	00	0	16	2	0	0	3	15	o a,p		
20	19.0	19.0	19.9	-1.6	2.6	1.0	2.6		85	70	70	20	4	20	5	20	6	2	10	10	10	15	t a,p	
21																								

# Extenso-Tabelle

1944

**Trondheim (Voll)**

$\varphi = 63^\circ 25' N$

$\lambda = 10^\circ 27' E$

$g = 9.821$

$\Delta G = + 1^h$

**März III**

$H_s = 127$

$H_b = 133.0$

$h_t = 2.0$

$h_a =$

$h_d = 11.2$

$h_r = 1.3$

Datum	Luftdruck P			Lufttemperatur T					Relative Feuchte U			Richtung und Stärke des Windes D,F			> Sicht	Bewölkung und Wetter N,w			Niederschlag R	Schnethöhe h	Witterungsverlauf W		
	8	14	19	8	14	19	Max	Min	8	14	19	8	14	19		14	8	14	19				
1	64.6	63.4	62.9	-2.4	0.6	-1.2	0.8		61	57	55	16	3	00	0	00	0	5	6	0 -	0.0	10	+ n, o p
2	63.2	64.3	65.9	-7.2	-3.0	-4.4	-1.2		65	60	62	00	0	00	0	16	1	2	0	2 -	1.6	7	o p
3	65.0	67.3	69.9	-0.4	1.0	1.0	1.2		90	90	90	24	2	24	6	24	7	10	7	7 -	10 -	15	+ n, a, s \ p
4	81.4	82.2	86.2	-2.6	-1.8	0.2	1.0		87	91	85	24	5	20	7	24	2	7	10	10 -	5	8.8	+ n, a, p
5	97.4	99.0	91.1	-0.8	1.0	2.0	2.0		90	88	90	20	6	20	6	16	6	10	10	10 -	10	20	+ n, s p
6	10.3	13.6	16.6	2.8	4.0	4.0	4.6		87	85	87	20	4	16	3	20	6	10	10	10	10	10	+ n
7	23.0	24.0	25.1	2.8	4.2	3.6	4.6		91	90	84	16	2	20	2	16	1	9	9	9 -	2.6	10	+ n, + o a
8	23.4	22.3	19.3	1.4	4.0	2.8	4.4		88	81	87	16	1	16	1	20	2	9	10	10 -	0.0	4	+ p
9	07.8	00.7	94.3	3.4	3.4	4.8	5.6		91	93	93	16	1	00	0	16	4	10	10	10 -	10.3	15	+ n, a, + p
10	90.4	84.9	75.5	1.4	2.0	2.6	4.8		91	91	76	24	3	24	4	25	5	10	10	10 -	10.5	20	+ n, + a, + p
11	72.9	81.0	85.7	-0.4	2.6	1.8	2.8		91	86	88	24	4	24	1	24	3	10	10	10	10	5	+ n, + a
12	77.6	71.1	69.1	0.4	-0.2	-0.2	1.8		85	90	91	20	2	16	4	24	2	10	10	10 -	0.1	7	+ n, o a
13	64.5	66.7	70.5	-5.0	-0.6	-1.6	-0.2		81	71	76	00	0	00	0	00	0	0	0	0	2.0	7	+ n, o a
14	76.8	78.9	81.0	-4.2	0.6	0.4	0.6		90	90	91	16	1	00	0	00	0	8	19	10 -	0.0	5	+ n, + a, + p
15	89.3	91.4	92.5	-2.6	-0.4	-1.6	0.4		90	86	90	16	1	16	1	00	0	7	5	5 -	7.0	10	+ n, + a, o 14, + p
16	95.0	95.8	95.8	-7.8	-0.8	-5.0	-0.4		90	65	65	00	0	08	1	00	0	0	0	0	1.4	12	+ n, o a, p
17	95.7	95.4	96.0	-1.2	1.2	2.6	2.6		70	91	96	00	0	16	1	20	4	10	10	10 -	12	12	+ o a
18	89.6	93.1	92.6	1.8	2.6	1.0	3.2		66	90	87	00	0	16	2	16	2	10	3	5 -	0.0	9	+ n, + a, + p
19	70.5	71.0	77.2	3.8	2.8	0.0	4.0		63	78	75	16	4	00	0	20	4	10	10	10	8	8	+ n, + a, + p
20	86.0	85.7	86.7	-2.4	-1.0	-2.4	0.0		90	91	83	16	1	24	2	24	4	6	3	10	1.0	10	+ n, + a, + p
21	95.9	98.5	90.0	-1.8	-1.0	-2.0	-0.4		76	74	76	24	2	20	1	00	0	5	9	8 -	1.7	15	+ n
22	98.8	98.3	95.8	-4.0	-0.4	-1.2	0.0		88	84	93	16	2	00	0	16	3	10	10	10 -	0.2	15	+ o n, + a, + p
23	86.4	92.4	96.0	-2.6	-1.8	-3.6	-1.2		94	91	83	32	3	00	0	00	3	10	3	5 -	14.5	30	+ n, o a, p
24	95.4	99.4	10.3	-2.6	-1.0	-6.0	-1.0		86	63	77	32	1	08	1	16	1	6	0	0	0.2	30	+ n, o a, p
25	97.0	94.9	92.7	-2.8	-0.4	2.4	2.4		64	90	90	08	3	00	0	24	4	10	10	10 -	10	30	+ n, + a, + p
26	94.7	97.3	98.3	2.2	2.0	1.0	4.8		91	92	92	16	3	28	1	32	1	3	10	10 -	11.4	20	+ n, o a, + p
27	95.9	92.7	98.7	0.0	2.8	1.0	3.2		93	91	90	00	0	20	3	20	4	10	10	10 -	0.2	20	+ n, + a, + p
28	92.6	92.2	91.1	0.0	0.8	0.8	1.6		94	94	93	20	3	20	1	24	2	10	10	10 -	7.0	20	+ n, + a, + p
29	91.0	91.5	91.5	-3.2	-2.0	-4.0	0.8		92	87	85	32	1	08	1	08	1	10	8	6 -	11.8	30	+ n, + a, o p
30	90.3	90.0	89.5	-7.6	-4.0	-5.0	-3.8		84	70	70	00	0	04	1	00	0	6	1	5 -	0.2	30	o a, p
31	91.8	92.8	93.8	-12.5	-4.4	-6.0	-3.6		86	70	74	16	1	00	0	00	0	2	0	0	0	30	o a, p
M	90.8	91.3	91.7	-1.7	0.4	-0.4	1.5		84	82	83	1.9		1.6		2.2		7.6	6.8	6.5	111	12	

April IV

1	97.1	97.9	99.3	-10.0	1.6	-0.2	1.6		73	67	80	16	2	16	1	00	0	0	10	10 -	1.4	30	+ p
2	99.9	00.5	61.0	-2.6	1.2	-1.2	2.3		81	71	85	16	1	00	0	20	0	7	0	0	0.0	30	+ n, o a, o 19
3	02.7	02.8	02.4	-4.8	3.8	-0.2	3.8		74	60	55	16	2	00	0	12	3	0	0	0	0.0	30	+ a, p
4	03.3	02.1	01.9	-3.6	1.4	-0.6	1.5		66	65	70	00	0	32	2	00	3	0	0	0	0.0	30	o a, p
5	02.5	03.1	03.3	-8.6	2.2	1.0	3.3		78	60	58	04	2	20	0	00	0	0	0	0	0.0	30	+ n, o a, o 19
6	05.5	05.4	03.5	-3.2	3.2	0.6	4.5		76	64	65	16	2	00	0	00	0	0	0	0	0.4	30	+ o a, p
7	96.9	00.9	04.0	-2.4	1.4	1.4	2.7		92	90	81	24	3	24	2	16	1	10	10	10 -	0.2	30	+ n, + a, + p
8	05.2	01.4	99.5	-5.0	2.6	1.4	3.7		80	60	86	16	2	00	0	00	0	1	10	10 -	0.2	30	o n, a, + p
9	98.7	99.2	99.0	0.6	1.2	0.6	1.7		95	94	84	00	0	00	0	00	0	10	4	2.8	30	+ n, a	
10	98.4	97.7	96.4	1.2	5.0	4.8	5.1		93	86	81	00	0	00	0	00	0	6	9	1 -	0.0	30	- n, + p, o 19
11	93.6	92.5	92.6	1.4	3.6	2.8	4.8		92	72	68	32	1	16	1	32	2	10	10	10 -	0.4	20	+ n, o a
12	95.9	96.8	97.7	-0.4	3.4	2.4	3.9		92	80	85	00	0	00	0	16	1	10	10	10 -	0.0	20	+ n, + p
13	99.6	99.4	98.9	1.8	2.4	1.8	4.9		85	73	92	20	1	32	1	00	0	9	10	10 -	3.1	20	+ n, + a, + a, + p
14	94.4	94.6	94.1	1.6	5.0	4.0	5.3		95	87	90	16	1	00	0	16	1	10	10	10 -	5.0	12	+ n, + a, + a, + p
15	90.2	89.0	88.6	2.6	4.2	4.0	4.3		94	94	93	24	1	00	0	20	1	10	10	10 -	0.0	20	+ n, + a, + a, + p
16	91.8	92.8	90.7	-0.2	1.6	1.2	4.0		90	81	85	32	1	00	0	32	3	10	10	10 -	15.4	12	+ n, + a, + a, + p
17	98.8	90.8	92.2	-0.4	0.0	-0.4	1.2		96	90	91	32	4	32	3	20	1	10	8	8 -	8.4	17	+ n, + a, + a, + p
18	98.7	02.1	04.0	-1.4	1.0	0.6	2.9		93	84	90	16	4	24	5	24</							

# Extenso-Tabelle

1944

## Trondheim (Voll)

$\varphi = 63^\circ 25' N$

$\lambda = 10^\circ 27' E$

$g = 9.821$

$\Delta G = +1^\circ$

Mai V

$H_a = 127$

$H_b = 133.0$

$h_t = 2.0$

$h_a =$

$h_d = 11.2$

$h_r = 1.3$

Datum	Luftdruck P			Lufttemperatur T					Relative Feuchte U			Richtung und Stärke des Windes D,F			> Sicht	Bewölkung und Wetter N,w			Niederschlag mm	Schneehöhe m	Witterungsverlauf W	
	8	14	19	8	14	19	Max	Min	8	14	19	8	14	19		14	8	14	19			
1	86.3	85.6	88.5	4.2	7.0	2.6	7.0		94	90	90	00	0	24	4	24	4			1.0		
2	80.8	74.8	71.9	2.6	7.0	5.2	7.1		85	60	71	32	1	04	3	16	2			7.0		
3	75.1	79.0	83.2	2.6	4.6	2.4	5.2		80	70	70	32	3	32	3	32	5			0.2		
4	90.8	90.8	90.2	0.4	3.8	3.2	4.3		62	58	58	32	4	32	3	32	5			0.0		
5	92.4	94.7	95.3	-0.8	3.0	3.0	3.5		66	60	56	32	1	32	4	32	2					
6	02.9	05.4	06.5	0.4	4.4	4.8	4.9		65	60	60	16	1	32	1	32	2					
7	10.5	11.1	10.7	2.6	8.0	7.8	8.7		58	54	52	16	1	32	2	00	0					
8	11.7	10.8	09.5	6.0	10.4	10.8	11.5		60	54	50	00	0	32	1	32	1					
9	08.9	06.8	05.2	8.0	11.0	12.4	13.5		63	53	53	32	1	32	3	12	2					
10	01.0	00.1	99.2	7.0	12.4	8.2	12.5		64	65	80	00	0	32	3	00	0					
11	92.5	95.5	96.7	7.8	11.0	9.2	11.7		70	68	71	20	3	32	1	24	2			0.5		
12	99.4	00.4	99.4	6.6	10.0	9.2	10.3		90	80	87	00	0	00	0	16	1			0.4		
13	00.2	99.4	98.1	8.2	9.2	8.4	9.5		91	95	94	12	1	00	0	12	1			10.8		
14	02.3	04.5	05.0	4.4	4.6	4.0	8.4		94	92	90	16	2	4	32	3	00			10.0		
15	06.9	09.2	10.4	5.6	6.2	5.6	6.3		90	75	76	32	3	32	4	32	2			5.4		
16	11.4	12.3	12.5	5.2	8.4	7.2	8.5		85	73	88	00	0	00	0	32	1			0.5		
17	14.2	13.6	13.0	6.4	10.4	7.8	10.9		92	70	89	16	1	16	1	16	2			0.4		
18	12.8	11.7	09.9	5.8	8.6	9.6	10.1		90	70	65	32	1	32	2	00	0					
19	C3.9	02.7	03.2	6.2	7.0	5.2	9.6		88	84	78	24	1	24	4	28	5			0.0		
20	04.2	01.3	97.6	5.0	5.4	4.4	5.5		67	62	65	32	3	32	1	00	0			0.4		
21	88.2	86.9	88.1	3.8	7.0	3.4	7.3		88	70	91	20	4	20	4	24	3			1.2		
22	92.8	95.1	97.0	5.8	7.0	6.4	7.0		74	65	87	16	1	32	2	20	2			1.2		
23	01.3	99.3	98.1	4.2	6.8	4.8	7.5		78	65	65	16	1	32	4	28	3			0.5		
24	91.5	91.8	91.8	1.8	4.4	3.2	5.5		91	77	84	16	1	28	4	28	5			4.0		
25	90.3	89.8	90.0	1.8	5.4	3.6	5.9		92	84	90	24	4	24	3	20	3			6.6		
26	95.0	97.8	00.3	5.0	7.4	8.0	9.3		70	61	57	16	2	16	1	32	1			2.4		
27	98.9	98.7	05.3	8.6	11.6	12.2	14.2		62	70	72	24	1	20	2	20	2			0.5		
28	13.2	14.6	11.4	14.2	13.8	13.8	14.5		68	64	66	16	6	16	4	16	3			0.0		
29	10.6	10.3	10.0	8.2	14.4	10.0	14.5		76	80	83	16	2	24	2	20	3			0.1		
30	09.7	07.8	06.3	8.6	8.6	8.2	10.5		86	76	80	20	1	28	2	28	3			0.0		
31	02.9	03.7	04.1	5.4	7.4	6.6	8.2		94	81	85	24	3	24	4	24	4			7.0		
M	00.8	00.2	00.4	4.9	8.0	6.8	8.8		77	71	74	1.7		2.5		2.2				60	0	

Juni VI

1				6.0	8.0	8.6	9.2		88	70	64	16	1	32	2	32	2			3.6		
2				10.0	14.2	12.4	14.8		66	55	60	16	1	16	4	32	1			0.4		
3				9.0	7.2	8.6	12.4		74	88	85	32	1	00	0	28	2					
4				9.4	13.8	13.2	15.0		75	56	56	32	3	12	6	12	5			2.0		
5				11.6	10.8	11.2	13.2		65	74	68	16	6	12	6	12	6					
6				13.0	14.8	13.2	16.8		64	60	63	16	5	12	5	12	6			1.2		
7				12.0	18.8	18.0	19.4		67	55	55	00	0	12	4	16	2					
8				13.8	17.4	16.6	19.4		68	65	62	32	3	32	2	16	2					
9				11.4	16.4	12.0	16.6		94	71	91	32	2	32	3	28	1			4.0		
10				9.6	11.4	10.6	12.0		70	60	60	04	3	32	5	04	4			19.7		
11				8.8	11.6	10.2	13.0		60	55	84	08	6	04	5	16	1					
12				8.0	14.6	9.6	15.4		68	77	90	04	1	16	1	08	1			4.1		
13				10.4	12.2	11.8	12.2		87	74	70	32	1	32	3	32	1			12.6		
14				10.0	12.0	11.0	14.4		81	74	72	12	2	04	3	08	2			5.4		
15				12.6	15.2	11.6	15.4		66	72	80	20	5	00	0	16	1			2.0		
16				7.8	9.2	11.0	11.6		92	88	90	16	1	20	2	24	3			1.2		
17				9.4	12.6	13.0	14.0		92	77	71	32	1	20	1	16	1			7.4		
18				10.2	16.6	13.8	17.2		90	65	70	20	1	24	1	24	3					
19				14.2	16.4	13.2	16.4		80	81	85	20	1	20	2	20	2					
20				10.6	11.8	10.4	13.2		91	86	90	20	1	20	3	24	2			0.5		
21				8.4	10.4	9.4	10.4		93	76	77	24	4	20	4	20	4			2.5		
22				6.0	6.8	4.8	9.4		85	81	90	24	4	20	3	24	3			1.0		
23				6.4	11.0	8.2	11.4		87	70	78	24	2	24	4	24	3			5.6		
24				9.0	11.2	11.6	12.0		75	66	60	00	0	32	3	32	2			0.0		
25				10.2	16.0	14.4	17.4		66	56	57	32	2	32	4	16	3					
26				12.8	16.0	11.2	16.4		72	64	90	16	1	16	1	24	1					
27				12.6	16.4	19.0	19.0		85	75	70	04	3	32	3	16	1			5.2		
28				17.4	13.8	12.4	19.0		66													

# Extenso-Tabelle

1944

## Trondheim (Voll)

$\varphi = 63^\circ 25' N$   $\lambda = 10^\circ 27'E$   $g = 9.821$   $\Delta G = +1^h$   $H_a = 127$   $H_b = 133.0$   $h_a = 2.0$   $h_b = 11.2$   $h_r = 1.3$

Datum	Luftdruck P			Lufttemperatur T						Relative Feuchte U			Richtung und Stärke des Windes D,F			> Sicht	Bewölkung und Wetter N,w			Niederschlag Z	Schneehöhe H <sub>s</sub>	Witterungsverlauf W		
	8	14	19	8	14	19	Max	Min	8	14	19	8	14	19	14	8	14	19						
1	97.2*	98.3*	99.8*	15.0	17.0	17.0	17.3	8.2	70	71	66	32	1	08	1	08	1	9-	10-	9-	0.5		o n, o p	
2	90.7*	91.4*	91.5*	15.0	19.9	17.0	19.9	11.6	84	68	80	32	3	20	2	81	2	3-	10-	3-	0.8		-o n, i p	
3	93.1*	93.0*	91.7*	12.4	15.8	16.6	17.5	11.6	90	85	79	00	0	16	1	16	1	9-	6-	3-			. n, -o p	
4	99.6*	97.8*	96.1*	13.6	19.5	21.5	21.8	12.1	91	70	63	04	2	16	2	16	1	8-	1-	1-			-n, -o a,p	
5	95.6	95.1	94.8	17.2	23.0	22.4	25.0	13.7	84	57	48	02	2	00	0	28	1	8-	3-	1			-o n,a,p	
6	97.2	97.1	90.6	17.3	24.9	17.2	25.5	13.1	79	42	86	02	2	02	1	26	3	9-	1-	6-			-o n, -o a, -o p	
7	93.7	92.7	91.2	18.4	21.6	21.2	22.3	14.6	66	54	57	04	2	04	1	30	1	8-	1-	1-			-o n,a,p	
8	90.2	98.6	95.9	17.4	22.6	22.8	24.4	13.2	83	53	49	02	1	04	2	02	1	8-	0-	1-			o n, -o a,p	
9	94.4	91.4	88.8	19.9	21.9	20.9	23.5	14.8	71	64	84	06	1	04	2	17	3	8-	2-	8-			-o n,a,p, R+	
10	83.6	81.4	81.8	20.1	20.6	17.6	23.3	15.9	89	88	95	02	2	14	3	12	1	6	5-	10-	10-	2.2		-o n, -o R+i p
11	83.8	85.1	84.8	14.6	14.1	13.9	18.5	13.3	97	97	96	20	1	00	0	26	1	5	10-	10-	10-	21.2		-o n, -a, -a,p
12	85.0	86.6	88.0	12.9	15.4	13.0	16.2	12.3	95	88	97	21	1	04	2	2	2	7	10-	10-	10-	1.8		-o n, -a, -a, -i p
13	91.5	88.9	89.2	15.8	18.7	15.8	19.2	12.5	92	72	82	03	2	04	3	06	2	8-	2-	9-	10-	4.4		-i o n, -o a,p
14	88.6	88.0	87.2	14.9	20.9	19.4	21.6	12.4	85	46	40	18	1	17	2	20	2	9-	4-	1-	3.5		-o n, o a, -o a,p	
15	91.9	93.2	93.5	14.3	17.0	16.8	19.3	12.5	80	70	83	28	1	02	1	00	0	9-	3-	6-	5		o n,a	
16	97.2	97.7	90.1	16.0	21.3	15.2	21.3	12.1	90	65	91	04	2	26	4	28	5	9-	6-	7-	3.5		-o n, -o a,p	
17	96.4	96.5	97.8	13.6	19.3	16.9	20.3	12.6	95	67	78	08	1	18	1	26	3	9-	10-	3-			-n, -o a, o p	
18	96.9	94.4	94.7	14.7	17.5	16.4	18.3	13.4	84	68	79	08	1	07	3	04	2	9-	8-	1-			-o a	
19	93.5	93.1	92.5	12.4	17.0	15.3	17.0	11.5	89	71	86	24	2	26	4	30	2	9-	10-	4-			-i n,a	
20	92.5	92.5	92.5	11.8	12.0	12.5	14.4	10.5	96	79	79	20	2	25	4	28	4	9-	9-	10-	0.1		-o n, -o a, -o p	
21	91.7	90.5	98.7	10.8	14.6	15.7	16.3	10.1	98	73	73	18	1	10	1	21	1	9-	7-	4-	2.7		-n, -a, -a, -o p	
22	97.9	98.2	98.8	12.9	13.9	12.1	15.7	10.9	96	88	82	00	0	30	2	24	1	8-	10-	10-	0.1		=n,a	
23	90.8	90.3	90.1	10.2	12.9	11.2	13.8	8.3	66	60	58	28	2	28	5	30	3	9-	7-	9-			-n,p	
24	99.5	99.6	99.8	10.8	10.2	13.3	11.0	13.5	6.3	86	64	66	28	2	30	4	28	4	9-	3-	6-	0.7		i n,a, -o p
25	94.1	95.1	94.4	9.6	10.8	11.5	13.4	6.1	84	64	60	22	3	26	3	28	1	9-	8-	4-	0.7		-i n,a, -o i p	
26	94.5	92.5	91.8	12.2	16.5	16.2	17.7	5.9	71	60	52	04	1	02	2	15	1	9-	2-	4-	0.1		-o n, -a, e 11, -p	
27	98.4	97.9	97.7	17.3	21.9	18.6	22.6	10.5	58	24	52	18	5	20	7	18	6	8-	4-	3-	0.1		-o i n, -o a,p	
28	99.1	91.4	98.8	15.8	15.9	16.8	18.6	14.9	58	60	50	18	6	18	5	18	6	8-	10-	10-	0.8		-o n, i a, -o p	
29	98.5	98.8	99.7	15.7	16.3	18.0	19.4	13.2	90	83	68	04	1	16	3	14	3	7-	10-	5-	0.1		-n, -o a, -o p	
30	91.9	92.7	93.1	16.8	20.1	17.1	15.1	8.1	68	70	32	1	02	2	28	2	9-	9-	4-	4-		-n, -o a, -o p		
31	95.7	96.7	98.2	15.3	19.2	15.8	20.2	13.5	95	76	78	18	2	30	3	26	1	7-	10-	2-	9-		-n, -o a,p	
M	98.2	98.0	97.9	14.6	17.9	16.6	19.3	11.7	84	68	72	1.7		2.5		2.2	8.3	5.7	5.5	6.1	43			

## August VIII

1	11.0	10.7	10.1	13.0	17.1	15.7	17.4	11.6	96	72	73	32	1	02	2	04	2	8	10-	6-	1-			-n,a, -o p
2	11.0	10.1	98.8	13.7	17.9	17.4	19.0	8.3	78	55	53	04	1	04	2	08	1	9-	1-	0-	0-		-n, -o a,p	
3	09.3	08.9	09.0	15.8	21.8	21.5	24.4	9.3	77	53	48	06	2	04	2	26	1	9-	0-	0-	0-		-n, -o a,p	
4	12.4	12.3	12.9	17.1	21.3	15.3	21.5	12.9	73	65	80	20	2	28	3	28	4	8-	0-	0-	0-		-n, -o a,p	
5	13.6	12.4	10.3	11.5	15.2	14.2	15.9	9.2	95	72	81	28	1	04	2	04	2	5	10-	7-	0-			-n, -o a,p
6	97.8	98.4	98.6	14.6	16.6	14.1	16.8	9.6	87	76	80	24	1	30	4	28	2	5	0-	5-	7-			-n, -o a, -o p
7	94.7	93.0	91.9	13.2	18.8	18.2	18.9	8.1	93	61	75	18	1	00	0	32	1	7-	9-	8-	0-		-n, -a, -i p	
8	98.8	97.3	95.9	15.3	20.1	15.1	21.1	11.2	83	62	77	20	1	04	2	20	2	6-	3-	1-	2-	0.0		-o n,a,p
9	96.9	91.2	89.8	12.3	13.7	14.0	15.1	11.1	95	99	91	24	1	30	2	26	1	5-	10-	9-	0.5		-i n, -a, -i p	
10	88.7	88.6	87.8	12.1	14.7	13.3	15.3	9.7	89	79	87	26	1	28	1	14	2	7-	10-	8-	8-	0.0	-n, -i a, -i p	
11	83.6	82.2	87.0	12.1	19.7	14.8	19.7	10.9	90	85	69	04	1	24	1	26	4	7-	9-	9-	6-	5.4		-i n, -i a, -o p
12	88.0	85.0	87.4	12.2	16.0	12.5	16.9	10.1	87	64	81	18	1	04	4	24	2	10-	9-	6-	8-	4.8		-n, -o i a, -o R+i p
13	90.8	90.3	90.7	9.8	15.9	11.5	14.5	7.9	85	61	74	20	4	23	5	24	4	9-	5(1)	8-	7(1)	13.1		-o n, o 8, -a, -i p
14	94.0	96.6	96.9	8.6	10.1	9.1	11.8	8.1	90	78	79	24	2	25	3	24	4	7-	10(1)	9(1)	10(1)	1.9		-i n, -i a, -p
15	92.6	92.5	98.4	10.0	12.0	11.0	12.7	8.3	85	69	70	21	2	28	1	06	3	10	8-	7-	7-	6.3		-i n, o i a
16	92.0	91.5	89.2	10.9	12.0	13.0	13.1	9.9	93	93	92	04	1	04	1	18	1	4-	10-	10-	10-	10.3		-n, -i a, -i p
17	86.3	86.3	86.0	13.6	15.5	13.5	16.5	12.4	72	78	87	00	0	00	0	15	1	6-	10-	10-	10-	0.7		-i n, -a, -o p
18	87.4	83.5	81.0	14.7	17.6	19.9	20.5	11.8	87	78	58</													

# Extenso-Tabelle

1944

**Trondheim (Voll)**

$\varphi = 63^\circ 25' N$

$\lambda = 10^\circ 27' E$

$g = 9.821$

$\Delta G = +1^{\circ}$

**September IX**

$H_a = 127$

$H_b = 133.0$

$h_t = 2.0$

$h_a =$

$h_d = 11.2$

$h_r = 1.3$

Datum	Luftdruck P						Lufttemperatur T						Relative Feuchte U			Richtung und Stärke des Windes D,F			Sicht V			Bewölkung und Wetter N,w			Niederschlag R	Schneehöhe h_s	Witterungsverlauf W
	8	14	19	8	14	19	Max	Min	8	14	19	8	14	19	14	8	14	19									
1	78.5	80.8	83.5	11.3	14.7	11.2	14.7	7.5	34	69	79	04	1	04	3	28	1	10	2	-	2	9	-	1.3			
2	95.1	96.8	96.9	8.0	12.6	8.6	13.0	7.5	78	61	74	24	2	26	1	06	1	10	7	-	3	3	-	0.2			
3	94.2	90.5	88.7	6.4	11.0	11.3	13.3	5.8	89	72	64	06	4	04	4	14	1	8	10	-	7	-	7	-	0.1		
4	86.4	88.8	89.6	7.5	10.5	8.9	11.3	4.7	57	73	69	20	1	24	1	05	1	9	9	-	9	-	5	-	0.1		
5	89.4	87.8	85.1	5.2	10.7	10.3	11.9	2.9	78	68	78	06	3	06	3	04	1	10	2	-	3	3	7	-	0.1		
6	83.2	84.6	87.0	8.4	12.7	9.8	12.7	7.1	91	72	81	00	0	32	1	18	1	8	10	-	6	-	8	-	0.9		
7	93.6	96.1	96.7	6.4	13.1	9.4	13.1	5.8	90	61	69	20	1	06	1	00	0	10	2	-	2	1	1	-	0.8		
8	87.5	80.7	78.5	7.1	9.0	9.2	9.4	5.5	92	94	94	07	4	04	6	06	4	4	10	-	10	-	10	-	0.8		
9	86.3	92.7	94.4	8.3	7.6	6.5	9.2	6.5	95	82	81	24	3	30	4	22	2	7	10	-	10	(+)	3	-	11.1		
10	97.8	99.3	99.9	6.0	9.6	7.1	10.2	4.1	78	68	89	20	4	20	4	18	2	7	7	-	8	-	10	-	1.6		
11	03.8	07.5	10.6	7.8	8.4	8.2	9.0	6.2	95	89	90	18	3	22	2	00	0	7	10	-	10	-	10	-	3.1		
12	16.0	16.2	16.8	8.6	10.4	9.8	11.2	7.7	92	90	89	23	3	18	2	18	1	8	10	-	10	-	8(+)	-	5.7		
13	17.1	16.7	15.0	8.2	11.1	8.6	11.5	8.1	92	79	75	20	2	06	2	08	1	8	10	-	9	-	1	-	0.7		
14	12.9	10.6	10.2	7.0	10.9	9.8	12.5	2.8	81	73	78	18	1	04	3	04	1	10	0	-	1	2	1	-	0.7		
15	09.1	05.0	03.2	8.4	13.3	12.6	13.6	5.7	78	68	71	18	1	30	1	18	3	7	0	-	8	-	10	-	0.7		
16	02.1	00.1	99.6	12.0	17.4	15.2	17.4	11.0	79	68	68	16	1	22	1	18	4	8	8	-	9	-	8	-	0.0		
17	02.2	03.5	06.9	11.8	13.7	10.7	15.2	10.6	92	90	89	18	1	00	0	00	0	7	10	-	8	-	9	-	4.0		
18	09.9	10.4	11.0	10.2	12.9	12.4	12.9	9.5	92	92	94	22	1	00	0	00	0	4	10	-	9	-	10	-	3.3		
19	12.8	11.5	09.6	10.1	16.3	15.8	16.7	9.1	94	73	81	21	1	06	2	16	1	10	10	-	0	0	0	-	2.5		
20	07.5	05.7	03.3	13.0	16.3	13.5	16.6	10.3	71	54	62	17	4	18	5	18	5	9	1	-	2	-	7	-	0.7		
21	06.9	07.7	08.8	10.3	15.7	12.0	17.3	6.2	76	61	74	00	0	04	1	00	0	10	2	-	1	1	0	-	0.0		
22	07.0	04.7	02.1	13.3	17.0	14.0	17.2	8.8	68	55	58	18	4	18	6	17	6	7	1	-	5	-	4	-	0.7		
23	97.1	92.7	91.3	11.9	14.4	12.5	14.4	10.5	61	54	60	17	5	16	4	17	5	8	6	-	4	-	4	-	0.7		
24	89.8	89.5	89.7	10.0	15.9	11.3	15.9	9.5	90	73	90	28	1	12	1	28	1	7	10	-	10	-	10	-	2.0		
25	87.4	89.0	83.0	9.6	10.7	8.0	11.3	8.0	93	81	90	18	2	25	2	08	1	8	9	-	10	-	3	-	9.9		
26	67.5	68.9	70.4	7.0	7.9	6.8	8.3	6.1	94	87	89	18	2	18	3	20	2	5	10	-	10	-	10	-	4.6		
27	67.8	70.4	74.2	3.8	10.0	8.0	10.0	3.2	85	65	65	00	0	04	2	16	4	10	9	-	3	3	3	-	4.5		
28	84.4	89.1	92.1	5.0	7.4	4.1	8.0	4.1	86	78	79	18	4	20	3	18	3	8	10	-	10	-	3	-	1.1		
29	88.7	83.6	80.3	5.0	9.7	9.0	9.7	1.5	68	65	74	17	3	18	5	20	6	10	8	-	6	-	10	-	1.0		
30	80.2	82.4	83.8	8.9	9.8	7.7	10.7	7.7	90	78	71	18	1	22	3	24	3	10	8	-	10	-	10(+)	-	2.1		
M	95.4	95.4	95.4	8.6	12.0	10.0	12.5	6.8	85	73	78	2.1		2.5		2.1		8.0	6.8	6.5	6.2	6.1					

**Oktober X**

1	86.3	86.9	86.4	4.3	8.4	6.2	8.8	3.5	76	59	81	18	4	16	3	20	4	10	5	-	10	-	10	-	3.7			
2	94.5	96.4	96.5	6.4	7.5	4.1	9.3	4.1	73	84	23	4	24	3	16	2	10	10	+	9	5	-	5	-	13.4			
3	95.2	95.4	98.2	2.5	10.0	9.1	10.0	0.8	84	58	57	08	1	18	2	08	3	10	3	-	9	-	9	-	1.5			
4	05.6	05.8	04.5	3.3	8.0	5.1	8.2	1.8	80	88	86	16	1	26	1	00	0	7	0	-	3	-	0	-	0.2			
5	97.9	96.9	87.7	7.3	6.5	4.8	8.0	2.4	89	64	66	06	18	5	26	4	24	3	10	10	(=)	7	7	7	0	0.2		
6	86.4	99.0	93.5	3.3	4.7	10.4	10.8	3.0	90	87	59	18	2	18	4	24	6	5	10	-	10	-	10	-	2.6			
7	93.4	92.3	95.4	9.9	10.5	8.8	10.7	8.6	89	94	94	24	4	24	3	24	2	4	10	-	10	-	10	-	10.6			
8	92.6	95.5	97.2	7.0	6.4	5.2	8.8	5.2	85	85	86	22	3	24	3	26	4	7	81	-	5	-	6(+)i	-	12.9			
9	97.7	98.4	97.8	6.2	9.0	7.4	9.0	4.7	74	66	75	18	2	20	3	00	0	10	3	-	9	-	10	-	8.0			
10	98.2	96.2	95.3	7.2	11.6	6.6	11.6	6.6	67	79	84	04	1	32	1	00	0	10	3	-	2	-	0	-	0.1			
11	92.5	93.0	92.2	9.9	11.8	9.9	11.8	6.2	65	72	85	16	4	24	1	24	2	7	8	-	5	-	4	-	0.6			
12	87.8	86.7	89.1	11.1	15.4	12.2	14.3	7.0	72	58	58	17	5	18	5	16	6	10	3	-	8	-	0	-	0.1			
13	86.8	85.9	85.1	11.8	14.3	12.8	14.3	10.6	58	62	62	16	7	16	5	16	6	7	9	-	7	-	8	-	0.1			
14	86.0	85.2	81.7	7.5																								

# Extenso-Tabelle

1944

**Trondheim (Voll)**

$\varphi = 63^\circ 25' N$   $\lambda = 10^\circ 27' E$   $g = 9.821$   $\Delta G = +1^h$   $H_a = 127$   $H_b = 135.0$   $h_a = 2.0$   $h_b = 11.2$   $h_r = 1.3$

Datum	Luftdruck P						Lufttemperatur T						Relative Feuchte U			Richtung und Stärke des Windes D,F			> Sicht			Bewölkung und Wetter N,w			Niederschlag R	Schneehöhe H <sub>s</sub>	Witterungsverlauf W		
	8			14			19			8			8			14			8			14							
	8	14	19	8	14	19	Max	Min	8	14	19	8	14	19	8	14	19	8	14	19	8	14	19						
1	96.4	99.0	00.3	-0.4	0.5	-0.7	3.6	-0.7	93	85	85	04	1	02	1	00	0	10	10	10	10	10	10	6.2	3	+ a			
2	97.1	94.6	93.3	-4.8	1.3	1.9	1.9	-5.8	90	84	81	18	1	08	2	2	6	3	0	0	0	0	0	0		3	- a, a, - p		
3	85.1	80.7	76.8	3.0	5.1	1.6	5.1	-1.6	68	59	68	17	4	17	4	16	2	8	0	1	1	0	0	0	3	- a, - p			
4	71.0	73.0	73.6	0.1	1.3	0.1	2.3	-1.4	74	87	74	16	2	22	2	20	2	6	10	8	6(m)	3	0	0	0	0	- a, f a, - p		
5	57.9	60.0	60.1	5.4	5.4	3.8	6.4	0.0	64	66	68	18	4	17	2	0	0	10	8	10	3	3	3	1.8	3	- a, a, p, - p			
6	65.4	63.0	66.0	4.0	6.2	5.1	6.8	2.1	58	50	50	16	6	18	7	18	7	10	4	9	2	2	2	2	3	3	- a		
7	70.3	72.1	75.0	3.0	3.8	1.9	5.1	-1.6	56	66	66	16	2	18	3	20	4	10	7	7	5	5	5	5	3	- a, a, p			
8	81.0	79.9	78.0	-3.7	-1.9	-1.7	2.3	-4.4	80	80	78	16	1	20	1	20	1	8	6	4	4	7	7	7	3	- a, a, - (m) a, - p			
9	75.3	79.6	84.6	-0.3	0.3	-2.3	0.3	-2.8	93	89	92	22	1	20	1	16	2	5	10	5	5	3	3	3	1.8	3	- a, a, + a, - p		
10	92.0	96.5	99.1	-1.6	0.9	2.3	2.3	-2.9	94	94	94	22	1	23	2	25	2	4	10	10	10	10	10	10	1.8	3	- a, a, + a, - p		
11	06.6	09.4	10.1	2.2	3.0	2.7	3.0	-2.2	94	93	92	20	3	18	2	20	1	6	10	4	10	10	10	10	7.8	1.7	+ a, a, p, - p		
12	10.0	07.5	06.6	-1.1	1.0	3.2	3.2	-1.3	85	77	71	06	0	08	2	10	3	3	3	4	5	5	5	5	3	- a, - a, - a, p			
13	03.4	05.0	08.0	2.8	4.0	3.4	4.0	-1.7	80	76	74	00	0	06	2	08	4	08	4	10	7	1	5	5	3	3	- a, a, p		
14	06.7	08.5	09.9	-0.6	0.7	1.1	3.3	-0.8	72	63	66	08	2	06	4	08	4	10	6	6	2	2	0	0	3	3	- a		
15	12.3	15.0	16.5	0.1	-0.1	-2.3	1.1	-2.3	66	58	63	07	5	08	4	08	2	10	6	6	2	2	0	0	3	3	- a, a, + a, - p		
16	16.2	15.2	15.7	-3.7	-1.1	-3.5	-0.7	-4.8	65	59	68	04	1	16	2	08	1	8	1	1	1	0	0	0	3	3	- a, a, p, - p		
17	12.1	09.7	07.9	-3.1	-1.1	-2.7	-0.9	-4.0	71	56	64	14	4	16	3	14	3	10	0	0	0	0	0	0	3	3	- a, a, p, - a, p		
18	97.3	94.8	91.3	-1.3	0.6	-0.7	-0.3	-3.0	58	54	58	16	6	17	6	16	4	10	7	7	7	7	7	7	3	3	- a		
19	88.2	85.3	80.9	0.5	2.5	2.5	2.8	-1.7	61	60	63	18	2	17	3	16	1	10	9	9	9	9	9	9	3	3	- a		
20	73.3	73.8	75.7	1.7	1.1	-0.1	2.7	-0.1	69	71	74	10	5	04	2	10	3	10	9	9	9	9	9	9	3	3	- a		
21	81.9	85.8	88.4	-1.1	-0.1	-1.1	0.8	-2.8	94	78	93	24	2	24	3	25	3	8	10	8	8	8	8	8	3	3	+ a, a, + a, a, + p		
22	91.2	88.6	86.6	-2.1	3.7	7.7	-0.3	-7.7	84	81	76	18	4	20	2	20	6	10	3	3	2	2	2	2	3	3	- a, a, p		
23	77.2	70.1	66.9	-3.5	0.7	3.2	3.6	-8.1	66	63	62	10	2	18	6	22	6	10	3	3	2	2	2	2	3	3	- a		
24	61.3	62.5	65.5	4.0	4.8	4.0	4.8	-0.7	62	58	58	16	4	18	3	00	0	10	2	2	2	2	2	2	3	3	- p		
25	67.8	69.9	70.3	-2.1	-2.9	-3.1	4.1	-4.3	72	78	82	18	1	00	0	20	1	7	3	3	3	3	3	3	3	3	- a, a, p, + p		
26	74.6	82.5	88.4	1.5	1.1	-1.9	1.8	-3.1	84	84	89	22	4	28	3	24	1	3	10	10	10	10	10	10	1.4	6	+ a, a, + a, a, + p		
27	97.5	00.8	01.0	-7.1	-7.1	-7.1	-1.1	-8.4	89	81	76	18	2	20	2	20	6	10	3	3	2	2	2	2	3	3	- a, a, p, + p		
28	97.6	91.5	85.2	-5.1	0.3	1.9	2.3	-8.6	62	60	62	16	2	18	4	20	7	10	3	9	10	10	10	10	10	- a, a, + p			
29	86.2	89.3	88.7	4.8	4.2	2.8	5.0	-2.4	60	58	59	18	7	18	4	16	3	8	2+	4	4	7	7	7	7	7	- a, a, - a, + 14, - p		
30	88.9	89.5	89.2	5.0	5.8	6.4	6.4	-2.8	58	58	58	18	5	18	6	20	5	8	8	6	6	9	9	9	9	- a, a, p, + 14			
M	88.1	88.5	88.6	-0.1	1.1	0.4	2.7	-2.4	74	71	72	2.9	2.9	2.9	2.5	8.2	5.6	5.6	5.6	5.5	31	2	2	2	2	2	2		

## Dezember XII

1	95.1	89.4	87.2	0.9	5.2	5.2	6.4	0.6	74	56	62	06	1	18	3	20	5	10	9	4	6	6	0.1	0.1	+ a, a, - a		
2	69.7	64.2	69.4	7.8	8.0	3.0	8.7	3.0	62	63	87	14	0	02	1	00	0	8	8	8	10	10	10	0.1	0.1	- a, - + p	
3	74.4	75.5	74.7	-1.3	-1.1	-2.9	3.2	-2.9	78	72	74	00	0	0	1	14	5	06	5	3	6	6	2	2	2	2	- a, a, p
4	72.5	72.7	73.4	-2.9	1.4	1.1	1.4	-3.4	78	68	04	04	1	14	5	06	5	7	3	6	6	2	2	2	2	- a, a, p	
5	74.9	74.1	73.9	1.1	0.7	-0.9	1.8	-1.3	51	69	74	06	4	10	1	12	1	8	4	4	4	0	0	0	0	- a, a, p	
6	75.3	75.5	75.9	1.1	3.1	2.8	3.1	-1.0	68	63	65	16	4	18	9	5	10	4	7	3	6	6	4	4	5	- a, - a, - p	
7	76.6	76.1	78.2	1.5	1.9	1.5	3.0	-0.7	64	62	63	14	3	18	1	14	4	08	7	7	1	1	1	1	2	- a, a, p	
8	79.6	81.9	83.7	4.0	4.8	3.8	4.9	-1.6	62	61	60	08	4	06	4	08	7	8	7	8	8	8	8	8	8	- a, a, p, + 14	
9	85.2	86.6	81.8	1.1	0.3	-0.7	3.7	-0.7	60	62	61	10	4	10	1	10	3	10	10	3	3	3	3	3	3	- a, a, p	
10	72.0	73.9	75.6	-3.6	-0.5	0.5	1.0	-3.7	94	68	65	00	0	16	4	14	4	8	10	6	1	1	1	1	1	- a, - + a, - a, - a, - p	
11	82.8	86.6	88.4	-2.8	3.0	1.9	3.2	-0.2	63	62	60	10	4	18	4	16	3	7	8	5	5	0	0	0	0	- a, - a, p	
12	87.8	87.9	90.8	-1.2	-3.4	-2.1	2.0	-3.8	70	79	87	16	1	18	2	20	2	20	1	7	3	7	7	7	7	- a, - a, - p	
13																											

# Extenso-Tabelle

1944

Tromsø

$\varphi = 69^{\circ} 39' N$

$\lambda = 18^{\circ} 57' E$

$g = 9.825$

$\Delta G = +1^{\circ}$

Januar I

$H_a = 102$

$H_b = 114.5$

$h_a = 2.8$

$h_b = 12.3$

$h_a = 20.7$

$h_b = 1.7$

Datum	Luftdruck P			Lufttemperatur T						Relative Feuchte U			Richtung und Stärke des Windes D,F			> Sicht	Bewölkung und Wetter N,w			Niederschlag R	Schneehöhe h <sub>s</sub>	Witterungsverlauf W			
	8	14	19	8	14	19	Max	Min	8	14	19	8	14	19	14	8	14	19							
1	78.8	79.8	81.3	-7.2	-8.1	-8.4	-4.4	-8.8	78	74	84	18	1	18	2	20	2	10	0	1	1	34	34	→ n, p	
2	81.7	81.1	80.2	-9.2	-8.5	-8.5	-8.3	-9.8	86	87	81	00	0	00	0	20	1	10	0	2	0	34	34	→ n, → p	
3	81.9	83.3	84.1	-7.9	-8.7	-7.2	-7.0	-9.7	80	84	83	00	0	18	2	18	3	10	0	5	8	30	30	→ n	
4	88.5	90.9	92.2	-4.2	-3.9	-3.3	-3.3	-7.4	88	86	18	22	2	18	2	18	2	10	10	10	9	37	37	• n, a, p	
5	91.8	88.6	80.9	-3.2	-3.9	-4.6	-2.8	-5.1	76	70	64	22	18	3	18	3	6	9	9	8	6	6.0	40	• n, * a, a	
6	62.6	62.0	63.5	-6.3	-6.3	-5.1	-4.2	-8.2	60	72	89	18	2	03	2	00	0	9	2	10	10	4	0.6	39	* p
7	73.4	76.1	77.1	-5.9	-7.0	-7.0	-3.5	-7.3	82	73	83	31	3	03	2	02	2	8	8	8	8	2.1	35	* n, * a, * p	
8	75.8	75.2	73.9	-6.8	-7.1	-6.7	-6.6	-8.2	79	91	81	19	3	19	4	19	4	3	9	10	10	4.5	36	* n, a, p	
9	71.6	72.7	74.1	-7.6	-8.6	-8.6	-6.5	-9.3	77	76	78	19	3	19	3	19	5	7	3	3	7	37	* n		
10	77.2	78.4	79.6	-6.4	-3.6	-2.0	-2.0	-8.8	84	86	82	19	3	17	3	16	2	9	10	10	10	0.1	35	* n, a, * p	
11	83.7	86.7	89.3	-3.0	-2.5	-3.4	-2.0	-4.6	87	67	71	23	2	30	4	30	3	8	9	8	10	8	3.6	42	* n, a, p, -19
12	95.2	90.6	82.0	-5.8	-4.6	-4.8	-3.1	-6.1	78	68	77	04	1	02	2	04	2	9	8	9	9	10	7.8	48	* n, a, - p
13	99.4	94.4	89.6	-5.2	-4.7	-1.9	-1.6	-6.3	67	64	43	17	2	04	2	19	4	10	3	9	9	10	0.3	45	* n, a, p
14	76.2	78.7	80.8	0.1	-0.8	1.2	1.2	-2.3	60	74	68	17	5	17	5	19	5	7	10	10	8	0.0	39	* n, a, * a, * p	
15	74.4	67.5	69.1	2.9	5.9	5.0	6.5	0.4	60	74	55	17	5	22	5	22	7	7	10	10	10	0.0	39	* n, a, * a, * p	
16	88.6	96.9	97.5	2.9	1.7	1.8	5.0	0.7	76	79	74	02	5	01	3	02	2	5	10	△	10	8	20.4	29	* n, a, * a, * p
17	86.5	84.4	84.5	2.6	1.6	1.9	3.0	0.5	90	90	95	18	3	18	4	18	4	7	8	10	8	10	5.8	28	* n, a, * a, * p
18	82.6	86.2	88.6	2.8	2.0	3.2	4.5	1.4	87	87	72	18	5	18	3	18	4	6	10	10	7	10	10.8	25	* n, a, * a, * p
19	80.6	85.2	84.6	4.2	3.0	3.0	4.7	2.0	75	75	74	17	4	19	3	17	4	8	10	10	9	9	3.5	20	* n, a, * a, * p
20	87.9	90.1	86.6	1.3	3.0	3.4	3.5	0.5	82	65	57	18	3	18	4	18	5	9	10	10	9	2	2.6	20	* n, * a
21	80.8	75.7	72.2	4.3	2.0	1.8	4.7	-1.4	51	49	56	18	4	18	5	16	4	10	10	10	4	1	0.1	20	
22	68.9	66.0	66.8	0.5	-1.2	-2.1	1.8	-2.4	70	59	55	17	3	18	3	18	3	10	3	4	1	1	18		* a, -19
23	63.1	61.2	60.8	-3.1	0.2	1.2	1.2	-4.5	69	63	67	05	2	17	4	17	3	9	4	10	10	10	18		
24	63.5	65.8	67.9	0.8	0.6	0.2	1.5	-0.3	71	72	96	18	4	19	3	19	2	10	10	10	10	1	6.2	21	* p, -19
25	73.1	74.5	75.3	-0.8	-1.4	-4.0	0.2	-4.0	80	85	88	20	1	18	2	18	2	10	9	9	9	1	6.2	21	* n, * a
26	75.2	74.8	76.3	-5.6	-4.8	-1.4	-1.4	-6.4	85	82	58	18	1	00	0	18	4	10	4	10	10	10	21		
27	71.8	64.6	62.2	-0.5	0.0	-2.0	0.7	-2.2	58	51	57	17	5	17	4	18	5	10	4	10	10	10	21		
28	65.0	68.4	72.0	-1.4	-1.6	-0.7	-0.6	-2.1	62	69	76	18	4	18	5	18	4	10	8	9	9	10	20		
29	79.8	81.6	77.3	-0.9	1.0	0.5	1.2	-1.4	90	78	65	21	3	18	3	18	4	10	9	9	9	10	7.6	30	* n, * a
30	68.9	71.0	75.2	-1.8	-2.8	-1.2	0.5	-3.8	62	79	79	19	3	18	4	18	2	9	9	10	10	10	1.2	32	
31	88.9	90.6	87.2	-0.4	-0.8	-3.0	0.2	-3.7	96	89	87	18	2	22	2	00	0	9	10	9	7	4	12.6	50	* n, * a
M	78.6	79.2	79.1	-2.2	-2.3	-2.0	-0.5	-4.1	76	75	74	2.8	3	3.0	3.0	8.6	7.1	8.4	7.0	100	31				

Februar II

1	72.1	70.9	69.8	0.9	1.9	2.6	2.7	-4.0	73	69	61	18	5	18	5	18	5	9	10	9	7	1.8	44	* 14-16
2	67.7	70.4	71.3	-0.9	-1.2	-1.4	2.6	-1.8	87	89	88	18	4	18	3	18	2	8	10	10	10	0.1	40	* n, * a, p
3	70.4	70.6	70.7	-3.4	-1.3	-2.6	-1.3	-3.7	93	77	89	18	2	18	2	18	2	9	8	10	10	0.8	40	* n, p
4	73.4	75.8	77.6	-4.5	-4.3	-4.0	-2.2	-5.4	80	83	81	18	4	18	5	18	5	10	3	9	10	0.1	40	* p, n, * a, p
5	82.4	85.4	88.7	-1.8	-0.9	-1.4	-0.4	-4.2	92	89	87	18	5	00	0	25	2	8	10	9	9	1.0	40	* n, * a, p
6	91.9	86.6	80.9	-1.9	-1.4	-0.2	-0.2	-2.0	82	81	93	18	3	17	4	18	4	6	10	10	10	7.8	48	* n, * a, p
7	70.1	66.8	62.9	1.2	1.4	0.1	3.0	-0.4	85	75	84	18	5	18	2	17	2	10	9	10	10	1.0	46	* n
8	58.9	60.0	62.7	0.3	-0.5	-0.8	1.0	-1.6	70	80	74	23	2	00	0	00	0	9	10	7	9	46		
9	68.9	72.9	76.7	0.3	0.4	0.4	0.4	-1.3	88	88	86	18	5	00	0	00	0	9	10	9	9	44		
10	85.6	88.9	91.8	-0.8	-0.4	-3.0	0.4	-3.0	90	76	89	18	5	32	2	2	2	8	9	9	10	0.1	44	* n, * a, p, -19
11	95.1	97.4	98.0	-3.3	-2.5	-3.1	-2.4	-4.6	88	77	78	18	2	18	3	18	4	10	8	9	6	5.2	52	* n, * a, * a, * p
12	96.6	98.7	90.5	-1.0	1.6	2.8	2.9	-3.1	95	90	78	18	5	18	4	19	5	7	10	10	10	1.6	51	* n, * a, * a, * p
13	95.3	98.7	92.4	4.1	4.4	4.3	4.8	2.6	73	72	71	19	4	18	3	20	3	9	10	9	10	0.7	42	* n
14	96.0	96.6	99.6	1.6	2.2	2.3	4.9	0.9	58	47	55	18	5	18	4	18	5	10	7	8	7	36	36	* 14
15	99.8	96.6	95.2	1.5	3.6	0.8	3.6	0.4	50	49	18	5	18	5	18	5	10	8	7	7	6	36		
16	92.1	92.6	92.5	1.7	2.1	3.0																		

# Extenso-Tabelle

1944

**Tromsø**

Datum	Luftdruck P			Lufttemperatur T						Relative Feuchte U			Richtung und Stärke des Windes D,F			> Sicht			Bewölkung und Wetter N,w			Niederschlag R	Schneehöhe H <sub>1</sub>	Witterungsverlauf W
	8	14	19	8	14	19	Max	Min	8	14	19	8	14	19	14	8	14	19	8	14	19			
1	68.7	68.7	71.9	-1.7	-0.8	-1.4	0.0	-5.1	53	52	44	18	5	18	3	10	3	5	6	0.0	60			
2	73.3	72.5	71.1	-4.2	-2.1	-3.5	-1.3	-4.7	52	53	89	00	0	00	0	9	9	10	10	0.6	58	• n, o a		
3	67.7	70.2	72.2	-3.8	-1.8	-1.5	-1.2	-4.5	64	59	46	17	3	14	3	10	9	1	5	0.1	56	o a, • p		
4	78.5	80.8	83.0	-4.7	-2.6	-3.2	-1.3	-5.2	59	60	69	00	0	00	0	7	7	3	10	0.1	56	• n, o a, p		
5	82.0	83.5	87.1	-1.6	-1.2	-2.8	-1.2	-4.4	97	98	89	20	2	18	3	1	7	10	10	0.8	73	• n, o a, p		
6	94.6	90.6	95.2	-3.0	-2.4	-2.0	-1.5	-3.2	85	88	92	24	2	32	2	04	2	7	10	10	11.2	84	• n, o a, p	
7	99.2	12.5	14.2	0.6	1.0	0.2	1.3	-2.2	98	99	80	18	1	00	0	00	0	7	10	10	3.7	85	• n, o a, p	
8	77.1	16.8	13.4	-1.3	0.5	0.8	1.6	-1.7	92	79	95	00	0	00	0	3	9	6	7	10	1.4	79	• n, o a, p	
9	95.0	91.3	86.5	-3.1	4.3	3.3	4.5	0.6	86	87	91	18	5	20	4	20	3	7	10	10	2.1	72	• n, o a, p	
10	78.7	75.1	71.0	1.1	2.4	2.4	3.3	0.3	95	81	71	18	3	19	3	19	3	8	10	8	10	15.4	62	• n, o a, p
11	73.7	78.6	81.2	-0.3	0.2	-0.8	2.4	-1.3	94	79	76	27	3	21	2	21	3	7	10	9	9	2.9	60	• n, o a, p
12	80.4	76.9	74.0	-1.9	0.0	-1.6	1.0	-2.2	62	49	54	19	3	00	0	00	0	9	8	8	9	0.8	62	o a, a
13	72.7	74.2	75.3	-2.8	-1.1	-4.0	-0.8	-4.0	58	50	57	18	3	18	3	00	0	10	9	2	2	60	o a, p	
14	77.3	78.2	79.5	-5.2	-3.3	-3.4	-2.8	-5.9	62	56	58	19	4	18	4	19	4	7	10	7	8	59	o a	
15	83.9	87.2	90.5	-4.1	-1.4	-2.7	-1.3	-5.2	74	83	77	00	0	00	0	01	2	7	8	10	10	58	• n, a, p	
16	98.0	91.2	90.8	-4.0	-0.9	-4.3	-0.5	-4.5	65	42	51	00	0	00	0	16	3	10	6	1	1	1.6	58	o a, p
17	97.0	93.2	89.1	-4.6	-0.8	-1.4	-0.7	-5.3	48	40	44	18	4	18	3	19	5	10	6	2	10	58	o a, p	
18	88.2	84.1	88.4	0.5	2.9	0.0	3.4	-1.8	62	48	82	18	1	16	5	00	0	9	1	9	0.1	58	• n, o a, p	
19	86.0	82.6	79.2	-1.5	0.6	0.3	1.6	-3.8	52	56	45	00	0	18	3	17	2	4	8	10	0.2	58	o n, a	
20	78.2	81.1	85.1	1.2	1.2	-2.0	1.8	-2.0	78	78	82	20	3	22	2	02	4	8	10	10	0.1	58	• n, a, p	
21	94.1	96.9	98.6	-2.8	-2.8	-4.1	-1.8	-4.1	87	85	87	00	0	04	2	04	1	6	10	10	3.5	60	• n, o a, p	
22	99.5	99.8	97.5	-6.0	-2.3	-3.8	-2.2	-7.4	87	58	90	00	0	02	2	12	2	9	4	0	2.9	67	• n, o a, p	
23	96.3	96.3	99.6	-2.9	-0.6	-3.4	0.3	-5.8	58	40	46	07	2	12	2	10	1	10	7	2	2.8	68	• n, o a, p	
24	10.5	13.7	15.0	-5.8	-1.6	-4.8	-1.1	-7.7	78	52	50	14	1	20	2	18	2	10	0	0	66	o a, p		
25	12.2	09.3	09.1	-5.6	-1.3	-4.1	-0.8	-7.9	50	39	45	17	3	16	4	14	3	10	0	0	3	64	o n, a, p	
26	09.5	11.3	11.8	-4.7	-2.6	-4.0	-2.0	-6.4	48	50	55	16	5	17	4	18	3	9	1	1	2	63	o n, a, p	
27	10.2	07.0	04.5	-5.4	-2.6	-4.4	-1.5	-7.1	52	44	51	19	2	03	1	03	1	10	0	0	1	63	o n, a, p	
28	04.9	04.7	04.5	-3.7	-1.8	-4.1	-0.3	-5.9	41	36	39	07	1	06	3	05	1	10	1	1	1	63	o n, a, p	
29	02.9	02.4	01.8	-5.2	-3.4	-5.0	-1.7	-7.4	48	63	63	07	1	04	2	02	2	10	1	2	3	63	o a, p	
30	94.5	92.7	92.1	-5.2	-2.2	-3.5	-1.0	-7.2	84	74	79	19	3	14	1	14	1	9	10	6	10	0.7	63	• n, o a, p
31	90.2	90.5	90.2	-4.0	-2.2	-2.6	-1.6	-5.6	90	86	94	19	3	17	3	18	2	7	10	9	10	0.4	63	• n, o a, p
M	91.0	91.4	91.7	-2.9	-0.9	-2.3	-0.2	-4.5	69	61	67	20	2	2.2	2.1	6.8	6.3	5.8	7.1	57	64			

April IV																								
1	90.4	92.1	93.4	-2.2	-0.9	-1.0	-0.3	-3.3	86	78	72	18	3	19	3	18	3	8	10	8	2	10	5.7	73
2	98.0	90.8	02.9	-2.5	-0.1	-2.6	0.7	-3.1	73	56	54	04	3	20	2	00	0	10	1	1	1	0.6	73	
3	06.2	07.0	07.1	-3.4	-0.4	-2.6	0.2	-5.9	56	55	56	20	3	20	1	00	0	10	1	1	1	0.0	72	
4	08.1	07.4	07.0	-2.8	-1.0	-1.7	0.3	-6.8	60	63	69	21	2	20	1	00	0	10	1	1	1	0.2	70	
5	04.8	04.5	03.8	-1.6	1.0	-0.5	1.6	-3.5	90	76	71	18	2	18	2	20	2	9	10	10	1.4	70		
6	99.4	97.2	94.6	-1.5	-1.9	-1.3	0.9	-4.2	95	94	91	26	2	19	5	19	4	1	9(0)	10	10	4.4	78	
7	95.6	96.0	00.1	-2.2	-1.1	-2.0	0.4	-3.5	82	66	70	03	1	02	3	01	3	8	7	9	9	7.3	55	
8	03.4	03.9	03.1	-1.3	-0.1	-0.3	1.7	-3.5	88	84	84	18	2	24	2	20	1	8	9	10	9	1.9	90	
9	01.7	02.7	03.0	-0.1	1.3	-0.5	2.4	-1.4	84	78	88	19	3	19	2	20	1	10	9	7	7	1.2	88	
10	02.2	00.2	99.5	-1.6	-0.5	-1.6	1.9	-4.3	84	80	90	19	3	18	3	28	1	6	9	9	0.3	80		
11	98.7	01.5	04.0	-3.8	-4.4	-6.7	-1.0	-6.8	62	73	64	30	2	31	4	01	4	8	8	9	7	1.0	81	
12	06.5	05.6	04.1	-4.1	-2.8	-3.8	-2.4	-6.9	56	44	47	18	3	19	3	20	3	10	8	1	7	0.3	79	
13	01.1	00.1	00.0	-4.9	-2.1	-1.3	-1.3	-6.3	63	54	56	18	4	19	4	20	3	10	6	6	6	78		
14	89.3	83.5	81.9	-2.3	-2.5	-2.2	-1.6	-4.6	58	87	94	18	2	31	2	03	2	5	10	10	10	76		
15	87.9	89.2	90.7	-1.8	-1.2	-3.9	0.8	-4.9	92	62	63	20	1	25	3	02	2	8	10	9	3.7	92		
16	89.4	94.9	95.9	-2.4	-3.4	-4.4	-1.7	-6.3	86	52	60	31	5	02	2	03	1	9	10	8	6	4.2	92	
17	95.4	96.4	96.3	-1.3	-1.8	-1.8	1.2	-5.5	73	78	61	19	4	32	3	04	3	8	8	8	1.9	90		
18	96.8	98.1	99.7	-2.1	-0.6	-1.6	0.2	-4.5	78	64	67	24	2	26	1	32	2	10	10	9	0.5	88		
19	06.2	07.1	05.5	-2.1	1.2	0.4	2.0	-5.4	78	68	52	18	3	18	2	18	1	9	10	9	0.3	86		

# Extenso-Tabelle

1944

Tromsø

$\varphi = 69^\circ 39' N$

$\lambda = 10^\circ 57' E$

$g = 9.825$

$\Delta G = +1^\circ$

Mai V

$H_a = 102 \quad H_b = 114.5 \quad h_c = 2.0 \quad h_d = 12.3 \quad h_e = 20.7 \quad h_f = 1.7$

Datum	Luftdruck P			Lufttemperatur T						Relative Feuchte U			Richtung und Stärke des Windes D,F			Sicht >	Bewölkung und Wetter N,w			Niederschlag K	Schneehöhe E	Witterungsverlauf W					
				8		14		19		8		14		19			8		14								
		8	14	19	8	14	19	Max	Min	8	14	19	Max	Min	8	14	19	Max	Min								
1	96.7	94.6	93.2	0.0	2.8	1.4	8.8	3.6	-3.1	66	38	45	31	1	06	2	07	2	10	1	1	4	0.0	74	○ a,p		
2	88.5	87.4	86.9	1.7	3.3	1.9	8.8	3.9	-1.6	41	42	47	08	2	10	2	08	2	10	3	2	1	5	0.0	71	○ a,a,p	
3	88.6	91.2	92.6	0.7	2.0	2.0	8.0	2.0	-3.2	56	48	58	00	0	04	3	04	1	10	9	2	2	5	0.0	70	○ a,a,p	
4	97.0	97.9	98.2	-1.0	0.0	-1.7	0.9	0.9	-2.8	79	59	69	02	2	04	3	02	2	9	9	8	8	7	0.5	70	○ a,a,o,p	
5	97.2	97.8	98.6	-1.3	-0.3	-0.1	1.2	1.2	-3.2	55	59	49	04	1	02	2	32	2	9	8	9	9	4	0.5	70	○ a,a,o,p	
6	00.6	02.2	03.7	-0.7	0.1	0.5	0.5	0.5	-2.2	87	95	96	18	4	18	4	18	2	3	10	10	10	10	0.0	70	○ a, + a,p	
7	06.9	06.8	06.1	2.7	4.6	3.2	4.7	4.7	0.3	66	57	72	20	4	19	4	19	2	10	10	9	10	10	0.4	62	○ a, ○ a	
8	09.0	11.4	11.2	4.2	5.2	5.9	6.8	6.8	1.8	80	69	19	19	4	21	3	18	3	10	10	8	8	8	1.6	66	○ a, + a,p	
9	08.7	07.4	06.5	7.0	9.1	8.4	9.9	9.9	2.9	51	53	18	20	2	21	3	18	3	10	8	2	2	8	0.6	60	○ a,p	
10	03.4	01.6	09.8	7.3	10.0	9.6	11.2	11.2	5.9	50	44	43	20	2	18	2	03	2	10	8	8	8	8	0.5	50	○ a,p	
11	92.6	90.2	88.0	5.2	7.6	7.2	10.1	4.1	69	61	57	05	1	18	3	18	4	9	10	9	9	9	9	3.0	45	○ a,p	
12	89.7	93.1	94.5	4.8	4.6	5.1	7.2	3.1	73	75	72	18	3	18	4	18	4	9	9	8	8	8	8	3.1	35	○ a, ○ a, + a,p	
13	91.4	94.5	96.0	6.8	6.7	4.8	7.4	4.0	61	49	64	19	20	2	24	3	18	3	9	6	6	6	6	0.0	20	○ a, + a, ○ a	
14	00.1	04.4	07.0	3.5	3.1	4.0	5.1	2.9	68	70	79	20	3	24	3	18	3	9	6	9	8	8	8	0.5	5	○ b	
15	09.8	11.1	13.0	4.6	5.1	5.0	5.4	1.8	68	72	78	21	1	26	2	31	2	9	10	10	10	10	10	0.2	0	+ ap	
16	15.5	12.0	10.0	3.6	4.4	4.4	4.7	1.7	67	60	68	18	3	20	4	18	3	10	10	10	10	10	10	0.2	0	○ p	
17	09.9	12.1	12.2	3.6	4.7	3.6	5.1	2.9	89	71	73	26	2	30	1	27	2	9	10	10	9	10	7	0.6	0	○ a, + a, + a,p	
18	11.6	08.9	05.1	3.6	3.8	3.8	4.1	1.5	74	64	73	20	2	21	3	18	3	9	10	10	10	10	10	1.9	0	○ a, + a, + a,p	
19	96.7	97.3	01.3	3.2	3.8	0.4	5.1	0.5	86	78	82	28	2	31	1	03	2	10	10	10	10	10	10	1.0	0	○ a, + a,p	
20	02.5	00.9	09.9	-1.1	0.3	0.0	1.0	-2.0	68	52	54	01	3	03	1	03	2	10	10	9	9	9	9	0.9	0	○ a,a	
21	95.6	95.6	95.7	0.4	1.6	1.2	2.1	-2.0	40	42	47	02	3	02	2	02	2	10	1	1	1	1	1	0.0	0	○ a,a,p	
22	98.0	99.5	00.9	1.5	2.9	2.8	3.8	-1.7	54	44	46	05	2	04	2	05	2	10	1	1	1	1	1	0.0	0	○ a,a,p	
23	02.5	02.3	01.9	3.4	3.9	3.4	6.2	-0.7	52	42	42	29	1	06	5	05	3	10	1	1	1	1	1	0.0	0	+ a,p	
24	98.0	96.0	94.3	1.8	0.6	1.2	3.4	0.4	55	86	78	05	5	04	5	05	3	10	8	2	2	6	6	0.2	0	○ a,a	
25	89.0	88.4	88.4	4.0	6.4	6.3	7.7	0.6	59	57	41	04	1	16	3	18	3	10	8	2	2	6	6	0.0	0	○ a,a,p	
26	92.6	95.2	98.7	7.1	8.9	7.6	9.3	4.3	40	45	54	16	4	18	5	23	3	10	2	2	2	3	3	1.0	0	○ a,a,p	
27	02.2	00.8	98.8	5.7	9.1	8.8	10.3	4.0	65	42	45	22	2	18	2	18	3	10	9	2	2	9	9	0.4	0	+ a,a, + a,p	
28	99.1	99.5	04.0	9.5	7.3	4.9	10.2	4.9	55	70	77	18	2	20	2	20	2	10	9	7	10	10	10	0.0	0	○ a, + a,p	
29	10.3	10.5	10.3	4.2	7.2	5.8	8.7	2.4	74	61	78	20	2	20	2	20	2	10	9	7	10	10	10	1.1	0	+ a, + a,p	
30	09.0	07.6	05.3	6.4	7.0	4.7	8.0	4.3	84	82	93	18	2	20	2	20	2	10	9	10	10	10	10	0.6	0	○ a, + a,p	
31	00.1	99.5	99.3	3.6	5.0	5.1	6.0	2.4	82	80	81	00	0	00	0	00	0	32	2	8	10	10	10	2.1	0	○ a,a,p	
M	00.4	00.6	00.7	3.4	4.5	3.8	5.7	1.2	65	60	64	23	2	27	2	27	2	26	9.1	7.4	6.7	7.5	26	25	.	.	.

Juni VI

1	02.6	04.4	04.8	6.9	7.9	8.8	8.8	3.6	49	43	40	06	2	06	2	09	2	10	2	4	1	1	1.0	0	○ a,a,p
2	04.5	03.3	01.2	6.4	6.2	4.5	8.8	4.3	71	66	67	04	3	05	3	05	3	10	2	8	7	7	0	○ B,14	
3	09.9	00.5	01.3	7.8	10.0	9.8	10.3	2.6	45	40	41	09	3	16	3	17	2	10	2	4	1	1	0	0	○ a,a,p
4	02.6	02.7	01.6	9.2	11.5	10.8	12.4	4.9	44	40	43	32	1	06	2	03	3	10	1	0	0	0	0	0	○ a,a,p
5	00.8	99.8	98.8	10.8	14.2	13.1	15.2	5.4	46	36	44	03	1	09	1	03	3	10	0	0	0	0	0	0	○ a,a,p
6	99.5	00.0	00.1	10.4	13.8	12.8	14.1	6.5	57	51	53	03	2	03	2	03	2	10	0	0	0	0	0	0	○ a,a,p
7	00.4	99.9	99.4	12.8	14.5	11.0	15.5	7.1	58	49	66	30	1	30	2	04	2	10	4	8	9	9	9	0.4	○ a,a,p
8	98.5	98.1	96.8	6.5	8.7	7.6	11.0	4.6	70	58	63	03	1	04	3	03	3	10	7	3	8	8	8	0.8	○ a,p
9	95.5	95.6	96.1	6.3	8.8	10.4	10.4	3.7	65	57	41	05	3	05	3	10	2	10	1	1	1	1	1	0	○ a,a,p
10	98.1	99.1	98.9	7.6	9.4	9.0	10.4	4.6	41	38	38	08	3	09	3	10	2	10	1	1	1	1	1	0	○ a,a,p
11	01.2	00.6	99.0	6.5	7.4	7.3	9.0	4.8	43	42	46	06	2	06	2	04	2	9	1	1	1	1	1	0	○ a,a,p
12	94.7	95.7	96.5	8.6	10.4	10.9	12.1	5.4	59	53	56	18	18	5	18	4	2	9	8	8	8	8</			

## **Extenso-Tabelle**

194

Tromsø

• 29 •

1 - 100 2

17 = 9.825

$$\Delta G = +1^{\circ}$$

Juli VII

$H_s = 102$

t<sub>b</sub> = 14.3

$b = 2.5$

- 12.3 -

29.7 hz 1.

Datum	Luftdruck P			Lufttemperatur T					Relative Feuchte U			Richtung und Stärke des Windes D,F			Sicht v	Bewölkung und Wetter N,w			Niederschlag R	Schneehöhe h	Witterungsverlauf W		
	8	14	19	8	14	19	Max	Min	8	14	19	8	14	19		14	8	14	19				
1	05.7	05.4	05.7	8.6	9.8	10.4	11.4	5.0	73	59	61	26	2	04	2	03	3	10	7	7	8	3.1	• n, t° o s, op
2	04.8	05.7	05.5	8.4	9.0	7.9	10.6	6.3	71	70	88	29	2	28	2	27	2	9	8	10	10	0.2	o n, t° s, t° p
3	07.0	07.7	07.2	9.2	10.2	9.7	10.7	6.7	80	68	66	26	2	28	2	24	2	10	10	• s	• s, t° a, op		
4	04.7	03.1	01.3	8.8	12.7	11.7	13.0	5.5	71	61	64	05	2	04	2	02	3	10	1	2	6	0.0	o n, a, p
5	00.0	00.8	01.0	7.4	8.4	8.0	11.9	6.5	87	80	85	02	2	28	2	31	1	10	10	• t	• n	0.1	
6	02.3	03.4	03.6	7.2	7.8	8.4	8.6	5.5	87	72	69	02	1	03	2	04	2	10	9	8	7	0.6	• o n, a
7	03.7	05.8	04.0	7.7	8.3	7.8	8.9	4.6	71	69	77	03	1	02	2	26	2	10	9	9	8	0.1	• o n, a
8	04.2	04.5	03.8	7.8	7.6	7.4	8.4	5.7	82	84	85	00	1	29	2	30	2	10	10	10	10	0.0	• o n, a
9	01.0	99.7	97.6	7.4	8.8	9.2	9.6	6.0	89	89	73	00	0	03	2	03	2	9	9	9	9	0.7	• o n, - a, p
10	99.7	91.7	90.6	10.2	13.6	15.2	15.5	5.7	70	58	49	06	2	04	3	10	2	10	1	1	1	0.7	o a, p
11	91.5	91.7	92.2	13.0	16.8	15.8	17.2	9.6	42	39	34	06	2	15	3	15	2	10	1	1	6	0.0	o n, a, p
12	95.7	96.1	96.8	15.3	17.6	15.1	18.1	11.1	44	35	48	14	3	17	2	18	2	10	3	3	8	0.0	o n, a, p
13	98.7	98.5	98.0	15.8	18.8	18.4	20.0	10.7	58	50	52	14	1	07	2	22	2	10	7	7	3	0.0	o n, p
14	97.5	96.0	94.7	16.7	19.4	20.1	22.0	12.2	68	61	58	03	1	02	2	32	2	10	1	3	1	0.0	o n, a, p
15	94.4	94.8	96.0	19.4	23.1	21.8	25.0	13.7	64	50	52	32	1	26	2	08	0	10	1	3	1	0.0	o n, a, p
16	99.5	00.5	01.2	16.6	19.4	17.6	22.0	13.5	72	64	66	26	1	02	2	02	1	10	1	1	1	0.0	o n, a, p
17	04.6	07.0	06.1	13.4	12.6	10.0	17.9	9.8	87	85	92	26	2	22	2	30	3	6	10	10	10	0.0	o n, a
18	10.6	09.5	07.2	9.7	13.2	12.9	14.1	8.9	80	70	68	03	2	03	2	02	2	10	10	2	3	0.3	• o n, o a, p
19	02.2	01.4	00.6	10.9	14.1	13.6	14.2	8.0	85	78	75	00	0	02	1	05	2	10	10	10	10	0.0	• o n, a
20	01.8	03.2	03.6	12.0	13.7	13.1	15.1	9.1	88	76	76	03	1	27	2	02	2	10	2	4	1	0.4	o a, p
21	04.5	04.0	04.0	9.9	11.0	9.0	13.1	8.0	89	85	90	00	0	28	2	04	2	9	10	10	10	10(+) 10(+) 1.2	- s
22	02.9	02.3	02.6	8.2	7.4	6.9	9.0	6.2	88	89	92	02	1	04	2	03	2	10	10	10	10	10(+) 10(+) 1.2	• o n, a, p
23	01.8	01.6	01.4	8.7	9.9	9.0	11.0	5.5	89	95	76	16	3	26	2	26	2	9	9	9	6	2.0	• o n, a, p
24	01.7	00.4	98.7	8.8	9.4	7.8	9.9	6.6	73	74	86	02	3	02	3	02	3	9	9	10	10(+) 10(+) 1.1	t a, p	
25	94.6	95.7	99.9	8.2	9.3	8.9	10.8	6.6	92	88	94	16	2	10	2	18	2	7	7	10	10	6.4	• n, t a, p
26	01.3	04.6	06.8	9.2	9.4	10.5	11.6	7.7	73	75	60	18	3	26	3	26	1	9	8	9	5	10.8	• n, t° a
27	07.4	07.0	05.7	9.8	15.2	16.4	17.1	5.1	67	51	47	25	1	02	2	22	2	10	1	3	1	2.0	o n, a, p
28	06.6	06.8	06.9	15.8	20.2	17.8	20.6	11.3	61	49	56	26	1	01	1	02	1	10	1	7	5	0.0	o n, a, o 1p
29	06.9	05.2	04.8	14.9	16.6	14.2	17.8	11.6	75	70	78	02	1	06	1	06	1	10	9	9	8	1.2	• n
30	04.2	04.5	05.9	12.9	16.7	14.1	19.1	8.8	81	67	74	24	1	04	1	04	1	9	9	9	10	0.0	o n, a, t° p
31	07.7	08.5	09.0	13.2	13.6	11.7	15.0	11.6	85	83	96	04	2	04	1	01	1	9	10	10	10	2.3	• o n, a, t° o o p
M	02.0	02.1	01.9	11.1	13.0	12.3	14.5	8.2	75	68	70	1.5	2.0	1.8	9.5	6.3	6.4	31					

## August VIII

1	10.4	12.3	14.6	10.4	9.1	7.8	11.9	7.6	95	89	86	92	1	03	2	05	2	7	10	10	9	2.4	• n, • a, p	
2	15.9	16.3	16.2	8.0	9.0	8.5	9.4	6.8	95	76	81	18	1	27	2	02	2	9	10	10	9	0.9	• n, + a, p	
3	15.6	14.8	13.6	8.9	10.9	11.0	12.5	6.8	90	64	74	02	2	02	2	02	2	10	10	8	10	0.0	+ p	
4	11.3	10.1	10.1	9.8	13.8	11.7	14.4	8.5	86	68	75	01	3	20	3	27	2	10	10	3	1	0.0	+ n	
5	09.8	09.6	08.9	9.8	12.6	10.7	12.9	8.8	92	82	94	18	3	20	3	27	2	8	10	9(+)	10	1.1	• n, + a, + 17-17*	
6	02.0	98.4	00.0	12.3	13.1	9.8	14.7	9.5	78	79	90	20	3	22	4	22	3	6	10	10(+)	10(+)	2.6	• n, + a, + p	
7	03.0	01.9	00.2	9.0	10.8	9.3	10.9	7.9	84	85	87	24	2	20	2	24	1	8	10(+)	9(+)	10(+)	3.4	• n, + a, + p	
8	96.5	97.5	97.6	9.2	9.6	8.4	10.2	8.2	94	78	75	08	0	02	1	26	2	9	9(+)	10	9	0.4	+ n, a, p	
9	95.7	95.6	94.6	8.1	10.2	7.9	10.5	6.5	76	69	76	02	1	02	2	03	3	10	9	6	3	0.5	o p	
10	91.1	89.6	87.9	7.2	12.0	11.4	12.5	5.3	92	75	80	02	1	03	2	03	1	9	10	10	7	0.0	• n, o 19	
11	84.0	85.0	81.1	10.0	11.2	11.2	11.8	8.7	98	91	93	32	1	28	2	24	1	8	10	10(+)	9(+)	4.7	• n, + a, p	
12	78.1	79.7	80.7	10.8	11.2	10.5	11.4	8.3	94	88	86	20	3	22	2	20	2	7	10	10(+)	10(+)	6.1	• n, + a, + a, p	
13	81.2	83.9	83.9	10.3	10.7	8.6	12.4	8.3	84	85	85	19	1	02	2	03	3	9	9	8	9	9(+)	+ o n, a, + p	
14	91.4	94.5	96.2	6.5	9.0	6.6	9.0	6.3	86	66	84	04	2	02	3	04	3	9	10	10	7	2.2	+ n	
15	01.6	03.2	03.3	6.7	8.7	7.0	9.3	4.2	70	58	82	04	1	02	1	03	2	10	7	8	7	0.3	+ n, a, o 14	
16	00.2	95.9	99.1	6.8	12.2	12.0	14.0	3.5	81	57	57	05	2	04	2	14	2	10	1	3	3	0.0	o a, p	
17	85.8	84.3	84.0	10.3	11.4	10.2	12.5	7.9	71	84	95	03	1	18	1	06	1	9	9	10	10(+)	0.0	• n, + a, + p	
18	85.9	85.2	86.4	12.0	12.0	13.2	13.9	9.6	95	91	76	18	1	19	2	17	2	10	10(+)	10(+)	4.5	• n, a, o 14		
19	82.6	85.5	86.0	14.8	15.4	15.4	16.4	9.1	75	64	64	19	5	20	4	20	3	10	4	8	9	6.2	+ n, + a, + p	
20	87.5	95.3	99.8	10.0	8.8	7.6	15.4	7.4	81	86	91	20	5	26	3	27	2	8	10	9	9	2.2	+ n, + a, + p	
21	03.1	02.0	00.3	7.8	8.7	7.9	10.7	6.1	73	74	82	18	2	28	1	04	2	10	9	7	10	8	3.2	• n, a, + p
22	98.4	98.1	95.1	7.4	9.8	9.0	10.0	5.9	85	67	67	19	2	16	2	18	3	10	7	6	10	0.6	• n, a, p	
23	92.2	98.9	03.3	9.3	9.5	9.0	9.8	7.9	91	96	96	18	3	23	2	18	3	5	10	10(+)	10(+)	5.3	+ n, a, p	
24	10.2	07.3	03.3	9.5	14.4	14.2	14.8	7.8	88	62	83	18	2	24	2	18	3	10	9	8	10	6.1	• n, o a, + p	
25	02.2	02.4	99.0	12.2	13.6	15.9	17.2	11.8	89	85	78	28	3	24	2	18	2	8	10	9	10	0.3	• n, a	
26	96.3	97.0	96.0	10.9	10.6	9.9	15.9	9.6	87	81	82	26	2	20	5	20	5	8	8	10(+)	10(+)	4.8	• n, + a, + p	
27	99.6	97.0	99.0	9.4	13.7	12.0	14.5	8.1	84	59	62	19	3	17	5	18	1	9	9	6	8	4.0	+ n, a, o a, p	
28	83.8	82.9	04.2	11.3	11.0	10.0	12.5	8.5	67	91	26	20	2	20	2	26	2	10	10	9	8	0.1	+ n, + a, + p	
29	82.2	85.3	88.0	11.1	9.4	8.9	12.8	8.7	72	84	72	20	3	28	3	04	2	10	6	9	8	11.8	• n, o a, o p	
30	84.0	86.0	87.4	7.9	9.2	7.5	9.3	6.4	81	76	88	28	2	24	1	26	1	9	10	10	9	2.4	• n, a, p	
31	92.3	94.3	98.7	5.7	5.2	4.4	7.5	3.6	74	83	67	01	1	06	1	01	2	10	9	8	2	4.9	• n, a, o 8, 14	
32	95.9	96.4	96.1	9.5	10.9	9.9	12.3	7.5	83	77	80	2.0	2	2.2	2.1	8.8	8.8	8.6	8.2	86				

# Extenso-Tabelle

1944

**Tromsø**

$\varphi = 69^{\circ} 39' N$

$\lambda = 18^{\circ} 57' E$

$g = 9.825$

$\Delta G = +1^{\circ}$

**September IX**

$H_s = 102 \quad H_b = 114.5 \quad h_t = 2.8 \quad h_a = 12.3 \quad h_d = 20.7 \quad h_r = 1.7$

Datum	Luftdruck P			Lufttemperatur T						Relative Feuchte U			Richtung und Stärke des Windes D.F.			Sicht	Bewölkung und Wetter N.w.			Niederschlag mm	Schneehöhe cm	Witterungsverlauf W		
	8	14	19	8	14	19	Max	Min	8	14	19	8	14	19	8	14	19	8	14	19				
1	91.9	88.7	87.0	3.8	7.4	6.1	8.1	0.7	76	57	72	00	0	04	2	04	1	10	1	2	8	1.1		
2	98.7	95.4	95.7	4.2	4.9	3.2	6.8	3.0	90	95	84	20	3	29	2	20	2	9	9	9	9	2.0		
3	97.9	98.6	97.4	2.8	3.1	3.2	4.8	1.5	90	95	84	20	3	22	2	18	4	9	10	8	9	6.0		
4	90.0	88.0	85.4	3.3	5.3	3.6	5.3	0.7	89	58	77	20	3	22	2	18	4	9	8	8	10	11.9		
5	83.0	89.6	91.0	2.8	4.1	2.4	5.2	1.3	86	69	92	28	4	26	1	24	2	9	10	8	9	10.2		
6	91.8	92.2	92.9	2.4	5.6	2.9	6.4	-	0.5	76	51	70	19	3	18	1	31	2	10	2	2	1	2.9	
7	94.9	97.6	99.2	2.7	6.3	4.5	7.1	-	0.1	81	50	64	31	1	01	1	01	1	10	1	3	6		
8	91.6	99.5	96.2	4.6	7.5	5.4	8.1	1.9	71	42	54	20	2	12	1	04	3	10	1	1	8	0.5		
9	86.7	87.0	88.5	5.6	8.1	6.1	8.1	3.6	85	71	90	04	2	05	2	04	1	9	10	0	10	0.5		
10	91.0	93.5	95.5	5.9	6.2	4.3	6.6	4.1	97	99	88	00	0	32	1	32	2	8	10	0	10	2.6		
11	00.7	04.7	07.4	4.9	6.8	5.1	7.8	3.5	90	81	72	18	2	22	2	24	1	9	9	9	8	10.5		
12	10.4	12.0	12.7	4.8	7.4	5.0	8.0	3.6	91	74	84	18	2	18	2	32	1	9	10	0	7	2.3		
13	15.7	13.7	14.1	4.3	9.2	7.8	9.6	1.9	85	64	92	18	2	18	3	18	3	10	1	10	0	1.0		
14	15.0	11.9	10.6	8.1	10.4	9.2	11.0	7.3	74	63	67	18	3	21	3	19	5	10	7	8	8	0.4		
15	08.4	07.9	06.5	8.1	8.3	9.3	10.3	7.4	71	84	77	18	3	22	3	18	3	8	9	0	10	0		
16	02.6	02.6	02.3	9.8	10.4	10.6	10.7	7.4	73	72	72	18	3	18	2	18	1	10	10	10	10	1.3		
17	01.3	01.6	01.9	9.8	10.6	12.2	8.7	8.7	81	77	00	0	0	18	2	19	3	8	9	10	0	0.5		
18	01.5	03.2	05.0	12.2	11.4	11.5	12.5	10.6	73	87	92	18	4	18	4	18	4	8	10	10	10	0.0		
19	04.0	06.5	07.3	15.3	14.6	14.5	15.1	11.1	80	68	65	20	5	20	5	21	5	10	10	9	8	3.4		
20	07.9	05.8	03.1	14.0	18.2	12.6	18.7	12.6	58	46	76	18	4	18	2	04	1	10	1	1	10	0.1		
21	98.5	04.8	06.4	10.9	11.0	10.6	13.6	9.2	76	56	62	17	4	20	4	20	4	10	9	8	10	0.6		
22	08.4	09.1	06.2	15.7	15.2	10.0	16.2	9.3	64	56	85	20	4	20	3	03	2	10	9	8	6	1.8		
23	04.9	02.7	01.7	7.2	13.2	11.0	13.3	5.8	92	56	54	26	1	20	3	18	3	9	5	4	1	1		
24	98.8	98.5	98.2	10.8	14.2	10.5	14.4	8.8	64	49	62	19	3	18	3	08	2	10	1	2	6	0.6		
25	94.6	92.6	90.2	10.7	13.6	10.8	14.5	8.6	62	51	62	11	1	15	4	18	3	10	8	7	7	0.1		
26	78.4	71.6	71.7	12.6	14.6	12.8	17.6	10.0	64	64	50	31	1	16	4	16	5	10	9	8	9	6		
27	75.1	73.2	75.3	12.3	13.7	11.7	13.8	9.6	49	44	40	10	2	16	4	16	5	10	9	8	2	0.0		
28	82.4	83.1	84.9	8.4	11.9	9.2	11.9	6.7	57	51	54	18	4	17	5	18	4	10	7	1	4	0.9		
29	86.6	86.6	88.9	7.8	9.7	8.2	10.3	6.2	52	44	48	18	4	18	5	19	4	10	4	8	6	0.9		
30	87.9	87.9	87.8	6.6	9.3	8.5	9.7	4.7	53	55	56	18	1	12	2	10	1	10	8	9	9	10		
M	96.6	96.9	97.0	7.6	9.7	8.1	10.6	5.7	75	64	70	2.4	2.6	2.6	2.6	9.5	6.9	6.8	7.0	60				

# Oktober X

1	86.4	87.1	87.6	7.4	8.8	7.4	8.8	6.9	68	60	79	19	3	00	0	18	1	9	10	10	10	1.9		
2	90.2	92.2	95.1	6.2	7.4	7.1	7.6	6.0	94	89	89	18	1	00	0	18	1	7	10	10	10	2.5		
3	95.2	98.7	03.4	6.7	7.0	4.5	7.6	4.1	85	87	87	18	3	00	0	04	2	9	10	10	10	7.2		
4	06.2	03.4	99.3	3.0	5.1	4.0	5.2	2.3	89	73	78	16	2	18	2	18	3	9	9	9	10	3.1		
5	80.6	86.4	91.1	3.8	2.9	3.8	4.1	0.7	80	86	66	18	2	30	3	30	4	6	10	9	9			
6	94.9	95.1	91.0	3.5	3.0	2.3	3.8	1.6	88	86	78	26	2	29	2	20	2	9	9	10	10	22.1		
7	85.0	85.1	85.9	0.9	2.8	2.3	3.0	0.1	90	75	85	18	1	24	2	28	2	10	8	8	10	3.0		
8	88.1	88.6	89.0	0.4	2.2	0.0	2.6	-	0.3	89	66	66	02	1	02	1	02	1	9	9	7	2	0.9	
9	91.3	91.3	87.1	0.0	3.6	3.6	3.6	4.5	-	1.6	75	70	83	22	5	26	2	18	3	10	9	10	0.3	
10	84.8	94.2	96.2	5.4	5.8	5.6	6.4	2.9	80	81	83	22	5	26	2	18	3	9	9	9	9	8.7		
11	96.9	96.6	95.6	7.8	8.2	7.0	9.0	5.3	85	74	83	18	3	18	2	20	2	9	10	10	10	1.4		
12	94.5	92.1	90.1	7.0	7.4	6.4	7.6	5.7	76	72	78	18	1	00	0	00	0	10	10	8	8	0.3		
13	92.2	95.4	91.2	9.0	9.7	7.2	11.0	6.1	77	71	82	20	3	20	2	18	2	10	8	6	3	0.7		
14	88.7	87.8	88.4	6.1	8.6	9.5	9.8	5.3	72	69	68	26	2	28	1	18	3	10	8	8	8	0.2		
15	86.7	84.7	83.9	5.5	8.2	7.0	9.5	4.1	82	64	64	19	1	24	1	16	1	9	8	9	10			
16	87.7	88.4	88.7	8.1	6.2	7.0	10.0	5.4	68	92	78	19	2	18	1	19	2	9	10	10	8	1.8		
17	89.9	88.6	84.6	5.1	6.2	5.8	8.0	3.9	76	63	59	20	3	16	1	04	1	10	1	6	2	1.6		
18	70.7	70.4	70.1	11.4	10.2	12.7	4.6	4.6	64	61	63	16	5	18	4	20	2	9	9	9	6	3.8		
19	69.6	73.4	75.2	8.8	9.8	8.8	11.2	8.2	79	64	64	17	4	19	3	00	0	10	10	8	10	1.3		
20	77.9	83.4	81.1	7.6	7.0	8.9	6.3	6.4	61	64	64	18	5	20	3	18	5	10	10	8	10	0.0		
21	94.9	00.9	03.9	2.0	2.1	2.0	7.0	1.1	92	95	88	20	2	23	2	20	2	9	9					

# Extenso-Tabelle

1944

**Tromsø**

$\varphi = 69^{\circ} 39' N$   $\lambda = 18^{\circ} 57' E$   $g = 9.825$   $\Delta G = +1^{\circ}$  November XI  $H_a = 102$   $H_b = 114.5$   $h_c = 2.8$   $h_d = 12.3$   $h_e = 20.7$   $h_f = 1.7$

Datum	Luftdruck P					Lufttemperatur T					Relative Feuchte U			Richtung und Stärke des Windes D.F.			> Sicht	Bewölkung und Wetter N,w			Niederschlag Z	Schneehöhe H	Witterungsverlauf W	
	8			14		19		8			14		19		8				14		19			
		8	14	19	8	14	19	Max	Min	8	14	19	8	14	19	8	14	19	8	14	19	8	14	19
1	96.3	97.5	96.7	1.6	1.1	2.3	2.3	0.6	83	91	82	80	0	20	3	19	4	10	9	1	8	4.6	4.6	• n, o a
2	90.9	89.9	89.3	5.6	5.9	7.2	7.2	2.0	63	53	39	19	5	19	5	20	3	10	10	9	10	0	0	o a, - 19
3	85.6	84.5	83.5	5.2	4.7	4.4	8.0	3.6	54	53	56	20	3	18	4	20	4	10	6	0	1	0	0	• p
4	75.1	71.9	67.8	3.4	3.5	3.4	6.2	1.6	71	68	79	24	2	04	2	00	0	10	10	8	10	0	0	• n, o a
5	68.4	64.5	63.8	3.9	3.2	2.9	4.0	1.6	69	52	69	19	3	20	3	20	3	10	3	8	8	8	4.5	4.5
6	63.4	66.5	69.8	2.1	2.8	2.9	3.5	1.0	76	75	83	18	2	18	3	19	3	10	10	9	8	8	0	• p
7	74.0	76.2	77.9	2.7	3.0	2.2	3.3	1.2	60	60	60	18	1	17	3	18	2	10	2	1	1	1	1	• o n, o a
8	84.3	88.7	89.6	3.2	2.5	1.4	3.3	0.7	59	58	59	18	3	04	1	00	0	10	3	8	2	10	10	0.1
9	89.5	91.2	92.0	3.1	3.6	3.5	3.8	0.6	63	67	61	12	1	18	3	20	2	10	1	1	1	1	0	o a
10	96.0	96.2	96.9	2.8	2.3	2.1	3.7	2.0	64	74	84	18	3	04	2	19	2	10	10	9	10	10	0	0
11	04.6	09.9	13.1	2.2	3.2	3.0	3.4	1.5	81	71	78	18	4	18	3	18	3	10	5	9	10	10	0.5	0.5
12	18.4	20.2	20.3	1.0	0.2	-0.4	3.2	-0.7	88	93	94	19	1	00	0	00	0	9	1	2	-	0	0	0.1
13	19.9	20.5	21.3	0.5	1.0	-1.0	1.3	-0.9	72	65	58	19	2	04	2	12	2	10	1	1	0	0	0	0
14	24.3	26.7	28.0	0.2	0.1	-1.1	1.4	-1.3	58	56	57	04	2	12	2	19	2	10	1	1	0	0	0	0
15	28.8	28.8	27.6	-1.4	-1.2	-1.7	-0.6	-2.4	57	55	60	18	2	18	1	02	2	10	1	1	0	0	0	0
16	23.4	21.2	18.8	-1.5	-1.1	-0.1	-0.1	-2.8	73	77	78	18	2	18	3	20	3	10	10	10	10	10	10	0.1
17	14.6	13.2	10.9	0.8	1.3	1.4	1.4	-0.2	88	88	88	18	3	19	3	19	3	10	10	10	10	10	10	0.1
18	05.4	02.3	99.0	0.6	-0.6	-1.9	1.8	-2.1	71	80	74	18	3	18	3	18	3	10	4	2	1	1	1	0.1
19	93.4	91.7	89.4	-2.4	-2.0	-1.4	-1.4	-2.8	65	58	62	20	3	20	3	20	3	10	7	9	7	7	7	0.1
20	84.3	82.2	80.9	-1.7	-1.6	-0.7	-0.6	-2.4	69	69	76	18	2	19	3	18	3	10	1	1	1	1	1	0.1
21	80.3	81.2	83.5	-1.5	-1.1	-0.4	0.0	-2.2	75	94	64	18	3	18	1	30	4	7	7	10	10	10	10	1.6
22	87.0	88.2	88.0	-3.3	-3.2	-2.5	-2.5	-0.2	69	72	76	02	3	00	0	18	3	10	6	8	5	5	5	12
23	84.8	82.1	78.6	-2.7	-4.0	-4.0	-4.0	-1.7	91	74	78	18	3	18	1	30	1	10	5	1	1	1	1	0.2
24	72.1	72.5	72.8	-3.3	-3.1	-3.0	-3.0	-5.4	69	67	95	18	3	18	2	24	1	10	5	10	10	10	10	12
25	76.0	78.6	80.6	-0.8	-1.1	-0.7	-0.7	-4.5	78	96	85	04	4	32	2	03	2	7	10	10	10	10	10	12
26	77.4	74.8	80.4	-0.5	-0.3	-1.1	0.0	-1.6	91	96	94	04	4	02	2	04	3	5	10	10	10	10	10	2.2
27	92.6	94.2	92.7	-2.7	-2.5	-1.7	-1.1	-4.6	72	67	45	18	3	18	4	18	5	10	1	8	7	7	7	24
28	97.9	90.8	91.4	-3.0	-3.6	-5.1	-0.1	-5.3	61	78	91	00	0	19	2	00	3	10	1	1	1	1	1	22
29	94.6	93.8	94.7	2.3	-0.2	1.8	3.8	-5.6	51	93	66	16	5	18	6	18	4	9	10	10	10	10	10	20
30	90.4	90.5	89.6	3.4	3.5	3.9	4.1	1.6	67	60	56	18	4	18	4	17	4	10	7	8	7	7	7	18
M	93.1	93.4	93.3	0.7	0.5	0.6	1.9	-1.2	70	72	72	2.6	2.4	2.4	9.5	6.0	6.2	6.2	31	5	5	5	5	

# Dezember XII

1	91.1	93.2	91.4	4.7	3.8	3.0	4.9	2.5	62	59	59	18	4	17	4	16	4	10	7	6	3	1	13	7
2	85.7	79.6	75.0	4.2	7.8	7.0	8.5	2.5	62	48	55	17	4	17	4	20	3	9	10	10	10	10	0	0
3	74.0	75.0	76.9	6.0	4.6	3.8	7.4	3.8	49	61	60	16	4	18	4	20	3	9	4	7	7	7	0	0
4	81.9	83.3	84.2	3.5	2.5	1.1	4.5	0.7	44	73	45	14	2	15	3	17	3	9	9	10	10	10	3	3
5	91.1	92.3	91.8	3.0	0.8	1.3	4.0	-0.2	47	56	60	15	3	16	3	16	3	9	10	9	10	10	0	0
6	89.2	90.5	92.3	2.9	3.1	2.3	3.8	0.2	45	49	53	18	4	18	3	18	3	10	7	8	4	4	4	4
7	93.6	92.6	93.5	-0.2	-0.8	-1.0	2.8	-2.2	57	56	52	17	5	18	6	18	4	10	6	6	2	2	2	- 19
8	96.0	98.9	91.0	-0.8	-0.4	-0.2	-0.1	-2.5	56	67	56	18	5	18	5	18	4	10	6	6	1	1	1	- 19
9	02.2	00.8	97.3	-1.8	-0.8	-0.7	-0.1	-2.2	56	58	58	18	4	18	4	18	4	10	6	6	10	10	10	- 19
10	84.6	83.2	81.4	-1.9	1.5	2.2	2.7	-2.2	65	48	50	18	5	17	5	17	5	9	8	8	0	0	0	- 19
11	85.0	88.4	92.3	3.5	1.9	2.2	4.3	1.5	41	60	51	16	5	17	5	18	4	10	5	6	1	1	1	- 19
12	97.4	94.7	92.9	-0.2	-1.9	-1.7	2.4	-2.9	63	68	77	20	3	00	0	00	0	9	1	8	10	10	10	- 19
13	97.2	94.4	10.2	-1.0	0.0	0.2	0.2	-2.1	92	86	86	18	2	19	3	00	0	8	1	10	1	1	1	- 19
14	18.4	19.1	18.7	1.0	0.4	-0.4	1.8	-1.1	79	69	69	00	0	19	3	20	3	10	1	2	1	1	1	- 19
15	15.1	15.1	15.0	1.0	0.3	0.3	1.0	-1.9	62	62	62	17	3	18	5	18	4	10	1	2	1	1	1	- 19
16	14.3	12.9	10.5	-2.2	-4.0	-4.9	0.4	-5.1	57	68	77	18	4	16	1	18	1	10	1	2	1	1	1	- 19
17	04.4	03.4	02.4	-																				

1944

## Røros

 $\varphi = 62^\circ 34' N$  $\lambda = 11^\circ 23' E$  $g = 9.819$  $\Delta G = +1^h$ 

Monat	Mittlerer Luftdruck P <sub>a</sub> hPa	Mittlere Luftdruck P <sub>a</sub> hPa	Mittlere Lufttemperatur T <sub>m</sub>				Lufttemperatur T				Windverteilung nD, F <sub>n</sub>																	
			8	14	19	Dics	Max	Min	Max	Min	Dec	N	NE	E	SE	S	SW	W	NW	C								
I	925.2	1001.8	-8.4	-8.1	-8.9	-8.8	-15.3	4.1	16	-42.0	10	85	1.9	2	1.0	39	1.6	5	2.0	39	3.4	7	2.5	179	2.7	44		
II	36.0	13.2	-8.2	-4.1	-6.9	-6.9	-11.9	2.1	23	-30.3	28	105	2.2	3	1.0	23	1.4	6	1.8	55	3.1	55	3.6	35	1.7	20	2.8	31
III	31.7	18.4	-7.6	-1.3	-5.3	-5.6	-11.4	5.1	26	-27.3	31	8	2.0	3	1.0	15	2.0	6	1.4	39	1.5	63	1.6	55	2.1	21	2.5	38
IV	37.3	14.0	-4.9	2.3	-0.5	-2.8	-8.7	7.3	10	-32.3	1	12	2.4	13	1.3	13	1.3	5	3.0	39	3.7	69	1.5	14	2.2	40		
V	40.2	16.3	1.0	5.6	4.1	1.7	-2.6	12.9	13	-13.9	7	26	2.0	49	1.7	2	1.5	2	2.8	5	2.8	5	2.3	229	2.3	22		
VI	35.5	09.6	7.6	10.8	9.1	7.8	4.2	18.7	28	-1.0	2	13	1.9	2	1.8	95	2.1	215	2.9	6	3.3	35	2.3	2	2.0	14	2.5	19
VII	40.0	12.6	12.7	17.5	15.7	13.5	8.7	27.4	9	0.7	26	27	2.1	2	1.5	103	1.6	115	2.7	39	3.1	7	2.3	4	1.4	109	2.5	19
VIII	39.6	12.7	10.5	16.7	15.1	11.9	6.2	25.2	3	2.2	31	20	2.1	13	1.3	23	1.8	6	3.1	39	3.7	11	2.7	39	2.3	115	2.5	34
IX	38.0	12.5	5.3	9.6	7.6	6.5	3.0	17.6	19	-3.7	14	95	1.8	25	1.8	59	1.6	18	2.4	7	3.2	7	3.1	15	3.0	8	1.9	31
X	37.1	12.5	2.2	5.4	3.1	3.1	0.3	10.9	10	-7.9	22	03	1.0	0	-	4	2.6	21	5.0	145	5.1	65	2.6	5	1.7	65	2.5	35
XI	30.6	07.0	-5.2	-5.2	-4.5	-4.6	-8.6	3.1	5	-25.5	28	43	1.3	15	2.3	103	2.5	17	2.7	7	3.1	5	3.4	0	-	75	2.1	37
XII	34.4	11.1	-4.7	-3.6	-4.0	-4.2	-8.3	4.2	24	-20.8	14	3	2.0	39	1.3	12	2.2	20	2.8	75	3.1	95	2.6	75	3.1	9	2.5	21
1944	935.5	1011.0	0.0	4.0	2.0	1.0	-3.7	27.4	-42.0	1425	2.0	27	1.4	64	2.0	1385	2.6	71	3.0	71	2.8	51	2.2	162	2.5	371		

## Alvdal

 $\varphi = 62^\circ 1' N$  $\lambda = 10^\circ 40' E$  $g =$  $\Delta G = +1^h$ 

I			-10.5	-8.3	-10.2	-10.0	-17.0	6.0	16	-39.0	10	215	3.2	0	-	39	2.5	0	-	0	-	2	1.5	75	2.3	23		
II			-8.2	-2.7	-5.8	-6.2	-11.9	5.4	24	-30.5	28	235	3.0	0	-	29	2.4	1	3.0	0	-	16	1.5	19	6.0	16		
III			-7.8	-0.3	-3.8	-4.9	-10.8	5.3	6	-24.2	2	6	3.5	0	-	28	1.9	0	-	0	-	32	2.5	1	3.0	26		
IV			-3.0	4.3	2.0	-0.8	-6.7	10.4	27	-26.8	1	15	2.5	0	-	22	2.0	1	1.0	7	1.6	0	-	24	1.5	5	6.5	18
V			3.5	8.3	6.5	3.7	-1.8	16.2	15	-10.7	7	42	2.4	0	-	15	2.1	0	-	5	1.3	0	-	21	1.7	1	2.0	11
VI			9.0	12.1	11.0	9.0	4.5	20.8	19	-2.8	1	18	2.5	0	-	35	1.6	0	-	1	1.0	155	1.3	03	1.0	20		
VII			14.5	18.8	17.3	14.5	0.4	29.3	6	-1.4	26	22	2.0	1	1.0	35	1.2	0	-	1	3.0	0	-	17	1.4	0	-	17
VIII			12.1	18.7	15.9	13.1	6.5	27.0	3	-1.8	30	18	1.8	1	3.0	39	2.0	5	1.2	1	1.0	15	1.1	0	-	16		
IX			6.2	10.4	8.4	7.3	4.0	16.4	19	-2.4	10	6	1.2	0	-	45	1.8	0	-	3	1.3	0	-	16	1.1	0	-	20
X			2.5	6.1	3.4	3.3	0.1	16.2	7	-6.7	22	4	2.2	0	-	65	1.7	0	-	0	-	2	1.0	0	-	21		
XI			-5.1	-3.1	-4.9	-4.7	-9.3	3.8	5	-28.9	28	1	1.0	0	-	42	2.4	0	-	0	-	205	1.5	13	1.0	23		
XII			-4.3	-4.0	-4.5	-4.4	-8.0	3.2	2	-22.2	14	3	2.3	0	-	63	1.9	0	-	2	2.0	0	-	59	3.5	03	5.0	19
1944			0.7	5.0	2.9	1.7	-3.5	29.3	-39.0	180	2.5	2	2.0	4523	1.9	59	2.0	22	1.5	1	1.0	1865	1.6	165	3.3	232		

## Engerdal

 $\varphi = 61^\circ 41' N$  $\lambda = 12^\circ 1' E$  $g =$  $\Delta G = +1^h$ 

I			-8.8	-7.7	-8.0	-8.5	-14.2	1.7	6	-30.7	10	255	1.5	0	1.0	0	-	59	1.8	22	1.8	6	2.4	86	2.1	25	1.6	0
II			-7.8	-3.9	-5.2	-6.0	-10.9	3.4	25	-29.3	28	32	2.2	0	-	29	2.4	1	3.0	0	-	16	1.5	19	6.0	16		
III			-6.5	-1.3	-5.2	-5.3	-10.7	5.4	28	-21.7	2	355	1.7	0	-	4	1.2	275	1.5	13	1.0	22	1.4	22	1.6	26		
IV			-3.5	3.6	0.7	-1.6	-7.2	12.3	10	-25.9	1	27	1.8	0	-	75	1.8	42	1.8	43	2.1	0	-	8	1.4	1		
V			2.7	7.8	6.5	3.4	-2.0	15.9	15	-11.2	7	415	2.5	0	-	0	-	6	1.3	235	1.6	65	1.8	1	2.0	115	1.6	1
VI			0.5	11.3	11.0	8.7	4.5	19.5	19	-1.9	2	11	2.6	0	-	85	1.9	925	1.5	19	1.8	23	2.0	125	1.9	4		
VII			13.4	18.1	16.9	14.1	9.0	26.2	8	1.6	26	20	2.0	0	-	12	2.1	25	1.6	6	1.3	0	-	16	1.6	4		
VIII			11.8	17.8	16.0	13.0	7.3	25.0	5	0.2	14	145	1.8	1	2.0	0	-	16	1.9	43	1.8	2	2.2	19	1.0	11	1.2	4
IX			7.1	9.9	8.8	8.7	4.4	16.3	19	-2.0	10	105	1.6	33	1.0	0	3.0	123	1.3	335	1.9	55	2.2	3	1.0	11	1.3	10
X			5.1	6.1	3.7	3.7	0.3	17.1	7	-4.3	22	145	1.1	0	-	7	2.3	485	1.8	1	2.5	0	-	25	1.0	15		
XI			-2.9	-1.3	-2.2	-2.7	-6.4	-6.4	2.5	-24.8	28	145	1.5	0	2.0	0	-	7	3.6	32	2.1	2	2.5	0	-	95	1.2	11
XII			-2.4	-1.7	-2.0	-2.1	-4.2	5.0	2	-14.5	14	23	1.2	0	-	1	2.0	15	2.4	45	2.2	0	-	0	-	57		
1944			2.4	6.2	4.0	3.1	-1.0	30.4	-28.4	1325	1.4	141	1.4	39	1.3	15	2.3	3055	1.8	61	1.9	215	1.5	55	55			

## Dombås

 $\varphi = 60^\circ 4' N$  $\lambda = 9^\circ 7' E$  $g = 9.819$  $\Delta G = +1^h$ 

I			924.0	1002.2	-6.5	-5.6	-6.3	-6.4	-2.2	-10.8	7.0	15	-28.1	10	8	1.2	0	-	1	1.0	35	1.3	7	1.4	10	2.1	47


<tbl\_r cells="22" ix="2" maxcspan="1" maxrspan="1" used

## Jahresübersichten

1944

$$H_0 = 628 \quad H_b = 630.0 \quad h_2 = 1.0 \quad h_3 = \quad h_4 = 14.4 \quad h_5 = 1.9$$

Ratios

$H_1 = 48$      $H_2 =$      $H_3 = 1.0$      $H_4 =$      $H_5 =$      $H_6 = 1.5$

Alvdal

$$H_0 = 479 \quad H_b = \quad h_t = 2.0 \quad h_c = \quad h_{\ell} = 15.0 \quad h_r = 1.0$$

**Engerdal**

$$H_0 = 253 \quad H_b = \quad h_t = 1.9 \quad h_s = \quad h_d = 14.5 \quad h_r = 1.6$$

Ytre Rendal

1944		1945		1946		1947		1948		1949		1950		1951		1952		1953		1954		1955		1956			
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26		
7.5	8.8	5.8	29	11	14	18	12	7	10	1	12	10	18	15	11	12	12	12	19	19	12	12	12	17	2	13	
6.2	5.6	4.9	12	3	4	6	23	4	8	5	9	20	6	15	4	12	5	12	12	12	1	1	0	0	5	31	
7.1	5.8	5.1	23	7	2	17	19	4	2	21	15	20	12	17	10	12	1	1	1	1	0	0	0	0	0	24	
7.1	6.0	6.7	19	1	17	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	19	
5.5	5.1	4.7	35	15	15	17	39	15	4	0	0	0	0	0	0	0	1	19	18	11	8	4	0	0	0	0	
6.9	7.5	7.5	99	15	13	17	39	9	13	0	0	0	0	0	0	0	0	14	10	3	14	18	0	0	0	0	
5.2	5.2	5.6	39	23	21	0	80	9	0	0	0	0	0	0	0	0	0	18	10	3	14	18	0	0	0	0	
4.8	5.5	5.7	80	23	21	0	0	0	0	0	0	0	0	0	0	0	0	18	10	3	14	18	0	0	0	0	
8.8	8.2	7.9	72	12	10	1	39	13	18	10	17	22	17	14	4	1	0	0	11	7	17	17	0	0	0	0	0
8.1	6.8	7.4	5	5	5	23	5	19	23	0	0	21	11	12	7	1	0	0	0	0	7	15	1	0	0	0	0
8.1	7.4	7.4	38	5	5	23	5	19	23	0	0	21	11	12	7	1	0	0	0	0	0	0	0	0	0	0	
8.2	7.8	8.1	43	6	6	6	43	6	19	23	0	0	42	17	14	7	1	0	0	0	0	0	0	0	0	0	
7.0	6.6	6.4	528	25	192	14	111	14	1	0	0	46	192	111	14	1	0	0	121	85	3	12	0	2	0	6	36

$$H_0 = 643 \quad H_0 = 647.1 \quad h_0 = 1.9 \quad h_0 = \quad h_0 = 10 \quad h_0 = 1.9$$

Dombis

1944

## Fokstua

Monat	Mittlerer Luftdruck P <sup>c</sup> Std. hPa	Mittelbare Luftdruck P <sup>a</sup> Std. hPa	Mittlere Lufttemperatur T <sub>m</sub>				Lufttemperatur T				Windverteilung nD, F <sub>m</sub>																		
			8	14	19	Dies	Max	Min	Max	Dat	Min	Dat	N	NE	E	SE	S	SW	W	NW	C								
			I	II	III	IV	V	VI	VII	VIII	VIII	IX	X	XI	XII	1944													
I	-7.4	-6.3	-6.9	-7.2	-11.7	-3.4	15	-31.6	10	1	3.0	6	2.2	0	-	4	4.0	145	3.7	35	3.4	16	3.9	19	3.0	17			
II	-9.1	-6.5	-8.5	-8.5	-13.1	0.2	1	-26.4	28	13	2.0	55	1.4	4	1.2	5	3.9	185	4.5	195	3.6	9	3.4	3	3.8	21			
III	-8.8	-3.7	-7.7	-7.7	-15.2	4.6	9	-26.5	31	1	1.0	53	2.1	33	1.5	23	1.0	11	2.1	27	2.9	145	3.1	5	3.9	23			
IV	-4.3	0.0	-2.6	-3.8	-8.5	4.3	13	-26.3	1	1	4.0	85	1.9	23	1.4	5	4.3	14	3.7	24	2.6	123	3.6	45	4.4	18			
V	0.4	3.5	1.9	0.2	-4.0	9.4	27	-16.7	6	5	2.6	24	3.0	33	2.9	4	4.1	4	2.9	225	3.1	125	2.9	125	3.0	5			
VI	5.9	8.8	7.8	6.0	2.0	15.4	19	-5.6	24	23	2.6	195	2.5	3	2.5	15	4.1	145	3.4	23	2.8	75	3.1	4	4.0	1			
VII	11.4	15.3	13.2	11.2	5.7	23.8	8	-3.5	25	2	2.2	23	2.7	8	2.2	13	3.0	155	2.8	155	2.6	5	2.3	25	1.2	10			
VIII	10.2	14.6	12.5	10.1	4.3	23.5	24	-1.5	30	0	3.0	9	2.1	15	1.3	75	4.8	25	3.0	28	11	2.9	15	2.3	9				
IX	4.1	7.6	5.4	4.7	1.1	15.0	19	-4.7	27	23	2.0	73	2.6	6	2.2	11	3.7	255	3.2	265	2.4	23	2.4	0	1.0	8			
X	0.5	3.6	1.3	1.4	-1.5	0.4	7	-9.4	22	2	1.5	45	1.2	23	3.8	18	4.2	25	4.4	17	2.5	9	3.4	0	-	15			
XI	-7.2	-5.2	-7.3	-6.9	-12.2	2.8	13	-25.9	28	23	2.2	45	2.1	10	4.6	115	4.7	25	4.2	7	2.8	0	3.0	1	3.0	28			
XII	-5.7	-5.0	-5.8	-5.6	-9.2	2.5	24	-22.6	14	23	3.0	85	2.0	63	3.1	9	5.1	225	4.9	25	4.2	6	2.4	3	2.5	10			
1944					-0.8	2.2	0.3	-0.5		-5.0	23.8	-31.6	24	3.0	126	2.5	51	1.8	104	3.5	215	3.3	268	3.1	106	3.2	39	3.2	165

## Vinstra

Monat	Mittlerer Luftdruck P <sup>c</sup> Std. hPa	Mittelbare Luftdruck P <sup>a</sup> Std. hPa	Mittlere Lufttemperatur T <sub>m</sub>				Lufttemperatur T				Windverteilung nD, F <sub>m</sub>																		
			8	14	19	Dies	Max	Min	Max	Dat	Min	Dat	N	NE	E	SE	S	SW	W	NW	C								
			I	II	III	IV	V	VI	VII	VIII	VIII	IX	X	XI	XII	1944													
I	-11.1	-9.2	-10.6	-10.8	-15.6	6.1	30	-27.7	10	2	2.5	1	3.0	2.0	0	-	0	-	4	4.1	16	3.2	66						
II	-6.6	-1.4	-4.4	-4.8	-9.8	8.7	22	-22.0	28	23	3.2	19	3.7	6	3.3	53	3.2	2	2.0	1	12	3.5	149	3.8	43				
III	-6.4	-1.5	-1.6	-3.3	-8.5	7.3	26	-18.2	2	33	1.1	15	2.3	5	2.3	23	3.2	2	2.0	1	2.0	7	3.7	155	4.4	55			
IV	-0.3	6.2	4.2	1.5	-5.8	15.2	27	-18.9	1	0	-	0	-	12	2.6	85	2.9	49	1.8	0	-	19	3.1	15	3.4	55			
V	5.5	11.8	10.0	6.7	1.0	18.4	28	-6.7	6	4	4.1	85	2.8	12	3.0	43	2.9	2	2.0	0	-	155	3.4	159	3.4	31			
VI	10.3	14.6	13.4	11.0	6.6	23.5	19	0.5	24	4	3.8	6	3.5	16	3.0	16	3.2	4	3.5	0	-	7	3.5	6	3.7	31			
VII	13.9	20.9	18.8	15.9	10.6	30.3	9	3.7	25	1	4.0	2	2.0	10	2.8	143	3.2	35	2.6	3	2.3	5	2.6	1	3.0	53			
VIII	11.8	20.1	18.0	14.4	8.6	27.6	3	1.1	30	0	-	0	-	9	3.4	12	4.1	0	-	0	-	12	3.2	6	4.0	54			
IX	7.1	11.6	9.9	8.5	5.6	15.9	14	-1.7	29	2	5.0	1	4.0	18	2.9	8	3.0	0	-	0	-	3	3.2	2	3.0	56			
X	2.3	6.9	4.6	4.0	1.1	15.9	7	-4.7	22	0	3.0	15	3.0	7	3.3	13	3.1	1	3.0	0	-	6	3.0	3	3.0	61			
XI	-4.2	-2.1	-3.9	-3.7	-6.9	5.7	6	-22.2	28	0	2.0	75	2.5	12	2.5	75	3.5	1	1.0	0	-	13	2.3	6	2.2	52			
XII	-5.0	-3.9	-4.2	-4.5	-7.2	3.8	2	-16.7	14	4	1.6	3	3.3	63	3.5	7	2.8	15	3.0	0	-	59	3.5	179	2.6	48			
1944					1.4	6.4	4.5	2.9		-1.5	30.3	-27.7	24	3.0	335	2.9	1159	2.9	995	3.2	21	2.4	6	2.0	975	3.3	118	3.4	583

## Vollen i Slidre

Monat	Mittlerer Luftdruck P <sup>c</sup> Std. hPa	Mittelbare Luftdruck P <sup>a</sup> Std. hPa	Mittlere Lufttemperatur T <sub>m</sub>				Lufttemperatur T				Windverteilung nD, F <sub>m</sub>															
			8	14	19	Dies	Max	Min	Max	Dat	Min	Dat	N	NE	E	SE	S	SW	W	NW	C					
			I	II	III	IV	V	VI	VII	VIII	VIII	IX	X	XI	XII	1944										
I	-6.3	-4.9	-6.1	-6.2	-10.7	7.9	15	-24.4	10	8	1.4	55	1.2	0	1.0	24	1.0	1	1.0	09	3.0	05	3.0	37	3.4	16
II	-8.8	-2.8	-5.3	-6.3	-11.2	6.5	22	-23.9	28	35	1.1	05	1.0	09	1.0	155	2.3	1	5.5	1	5.5	0	-	34	2.3	31
III	-7.1	-1.9	-3.5	-3.4	-8.3	9.5	26	-16.9	2	63	1.9	05	1.0	0	-	05	2.0	0	-	0	-	395	3.1	28		
IV	-1.5	6.5	3.4	1.0	-4.3	11.3	13	-19.6	1	4	1.5	1	1.5	2	2.5	22	1.7	2	1.2	2	3.0	0	-	30	3.5	27
V	5.5	11.7	9.0	6.2	0.4	20.1	18	-8.0	7	45	3.0	55	2.1	0	3.0	75	2.2	1	3.0	3	1.7	0	-	53	2.8	18
VI	10.0	14.9	12.7	10.4	5.3	25.1	19	-1.2	24	43	2.0	55	1.0	1	2.0	155	2.3	3	2.2	125	2.4	0	-	28	2.7	31
VII	14.0	20.6	18.2	15.4	9.6	30.1	8	2.9	26	33	1.9	3	1.5	0	-	10	1.9	8	1.8	14	1.8	0	-	89	1.6	46
VIII	12.3	20.0	16.7	14.1	8.3	26.8	3	0.0	30	2	2.8	0	-	0	-	175	1.8	7	1.6	43	2.0	0	-	163	2.9	45
IX	7.0	11.3	8.4	7.9	4.0	13.5	19	-1.5	27	1	1.0	1	1.0	4	1.0	0	-	113	1.8	3	1.7	35	1.6	0	-	71
X	3.0	6.2	4.0	3.9	1.4	11.5	7	-4.0	22	13	1.0	0	-	2	1.0	55	1.0	19	1.0	39	1.0	0	-	89	1.1	65
XI	-5.0	-2.9																								

## Jahresübersichten

194

Monat		Mittlere Relative Feuchte U <sub>m</sub>		Mittlere Bewölkung N <sub>m</sub>		Niederschlag R		Zahl der Tage n										Fokstua															
Monat	H <sub>t</sub> = 922	H <sub>b</sub> =	h <sub>c</sub> = 1.8		h <sub>a</sub> =		h <sub>d</sub> = 6.8		h <sub>r</sub> = 1.5		Zahl der Tage n										Fokstua												
			8	14	19	Dien	8	14	19	Σ	Max	Dec	Lufttemperatur T	Niederschl. R	Windstärke r	Regen	Schne	Raupe	Nebe	Rei	Front	Hag	Gefü	Dun	Neb	Sonne	Wand	Bewöl	Schne	Wand			
I			7.1	6.9	6.1		55	25	7	7	30	14	16	16	0	0	16	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
II			7.1	5.8	5.6		25	9	8	29	18	16	16	0	0	16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
III			7.6	6.7	6.8		28	6	1	31	21	18	18	0	0	18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
IV			7.2	6.9	7.4		24	7	17	30	11	11	11	0	0	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
V			6.0	5.9	6.3		26	7	15	24	4	13	13	0	0	13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
VI			8.0	7.9	8.0		59	15	10	5	0	16	15	1	1	16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
VII			6.7	7.1	7.1		101	25	11	2	0	14	12	3	2	14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
VIII			6.2	6.8	6.5		81	28	21	2	0	13	7	2	0	13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
IX			8.2	8.3	8.3		71	26	25	10	0	19	10	2	1	18	3	1	3	0	0	0	0	0	0	0	0	0	0	0	0		
X			7.5	7.8	7.0		25	16	18	20	0	11	4	1	1	10	2	1	3	0	0	0	0	0	0	0	0	0	0	0	0		
XI			7.6	6.6	5.5		26	5	20	30	17	15	8	0	0	14	4	1	3	0	0	0	0	0	0	0	0	0	0	0	0		
XII			7.5	7.8	7.4		25	5	2	31	13	19	9	0	0	18	7	1	2	19	2	0	1	0	0	0	0	0	0	0	0		
944							7.2	7.0	6.8	546	28	244	98	181	104	10	125	31	7	91	116	21	29	1	3	0	5	2	51	229	20	164	200

$H_0 = 241$	$H_0 =$	$h_r = 2.1$	$h_0 =$	$h_d =$	$h_r = 1.6$	Vinstra
I		7.0	7.1	4.7	32	10
II		7.1	5.7	4.6	4	14
III		7.2	6.5	6.5	11	31
IV		6.7	6.6	6.2	20	28
V		5.6	6.0	5.9	27	16
VI		7.8	8.0	8.6	101	7
VII		6.5	6.5	7.5	63	0
VIII		5.8	7.1	6.9	66	11
IX		9.5	9.4	9.5	94	15
X		8.7	8.3	7.5	31	18
XI		8.3	7.6	6.5	38	13
XII		8.4	8.4	7.5	47	30
1944		7.4	7.3	6.8	534	31
						198
					66	
					180	97
					15	13
					6	1
					0	118
					72	72
					7	7
					2	2
					0	0
					8	8
					2	2
					39	39
					262	262
					26	26
					177	177
					166	166

$H_4 = 635$	$H_6 =$	$h_t = 1.0$	$h_0 =$	$h_4 = 13.0$	$h_r = 1.6$	$\text{Åbjsrbräten}$
I		5.7	3.9	2.9	37	14
II		5.0	3.6	3.8	3	14
III		5.1	4.6	3.9	10	5
IV		6.1	5.4	4.9	14	5
V		5.7	5.2	5.0	33	14
VI		7.1	6.9	6.9	110	19
VII		5.9	6.2	5.8	123	20
VIII		4.5	5.8	5.9	128	21
IX		8.4	8.4	7.0	130	26
X		6.9	6.9	6.4	52	14
XI		7.6	6.2	5.8	72	18
XII		7.1	6.8	7.2	58	15
1944		6.3	5.8	5.5	770	40
					221	221
					66	66
					179	113
					25	25
					0	0
					108	81
					8	10
					0	0
					0	0
					10	10
					168	168
					79	231
					55	121
					180	

1944

## Røna

 $\varphi = 61^\circ 8' N$  $\lambda = 11^\circ 22' E$  $g = 9.819$  $\Delta G = + 1^h$ 

Monat	Mittlerer Luftdruck $P_0$ hPa	Sekundär- Luftdruck $P_1$ hPa	Mittlere Lufttemperatur $T_m$				Lufttemperatur $T$				Windverteilung n.D.F. $_m$																			
			8	14	19	Dts	Max	Min	Max	Dec	Min	Dec	N	NE	E	SE	S	SW	W	NW	C									
I	975.9	1004.3	-12.0	-8.4	-9.7	-10.5	-15.7	5.9	30	-30.4	10	10	1.0	0	-	0	-	5	1.2	5	1.2	1.0	0	-	72					
II	86.2	14.6	-8.8	-1.2	-2.5	-5.9	-11.4	7.9	25	-24.9	28	15	1.3	1	2.2	0	-	65	2.0	125	1.1	0	-	0	-	52				
III	81.1	0.9	-7.6	1.7	-2.2	-3.9	-9.6	7.3	7	-25.0	2	13	1.6	11	1.2	0	-	7	1.6	3	1.5	0	-	0	-	59				
IV	86.8	14.9	-1.2	5.6	2.9	0.4	-5.4	13.9	27	-21.7	1	13	1.5	2	1.0	0	-	0	125	1.4	53	1.4	0	-	0	-	57			
V	87.4	15.0	6.1	11.8	9.5	6.6	0.0	20.3	12	-7.7	7	40	1.9	9	1.2	2	1.0	0	-	115	1.5	15	1.0	0	-	2	2.0	27		
VI	82.0	08.9	10.7	14.6	15.0	11.0	6.3	25.3	19	-1.0	2	115	1.6	65	1.4	3	1.0	0	-	185	1.6	75	1.4	1	1.0	1	2.0	41		
VI	85.8	12.2	21.6	19.1	15.5	10.8	31.2	9	2.5	26	19	5	1.3	2	1.0	2	1.0	0	-	2	1.0	12	1.2	3	1.0	0	-	53		
VII	86.7	15.2	15.5	20.6	18.0	15.2	9.1	28.1	4	0.0	30	5	1.3	3	1.3	0	-	3	1.3	16	1.9	6	1.5	0	-	0	-	62		
IX	85.5	12.7	7.6	12.7	10.0	9.1	5.7	19.9	19	-2.0	29	5	1.2	4	1.0	0	-	0	155	1.1	55	1.5	0	-	0	-	60			
X	86.1	13.7	5.7	8.1	4.9	5.1	2.1	21.1	7	-3.2	9	43	1.4	05	1.0	1	1.0	0	-	2	1.0	235	1.4	65	1.5	0	-	0	-	55
XI	79.3	07.3	-3.1	-1.2	-2.6	-2.5	-5.3	8.0	5	-16.6	23	199	1.5	55	1.0	0	-	0	2.0	1.5	6	1.7	1	1.0	1	1.0	67			
XII	84.6	12.9	-3.6	-2.0	-3.5	-3.5	-5.8	4.7	2	-16.9	14	6	1.0	2	1.0	0	-	1	1.0	14	1.5	3	1.0	0	-	0	-	67		
1944	984.0	1011.6	1.7	6.9	4.5	3.1	-1.6	31.2	-30.4	1595	1.5	465	1.2	8	1.0	05	1.2	1435	1.5	65	1.3	3	1.0	4	1.8	660				

## Vang på Hedmark

 $\varphi = 60^\circ 48' N$  $\lambda = 11^\circ 11' E$  $g =$  $\Delta G = + 1^h$ 

I			-6.4	-4.6	-5.7	-5.9	-10.5	5.9	30	-25.8	11	6	1.8	175	2.0	25	2.3	85	1.9	55	2.4	65	2.0	85	3.0	105	2.7	7	
II			-5.6	-1.2	-3.5	-4.1	-8.6	7.1	22	-22.2	28	45	1.8	195	2.4	135	2.4	95	2.1	105	2.4	105	2.1	105	2.0	105	2.7	1	
III			-5.4	0.5	-1.7	-5.2	-7.5	6.8	10	-15.9	2	8	3.1	225	2.7	15	2.8	75	2.1	55	1.9	65	2.2	105	2.0	9	2.0	1	
IV			-0.1	4.5	5.5	1.1	-2.9	10.4	21	-16.0	2	5	1.5	19	2.5	175	2.4	155	1.4	85	2.2	85	2.5	85	2.5	85	2.5	2	
V			5.9	10.9	9.9	7.9	2.4	18.9	12	-4.9	5	10	4.4	145	3.6	16	2.8	75	2.1	10	3.3	115	3.0	10	4.0	115	4.0	40	
VI			10.0	14.0	12.8	10.9	7.3	25.8	20	-3.6	22	3.6	13	2.9	135	2.7	135	3.1	65	2.8	9	3.4	0	0	0	0	0	0	0
VII			15.1	20.0	18.8	16.2	11.6	29.0	8	6.8	1	3	2.7	16	2.8	18	2.2	11	3.1	165	2.4	6	2.2	195	2.1	2	2.8	1	
VIII			14.1	19.6	17.7	15.2	10.2	27.0	4	3.8	30	23	5.6	6	2.2	14	2.5	25	2.5	10	2.8	8	2.2	11	2.4	55	3.2	11	
IX			8.1	11.7	9.9	8.9	5.9	15.8	19	-1.2	29	15	3.0	25	2.2	175	2.8	135	2.1	105	1.7	45	1.8	6	2.2	15	2.7	12	
X			4.2	7.8	5.6	5.4	2.8	18.4	19	-1.9	9	5	1.6	125	3.0	24	2.9	205	2.5	45	2.3	25	2.0	65	2.5	25	2.0	15	
XI			-2.1	0.5	-1.4	-1.3	-3.9	8.7	5	-16.7	27	35	3.7	27	3.0	265	2.5	9	2.1	35	2.7	25	2.0	3	1.5	6	1.8	6	
XII			-2.6	-1.7	-2.7	-2.4	-4.8	4.8	2	-15.4	14	3	1.5	265	2.1	37	2.7	85	1.9	4	2.5	2	3.0	35	1.3	35	1.6	5	
1944			2.9	6.9	5.2	4.0	0.2	29.0	-25.8	555	2.8	224	2.7	2.7	235	2.6	1475	2.3	1025	2.5	75	2.4	115	2.3	77	2.7	65		

## Ø. Toten

 $\varphi = 60^\circ 48' N$  $\lambda = 10^\circ 53' E$  $g =$  $\Delta G = + 1^h$ 

I			-5.5	-3.7	-4.6	-4.9	-8.5	7.1	30	-21.4	10	65	2.2	6	1.7	05	2.0	0	-	125	2.2	105	2.4	305	2.1	2		
II			-5.0	-1.4	-3.5	-3.9	-7.5	7.0	22	-19.2	26	7	3.1	35	1.6	1.7	35	1.9	95	2.4	16	2.4	11	2.0	275	2.5	0	
III			-4.2	0.9	-1.4	-2.4	-6.0	6.3	26	-12.5	2	115	2.7	75	2.4	15	2.8	75	2.1	105	2.0	105	2.6	85	2.5	0		
IV			-0.1	4.6	3.4	1.2	-2.5	10.7	22	-14.5	1	145	2.3	65	1.8	10	2.1	15	1.7	95	1.8	95	2.0	155	2.0	0		
V			6.0	10.8	9.7	7.0	2.5	20.2	12	-4.7	5	255	2.8	16	2.1	10	2.2	05	2.0	55	3.0	25	3.4	75	1.9	255	2.8	0
VI			10.5	14.3	13.0	11.1	7.5	24.8	20	-3.1	20	155	1.7	18	1.8	11	2.0	10	2.0	125	2.9	25	2.8	165	2.6	0		
VII			15.4	20.1	19.2	16.4	11.8	28.9	8	6.7	26	105	2.2	21	1.5	145	1.4	7	1.9	135	2.6	8	2.1	195	1.8	1		
VIII			14.7	19.6	17.6	15.3	10.0	25.0	4	4.4	30	7	1.4	11	1.7	105	1.4	65	1.6	155	2.6	95	2.6	175	1.5	1		
IX			6.6	11.7	9.5	9.0	6.1	15.5	11	0.4	29	55	1.4	14	1.5	155	1.5	75	1.4	145	1.5	115	1.5	7	1.4	12	1.6	3
X			4.8	7.7	5.6	5.5	3.0	17.6	7	-1.8	31	35	1.3	145	1.4	15	1.4	14	1.8	135	2.2	45	2.1	5	1.7	135	1.5	0
XI			-1.6	-0.4	-1.5	-1.4	-3.9	9.4	5	-13.3	28	10	1.8	18	1.9	85	2.2	6	1.2	95	1.4	95	2.1	10	1.4	19	1.7	0
XII			-1.4	-0.8	-1.1	-1.3	-3.6	5.8	2	-10.8	13	3	1.7	95	2.4	55	2.7	145	2.7	135	3.4	22	3.5	12	1.9	13	2.3	0
1944			3.5	7.0	5.5	4.3	0.7	28.9	-21.4	120	2.2	1455	1.8	1135	1.8	755	1.9	1315	2.3	142	2.4	106	1.8	255	2.2	8		

## Kutjern

 $\varphi = 60^\circ 34' N$  $\lambda = 10^\circ 33' E$  $g =$  $\Delta G = + 1^h$ 

I	</td

## Jahresübersichten

1944

$$H_0 = 225 \quad H_0 = 225.6 \quad h_s = 1.3 \quad h_0 = \quad h_I = 8.8 \quad h_r = 1.2$$

Rena

$$H_1 = 222 \quad H_2 = \quad H_3 = 1.9 \quad h_1 = \quad h_2 = 14.7 \quad h_3 = 1.3$$

## Vang på Hedmark

I	82	78	79	80	7.3	7.0	5.3	25	9	24	31	16	9	4	0	0	0	2	8	2	0	0	0	1	14	14	3	12	29		
II	76	64	66	70	6.9	6.2	5.7	29	9	4	7	29	7	4	0	1	0	2	5	0	1	0	0	0	8	2	4	12	12		
III	74	56	60	66	7.6	7.3	7.2	13	5	6	2	31	9	12	4	0	1	2	9	3	2	0	0	0	7	6	4	16	31		
IV	74	56	58	67	7.2	6.7	6.7	17	8	25	18	4	9	4	0	1	0	2	8	3	2	0	0	0	7	6	4	20	19		
V	62	47	44	55	6.5	6.1	6.5	28	10	3	2	0	0	8	3	1	7	1	7	4	3	0	0	0	10	1	24	5	11	0	
VI	73	57	62	72	7.2	7.2	8.0	98	23	5	0	0	0	19	15	2	3	0	0	19	0	1	0	0	1	6	0	23	33	16	
VII	73	57	57	68	5.7	6.3	5.8	57	12	29	0	0	11	6	2	2	0	0	11	0	0	0	0	0	2	2	0	11	11		
VIII	77	52	58	69	5.5	5.7	6.7	94	34	21	0	0	13	8	2	2	0	0	13	0	0	0	0	0	3	7	0	27	0		
IX	86	69	79	81	8.3	8.6	9.2	128	30	9	2	0	0	21	13	7	1	0	0	21	0	0	0	0	0	11	6	7	22	0	
X	87	74	78	81	8.8	7.5	6.9	49	15	1	2	0	0	18	8	1	1	0	0	18	0	7	0	0	0	11	7	7	15	15	
XI	81	78	80	80	8.4	7.3	7.5	59	16	19	27	5	17	9	2	3	0	0	6	13	1	1	0	0	0	11	8	11	15	0	
XII	84	82	84	84	8.3	8.7	8.3	48	10	19	27	0	15	11	1	1	0	0	6	12	4	1	0	0	0	15	4	7	1	21	
1944	77	64	67	75	7.3	7.1	7.0	620	34	169	44	159	89	18	26	3	0	115	56	13	13	1	2	1	6	102	48	225	28	186	140

$$H_0 = 270 \quad H_b = \quad h_k = 2.0 \quad h_v = \quad h_M = 10.7 \quad h_r = 1.7$$

G. Toten

$H_1 = 493$        $H_2 =$        $H_3 = 2.0$        $H_4 =$        $H_5 =$        $H_6 = 1.8$

Kutjern

I	83	75	82	81	7.0	6.3	3.7	41	14	24	31	16	17	3	12	9	2	7	2	0	1	12	1	0	0	0	0	3	3	18	5	6	31		
II	80	61	75	74	6.6	5.8	5.3	13	5	5	29	17	15	0	11	4	0	0	10	0	0	11	0	0	0	0	0	3	3	25	2	9	29		
III	76	54	64	68	7.2	6.7	6.8	28	10	1	30	9	14	7	0	11	4	0	0	9	0	0	7	3	0	0	0	0	3	3	31	2	9	31	
IV	75	58	68	68	7.1	6.8	6.1	29	15	25	25	0	7	0	11	8	0	0	10	0	0	8	0	0	2	0	0	3	3	26	4	13	27		
V	62	53	60	62	6.2	6.5	6.6	50	15	15	19	0	0	1	0	12	8	2	10	2	0	8	7	0	4	0	0	1	3	1	27	2	11	27	
VI	75	62	67	74	7.0	7.0	7.2	132	24	13	29	1	0	0	0	20	18	5	5	5	0	0	20	0	0	2	0	0	3	3	25	1	12	25	
VII	76	58	62	71	6.2	6.5	5.3	90	31	21	0	0	0	0	2	14	10	2	5	3	1	0	15	0	0	0	0	0	5	5	6	6	14	0	
VIII	92	75	87	87	8.2	8.5	8.3	131	25	30	5	0	0	0	0	21	16	5	3	3	0	0	21	0	0	0	0	0	1	1	10	0	17	20	
IX	91	79	89	88	8.6	7.6	7.2	80	18	18	12	17	6	6	0	18	11	3	8	8	1	0	17	1	0	0	0	0	5	5	10	10	15	27	
X	90	86	88	88	8.6	7.6	7.4	112	31	9	30	14	4	0	0	20	12	3	5	5	1	0	6	21	1	4	6	0	0	3	3	12	10	14	31
XI	89	86	88	88	7.8	8.6	7.7	117	31	6	30	14	4	0	0	20	12	3	5	5	1	0	6	17	2	4	6	0	0	3	3	10	4	21	31
1944	80	67	74	77	7.2	7.0	6.6	904	31	212	73	62	8	180	124	31	82	14	1	117	85	9	24	0	0	7	0	0	34	66	272	26	153	184	

$H_2 = 10$      $H_3 = 10$      $b = 1.9$      $b_5 = 1.5$      $b = 0.2$      $b = 1.5$

Flick

Monats- und

1944

Vinger

$\varphi = 60^\circ 13' N$   $\lambda = 12^\circ 1' E$   $g =$   $\Delta G = + 1^h$

Monat	Mittlerer Luftdruck $P_0$	Mittlerer Luftdruck $P_{10}$	Mittlerer Luftdruck $P_5$	Mittlere Lufttemperatur $T_m$				Lufttemperatur $T$								Windverteilung $nD, F_m$														
				8	14	19	Dies	Max	Min	Max	Dec	Min	Dec	N	NE	E	SE	S	SW	W	NW	C								
I	-7.3	-4.3	-4.9	-5.7	-6.1	-4.3	-3.7	-8.9	-6.5	30	-26.9	11	129	1.1	33	1.7	13	1.0	6	1.9	10	1.8	133	2.1	15	2.4	23	1.4	8	
II	-4.7	1.9	-1.2	-2.2	1.3	6.0	3.3	1.9	-7.2	7.5	10	-15.9	17	253	3.1	7	1.4	13	1.0	7	2.0	3	2.0	35	2.3	4	2.6	27	1.7	2
III	6.9	11.9	10.0	7.4	11.2	14.7	13.8	11.5	1.5	20.8	12	-6.2	7	19	2.0	19	2.5	13	1.3	9	1.9	7	2.2	113	2.0	11	2.3	145	2.4	0
IV	11.2	14.7	13.8	11.5	16.2	20.5	19.4	16.5	7.0	24.5	20	-1.5	2	5	2.6	8	2.5	9	1.9	18	2.4	163	2.2	143	2.9	113	1.9	0		
V	15.5	20.7	18.1	16.1	18.5	22.7	20.5	18.1	10.6	26.8	8	3.4	26	73	1.9	5	1.3	10	1.2	17	1.6	243	1.6	8	1.4	10	2.2	10	1.4	1
VI	8.5	12.3	9.8	9.4	8.5	12.3	9.8	9.4	6.2	15.9	19	-1.5	29	10	1.2	8	1.6	9	1.9	123	2.9	17	2.1	113	2.1	13	1.5	3	2.8	6
IX	4.6	8.4	5.9	5.8	-1.1	0.1	-0.5	-0.7	3.0	17.7	7	-1.7	9	1.4	13	1.6	13	1.8	145	2.0	213	2.1	7	2.0	10	2.0	6	1.3	4	
X	-1.1	-0.6	-1.1	-1.0	-1.1	-0.6	-0.6	-0.6	-2.7	10.3	5	-17.4	28	263	1.9	193	2.4	3	2.2	8	1.5	63	1.5	6	4.5	19	1.0	12	1.2	7
XI	1944								-3.0	4.9	2	-11.7	13	113	1.2	33	1.4	17	2.5	19	1.6	11	2.2	93	1.2	9	1.4	103	1.4	2
									0.4	28.8	-28.9		168	2.0	102	1.9	803	1.8	1483	2.1	152	2.0	2.0	129	2.3	119	2.0	165	1.8	34

Sermarks

$\varphi = 59^\circ 48' N$   $\lambda = 10^\circ 48' E$   $g =$   $\Delta G = + 1^h$

Monat	Mittlerer Luftdruck $P_0$	Mittlerer Luftdruck $P_{10}$	Mittlerer Luftdruck $P_5$	Mittlere Lufttemperatur $T_m$				Lufttemperatur $T$								Windverteilung $nD, F_m$																	
				8	14	19	Dies	Max	Min	Max	Dec	Min	Dec	N	NE	E	SE	S	SW	W	NW	C											
I	-3.6	-0.9	-3.1	-2.9	1.0	-7.6	8.9	30	-21.0	11	139	1.1	5	2.6	45	1.4	2	1.0	173	1.9	73	1.5	6	2.2	0	-	37						
II	-4.5	0.8	-2.4	-2.7	1.4	-6.7	8.0	23	-18.1	28	179	1.8	11	1.5	59	1.3	3	1.3	93	2.7	7	1.3	29	1.0	31								
III	-2.3	2.8	-0.1	-1.0	3.9	-5.2	10.0	18	-12.2	25	9	3.1	16	2.6	25	1.8	8	1.6	14	1.7	93	1.6	59	1.9	09	1.0	28						
IV	2.3	6.9	4.6	5.0	8.0	-1.8	15.8	27	-10.9	2	23	2.4	165	2.5	5	2.0	23	1.0	23	1.9	123	1.8	7	2.0	13	2.0	21						
V	7.9	11.9	10.0	7.8	13.2	2.3	19.8	19	-5.9	7	11	2.6	36	2.4	1	1.0	09	1.0	188	1.5	143	1.8	19	2.0	8								
VI	11.6	15.0	13.5	11.6	16.5	6.8	24.1	19	1.6	9	5	2.4	173	2.9	6	3.5	73	1.8	30	2.6	105	2.0	35	1.7	0	-	10						
IX	16.9	20.6	19.6	16.9	22.3	11.2	29.9	9	4.4	26	2	1.8	133	2.8	13	2.0	69	2.1	223	1.9	169	1.5	4	1.1	0	-	15						
X	16.3	20.3	17.9	16.4	21.3	11.5	26.2	2	2.8	15	5	1.0	5	1.7	4	1.1	23	1.2	29	1.9	123	1.8	23	2.6	15								
XI	9.6	12.9	10.4	9.9	13.9	6.3	18.0	19	0.9	27	5	1.1	129	1.8	12	1.7	7	1.8	123	1.9	10	2.2	19	2.0	05	1.0	29						
XII	5.1	8.8	6.8	6.4	9.6	3.7	19.9	7	-2.7	31	5	1.5	155	1.9	8	1.7	63	2.4	205	2.0	12	1.9	0	-	05	-	25						
XIII	-0.6	1.5	-0.1	0.0	2.4	-2.6	10.6	5	-13.0	28	8	2.3	25	2.4	13	2.5	23	2.2	93	2.1	33	2.1	19	1.0	0	-	27						
XIV	-0.7	0.0	-0.6	-0.6	1.6	-2.6	7.1	2	-11.0	15	43	1.1	113	1.9	18	2.2	11	1.2	193	1.7	63	1.8	2	1.0	0	-	20						
1944									4.8	8.4	6.4	5.4	9.6	1.3	29.9	-21.0	88	1.9	185	2.3	91	2.0	593	1.6	2263	2.0	1353	1.8	393	1.8	7	2.1	266

Tryvasshaugda

$\varphi = 59^\circ 20' N$   $\lambda = 10^\circ 41' E$   $g =$   $\Delta G = + 1^h$

Monat	Mittlerer Luftdruck $P_0$	Mittlerer Luftdruck $P_{10}$	Mittlerer Luftdruck $P_5$	Mittlere Lufttemperatur $T_m$				Lufttemperatur $T$								Windverteilung $nD, F_m$										
				8	14	19	Dies	Max	Min	Max	Dec	Min	Dec	N	NE	E	SE	S	SW	W	NW	C				
I	-3.2	-1.7	-2.8	-2.8	-5.7	5.8	30	-13.6	11	129	2.5	1.3	3.0	4	4.5	09	2.0	12	2.8	28	2.3	15	2.5	193	3.3	0
II	-4.4	-1.4	-3.7	-3.6	-6.1	6.4	24	-12.0	28	19	3.9	12	2.5	73	1.3	49	1.9	7	1.7	133	3.0	5	2.0	143	2.6	4
III	-3.3	0.6	-2.0	-2.2	-5.3	5.8	6	-10.1	31	243	3.3	9	2.6	43	2.4	43	1.9	7	2.3	213	2.2	8	2.2	113	2.9	2
IV	0.7	3.8	1.8	1.1	-2.0	11.6	27	-9.6	1	93	3.1	6	2.1	89	2.8	89	2.0	20	2.4	22	2.2	39	2.6	10	3.8	0
V	5.8	8.9	7.1	5.9	2.3	16.3	28	-4.2	5	12	3.0	23	3.4	93	2.2	1	1.0	134	2.4	19	2.2	4	2.4	10	2.6	1
VI	9.1	11.8	10.7	9.4	6.6	20.8	19	-2.9	11	35	3.0	12	2.7	13	2.8	15	2.3	29	2.5	12	2.3	35	2.5	0	-	2
IX	14.3	17.2	16.5	14.9	12.0	25.6	9	6.8	24	2	2.2	12	2.9	19	2.2	173	2.1	213	2.3	2	1.0	0	-	2		
X	13.7	17.0	15.2	14.2	11.4	22.4	5	6.1	15	2	3.0	53	2.4	6	2.2	10	2.0	45	2.6	113	2.7	49	2.3	53	2.8	3
XI	7.4	10.0	8.4	8.0	6.1	14.6	19	0.9	29	63	2.2	14	2.6	20	2.4	113	2.5	20	2.5	63	2.4	19	3.7	5	2.7	



Monats- und

1944

Dikemark

Monat	Mittlerer Luftdruck $P_0$	Mittel Luftfeuchtigkeit $P_{d0}$	Mittlere Lufttemperatur $T_m$				Lufttemperatur $T$				Windverteilung nD, F <sub>m</sub>																		
			8	14	19	Dics	Max	Min	Max	Dec	Min	Dec	N	NE	E	SE	S	SW	W	NW	C								
			-4.8	-2.2	-4.3	-4.5	1.1	-11.2	9.0	30	-23.1	11	1	2.0	29	1.0	4	1.1	3	1.1	6	1.2	27	1.1	17	1.9	27		
I			-6.0	-0.2	-4.3	-4.4	1.1	-10.1	7.6	23	-23.2	29	2	1.0	3	1.0	105	1.0	15	1.7	2	1.0	45	1.0	245	1.2	15	1.0	24
II			-5.4	2.3	-1.4	-2.6	3.9	-8.1	8.6	18	-17.1	2	40	1.4	39	1.0	15	1.0	5	1.0	19	1.0	23	1.0	215	1.2	153	1.5	24
III			-1.3	6.1	3.7	2.0	7.4	-3.2	14.5	27	-16.4	2	4	1.4	29	1.2	13	1.0	75	1.0	11	1.0	33	1.6	8	1.6	103	1.1	30
IV			7.5	11.7	10.0	7.8	13.3	2.7	19.2	28	-5.0	7	9	1.1	89	1.1	22	1.2	5	1.0	109	1.0	6	1.2	4	1.1	10	1.1	18
V			11.7	14.9	13.4	11.7	16.6	7.4	24.6	19	3.4	24	13	1.0	8	1.0	39	1.0	125	1.2	119	1.3	6	1.2	25	1.0	3	1.0	6
VI			16.6	20.3	18.7	16.6	22.0	11.4	28.8	9	-5.4	26	43	1.1	11	1.0	27	1.1	165	1.2	15	1.5	13	1.3	19	1.3	20	1.2	14
VII			15.9	20.3	17.7	16.1	21.6	11.1	27.0	2	6.3	22	0	-	09	1.0	20	1.0	175	1.2	9	1.3	33	1.4	23	1.3	20	1.2	20
VIII			9.2	12.8	10.1	9.7	14.0	6.7	17.5	17	-0.4	29	2	1.0	59	1.0	225	1.0	4	1.0	6	1.2	50	1.1	6	1.2	25	1.2	36
IX			5.2	8.5	5.9	6.0	9.4	5.2	18.9	7	-3.2	31	2	1.2	9	1.0	225	1.1	6	1.0	9	1.1	35	1.5	63	1.2	35	1.1	29
X			-0.7	0.5	-0.4	-0.5	2.0	-3.1	11.7	5	-16.6	28	39	1.6	89	1.4	18	1.0	09	1.0	3	1.3	21	1.0	6	1.2	10	1.3	38
XI			-1.7	-0.8	-1.6	-1.6	1.0	-3.7	6.5	2	-12.6	13	09	1.0	19	1.0	20	1.1	0	-	4	1.0	7	1.4	16	1.2	5	1.2	39
1944			4.1	7.8	5.6	4.7	9.4	0.3	28.8	-23.2	349	1.2	64	1.1	233	1.1	82	1.1	96	1.2	575	1.2	127	1.2	985	1.3	305		

Modum

Monat	Mittlerer Luftdruck $P_0$	Mittel Luftfeuchtigkeit $P_{d0}$	Mittlere Lufttemperatur $T_m$				Lufttemperatur $T$				Windverteilung nD, F <sub>m</sub>																			
			-4.0	-1.2	-3.3	-3.2	-7.4	9.6	30	-21.0	11	3	1.0	0	-	3	1.3	0	-	16	1.2	275	1.1	245	1.0	19	1.0	0		
			-5.0	0.0	-2.4	-3.2	-7.8	8.0	7	-19.2	29	7	1.0	0	1.0	4	1.0	3	1.3	175	1.2	24	1.1	32	1.0	25	1.2	0		
I			-2.9	2.8	0.7	-0.8	-5.3	10.4	18	-12.2	5	11.9	1.6	0	1.0	4	1.0	59	1.3	175	1.2	15	1.2	23	1.2	0	1.2	0		
II			1.4	7.0	5.0	2.9	-1.7	15.0	21	-11.0	2	12	1.2	19	1.3	5	1.0	5	1.2	355	1.2	175	1.1	15	1.2	23	1.2	0		
III			6.6	12.7	10.7	8.0	3.0	22.0	12	-5.0	5	26	1.4	9	1.2	10	1.1	7	1.1	309	1.2	6	1.0	4	1.0	0	-	0	-	0
IV			11.7	15.7	14.5	12.2	7.6	25.6	20	3.0	24	7	1.6	69	1.5	143	1.7	11	1.1	409	1.3	73	1.1	2	1.0	1	1.0	0	-	0
V			16.3	21.2	19.7	17.1	12.1	30.6	8	6.4	26	39	1.1	3	1.2	65	1.3	5	1.3	619	1.2	73	1.3	5	1.0	1	1.0	0	-	0
VI			15.6	21.5	18.6	16.6	11.2	27.6	5	4.0	15	2	1.5	0	-	1	1.0	4	1.0	40	1.2	263	1.3	115	1.5	8	1.1	0		
VII			8.9	13.3	10.3	9.8	6.8	17.8	19	-0.6	29	8	1.0	4	1.0	105	1.3	12	1.1	185	1.4	13	1.0	155	1.3	85	1.0	0		
VIII			4.6	9.0	6.9	6.2	2.9	21.4	7	-3.0	31	3	1.0	2	1.0	6	1.3	4	1.5	20	1.6	26	1.2	205	1.1	115	1.0	0		
IX			-1.8	0.4	-0.3	-0.8	-3.1	12.2	5	-14.2	28	145	1.4	43	1.8	193	1.5	43	1.0	10	1.4	39	1.0	22	1.2	143	1.0	0		
X			-1.5	0.1	-0.6	-0.9	-3.3	6.8	2	-13.2	14	23	1.0	0	-	75	1.7	113	1.3	13	1.3	22	1.2	143	1.0	0	0	0		
1944			4.2	8.5	6.6	5.3	1.2	30.6	-21.0	100	1.3	323	1.3	915	1.3	725	1.2	310	1.3	1955	1.2	194	1.1	1015	1.0	0	0	0		

Nesbyen

Monat	Mittlerer Luftdruck $P_0$	Mittel Luftfeuchtigkeit $P_{d0}$	Mittlere Lufttemperatur $T_m$				Lufttemperatur $T$				Windverteilung nD, F <sub>m</sub>																			
			-8.4	-5.6	-7.2	-7.6	-12.5	9.1	15	-22.8	10	89	1.1	6	1.4	1	1.5	1	2.0	49	1.3	14	1.5	8	2.3	25	2.0	25		
			-8.2	-2.5	-5.6	-6.2	-11.5	5.4	7	-21.9	28	09	1.0	35	1.0	1	1.5	153	1.9	5	2.8	153	1.9	95	2.4	205	2.0	16		
I			-6.6	2.3	-0.6	-2.9	-8.3	8.3	26	-19.9	2	7	2.8	5	1.8	1.5	153	2.0	6	1.7	9	1.6	125	2.0	285	2.6	12			
II			6.2	12.8	10.4	7.4	1.9	20.2	27	-5.7	7	105	4.1	185	2.7	5	1.4	11	3.0	45	3.4	12	2.9	5	2.5	205	2.5	6		
III			11.2	15.8	14.4	11.8	6.8	24.5	19	-1.1	24	125	1.9	145	2.3	18	2.6	65	2.8	25	3.6	125	2.8	21	3.0	22	2.6	11		
IV			15.3	21.3	18.7	16.2	10.9	30.5	8	5.0	26	9	2.2	6	2	2.2	19	1.5	143	2.7	7	2.6	7	1.9	4	1.8	14	2.2	26	
V			13.1	20.7	17.2	14.8	9.3	27.5	5	2.5	30	89	2.8	73	2.1	0	-	185	3.0	65	3.5	4	2.4	4	2.0	18	2.6	13	2.2	32
VI			7.1	12.3	9.7	6.7	5.7	16.5	19	-1.5	29	35	2.0	2	1.0	2	1.0	45	1.8	13	2.3	105	1.7	11	1.7	23	2.0	32		
VII			2.5	7.5	5.2	4.5	1.4	21.7	7	-3.5	31	43	2.8	3	1.7	3	1.0	55	2.1	18	1.8	7	1.7	153	1.9	25	1.7	35		
VIII			-4.8	-3.2	-4.3	-4.4	-7.6	5.8	6	-22.2	28	23	2.4	4	1.1	45	1.1	55	1.4	45	2.6	9	1.1	45	2.3	21	3.7	32		
IX			-4.2	-3.4	-4.2	-4.1	-7.0	4.7	2	-18.0	14	2	1.5	5	1.2	0	-	55	1.4	25	2.0	0	-	6	3.5	265	2.0	20		
X			1.9	7.1	4.9	3.4	-1.2	25.3	-20.8	159	3.0	25	3.0	132	2.2	25														

## Jahresübersichten

1944

$$H_s = 180 \quad H_b = \quad h_t = 2.0 \quad h_a = 15.3 \quad h_d = 15.0 \quad h_r = 2.0$$

Dikemark

$$H_1 = 133 \quad H_2 = \quad H_3 = 2.0 \quad H_4 = \quad H_5 = 6.6 \quad H_6 = 1.3$$

**Modum**

$$H_1 = 164 \quad H_2 = \quad H_3 = 2.0 \quad H_4 = \quad H_5 = 11 \quad H_6 = 1.7$$

Nesbyen

I	85	79	81	82	6.7	6.4	3.9	22	8	24	30	18	10	6	0	3	0	0	2	10	1	0	0	0	0	0	0	2	0	6	7	31			
II	81	65	74	75	6.1	5.1	4.9	1	1	2	29	16	5	0	0	3	0	0	1	4	0	0	0	0	0	0	0	0	14	7	11	29			
III	77	54	58	66	7.1	6.4	5.4	6	4	1	29	11	8	1	0	3	0	0	7	7	0	0	0	0	0	0	0	0	23	1	8	31			
IV	77	52	54	66	6.7	5.6	6.3	7	2	16	22	5	8	3	0	2	0	0	4	4	4	0	0	0	0	0	0	0	1	20	4	14	12		
V	69	45	47	62	6.5	7.2	6.8	26	12	16	7	0	11	5	1	5	0	0	11	5	5	2	0	0	0	0	0	0	0	21	4	10	0		
VI	73	54	56	69	7.3	7.8	7.3	85	14	28	0	0	22	16	3	3	0	0	22	5	0	0	0	0	0	0	0	0	0	1	16	0			
VII	76	54	64	74	6.2	6.8	7.5	85	14	13	0	0	17	12	3	3	0	0	17	0	0	0	0	0	0	0	0	0	1	2	22	1	12	0	
VIII	81	53	65	74	5.1	6.6	6.6	65	18	29	0	0	15	12	3	2	0	0	15	0	0	0	0	0	0	0	0	0	5	0	3	22	3	8	0
IX	95	71	81	85	8.5	8.7	8.3	114	26	1	2	0	21	17	4	0	0	0	21	0	0	0	0	0	0	0	0	0	4	8	8	1	22	0	
X	74	74	85	85	8.4	8.3	7.0	58	21	18	13	0	16	9	2	0	0	0	16	1	0	0	0	0	0	0	0	0	5	10	9	0	19	0	
XI	88	85	85	86	7.8	7.1	5.9	55	12	20	27	9	15	10	2	1	0	0	10	14	6	0	0	0	0	0	0	0	2	10	9	4	18	21	
XII	91	87	88	89	7.5	8.2	7.6	52	18	9	30	7	15	10	2	1	0	0	7	11	3	0	0	0	0	0	0	0	10	5	0	1	17	31	
1944	82	64	70	76	7.0	7.1	6.5	580	26	189	0	66	165	103	19	21	0	0	131	54	17	14	0	2	0	10	33	33	163	33	162	155			

$$H_a = 795 \quad H_b = \quad h_1 = 1.9 \quad h_2 = \quad h_3 = \quad h_4 = \quad h_r = 2.6$$

Geilo

$$H_1 = 990 \quad H_2 = \quad h_1 = 2.0 \quad h_2 = \quad h_3 = 7.8 \quad h_4 = 2.4$$

Haugastøl

I	80	79	80	80	6.8	6.2	4.9	56	14	14	31	12	19	12	2	6	3	2	19	1	0	0	0	0	0	9	7	19	2	8	31	
II	74	69	72	72	6.6	4.9	4.3	16	5	8	29	15	15	5	0	2	0	2	1	19	1	0	0	0	0	0	6	2	27	7	7	29
III	76	66	69	72	6.6	5.0	6.9	18	6	19	31	18	10	4	0	5	2	1	0	10	0	0	0	0	0	0	1	1	30	6	6	31
IV	76	67	70	73	6.2	5.7	6.6	13	3	24	30	10	14	7	0	2	0	0	5	14	4	1	0	0	0	0	7	0	28	1	0	30
V	73	60	66	72	7.5	6.4	6.3	36	12	3	21	3	13	8	1	2	0	0	0	7	7	0	6	0	0	0	4	2	29	3	13	8
VI	72	62	65	71	6.6	7.1	6.7	74	36	5	5	0	17	13	1	0	2	0	0	17	1	1	0	0	0	0	4	0	23	3	13	0
VII	74	58	63	71	6.3	6.7	6.5	120	33	10	0	18	15	4	0	0	0	0	18	0	0	0	0	0	0	1	1	1	1	11	11	
VIII	72	56	65	69	6.1	6.7	6.5	114	45	21	0	0	14	10	3	0	0	0	0	14	0	0	0	0	0	0	1	1	26	3	12	0
IX	83	74	79	78	80	8.8	8.6	9.1	124	28	16	4	0	23	17	3	0	0	0	23	5	4	0	0	0	0	5	2	21	0	24	2
X	84	79	85	85	7.7	8.2	8.3	37	10	4	17	0	17	11	0	2	0	0	15	15	10	6	4	0	0	8	2	17	0	17	2	
XI	85	80	82	82	8.3	7.6	7.2	79	14	20	30	10	19	13	3	4	3	1	2	18	1	0	0	0	0	0	3	10	14	2	16	26
XII	86	84	84	85	8.1	7.8	7.6	53	14	9	31	11	19	11	1	2	1	0	2	18	0	0	0	0	0	0	10	10	12	1	20	31
1944	78	70	75	76	7.1	6.7	6.7	740	45	229	0	79	188	126	18	25	10	4	105	107	18	11	0	0	0	2	62	34	273	25	156	180

1944

## Dagali

 $\varphi = 60^\circ 25' N$   $\lambda = 8^\circ 36' E$   $g =$   $\Delta G = +1^h$ 

Monat	Mittlerer Luftdruck P <sub>a</sub> 700 hPa	Perpetuum T <sub>a</sub> °C	Mittlere Lufttemperatur T <sub>a</sub>				Lufttemperatur T						Windverteilung nD, F <sub>n</sub>															
			8	14	19	Dies	Max	Min	Max	Dec	Min	Dec	N	NE	E	SE	S	SW	W	NW	C							
			1	-4.9	-3.5	-4.8	-4.7	-7.9	3.8	16	-18.6	10	0	0	1.0	2	1.5	5	1.6	0 <sub>9</sub>	1.0	65	1.2	74	2.7	5	2.0	0
I	-7.5	-4.1	-6.8	-6.6	-10.3	-4.1	-10.3	-4.8	-20.9	22	-20.9	28	0	0	1.0	3	1.0	4	2.2	0	-8	2.2	62	1.6	7	2.6	1	
II	-6.0	-2.1	-4.7	-5.1	-8.5	-5.6	-8	-16.8	22	0	-	0	0	-	0	-	3	1.3	1.9	1.3	105	1.4	75	1.7	39	2.7	1	
III	-2.8	1.6	-0.1	-1.6	-5.4	6.8	16	-17.4	1	0	-	1	1.0	1	1.0	6	1.6	2	2.8	243	1.3	51	1.8	43	1.8	0		
IV	2.0	5.5	4.2	2.5	-1.2	12.8	13	-9.9	7	0	-	0	-	53	1.0	16	2.2	0 <sub>9</sub>	2.0	180	1.4	51	1.8	0 <sub>9</sub>	2.0	1		
V	7.0	10.1	8.9	7.1	3.3	18.7	19	-0.9	24	0	-	0	-	7	1.5	3	1.8	20	1.6	55	1.6	1	1.5	4				
VI	12.2	16.2	14.7	12.7	8.2	24.3	8	3.8	26	0	-	3	1.0	53	1.4	19	1.0	22	1.0	243	1.0	0	0	-	6			
VII	11.4	16.1	13.8	12.1	7.6	24.3	24	0.3	15	0	-	0	-	9	1.4	6	1.9	23	1.9	463	1.7	2	1.2	6				
IX	4.7	7.9	6.1	5.4	-0.5	13.2	19	-1.5	29	0	-	1	1.0	143	1.4	19	1.1	3	1.5	85	1.4	31	1.5	0	-	13		
X	1.1	4.1	2.1	2.0	-0.5	10.8	7	-6.1	22	0	-	0	-	14	2.4	113	2.2	25	3.2	14	1.3	29	1.5	0	-	22		
XI	-3.7	-3.9	-4.9	-5.1	-6.0	1.8	30	-19.3	23	0	-	3	1.0	22	1.7	6	2.1	0	-	9	1.1	41	1.5	1	1.5	8		
XII	-4.8	-4.1	-5.0	-4.8	-7.2	2.3	2	-16.5	14	0	-	0	-	26	1.7	6	1.8	0 <sub>9</sub>	3.0	6	1.3	403	1.8	0	-	14		
1944					0.6	3.6	2.0	1.2	-2.2	24.3	-20.9	0	-	9	1.0	1003	1.6	138	1.5	21	2.0	171	1.4	557	1.6	243	2.1	77

## Svane

 $\varphi = 59^\circ 46' N$   $\lambda = 9^\circ 35' E$   $g =$   $\Delta G = +1^h$ 

Monat	Mittlerer Luftdruck P <sub>a</sub> 700 hPa	Perpetuum T <sub>a</sub> °C	Mittlere Lufttemperatur T <sub>a</sub>				Lufttemperatur T						Windverteilung nD, F <sub>n</sub>															
			8	14	19	Dies	Max	Min	Max	Dec	Min	Dec	N	NE	E	SE	S	SW	W	NW	C							
			1	-5.3	-1.4	-5.5	-4.9	-11.5	8.5	30	-24.0	11	21	2.1	0 <sub>9</sub>	1.0	1	1.0	11	1.3	143	2.1	13	1.0	4	1.5	303	1.6
I	-6.4	0.5	-4.5	-5.1	-11.4	9.1	22	-24.4	28	22	2.2	1.9	2.0	2	1.0	89	1.7	12	1.8	25	1.0	2	1.0	263	1.5	10		
II	-5.4	4.1	-0.2	-1.8	-7.9	8.9	6	-18.0	5	243	2.7	1.0	0.3	1.0	103	1.6	15	1.9	0	-	4	1.4	213	1.8	16			
III	1.5	7.2	4.4	7.5	-3.2	14.2	27	-15.0	1	23	1.8	1.9	1.7	2	1.5	15	1.6	15	1.6	0 <sub>9</sub>	2.0	39	1.9	193	1.4	10		
IV	7.4	12.3	11.2	7.9	1.9	21.1	12	-4.9	7	453	2.3	1.9	2.7	1.5	10	1.7	10	2.1	0 <sub>9</sub>	3.0	1	2.0	19	2.4	4			
V	11.7	15.4	14.2	11.7	6.7	24.0	20	1.0	24	143	1.9	1.5	0.9	1.0	20	2.5	24	2.1	0	-	2	1.2	19	1.8	30			
VI	15.8	20.8	19.7	16.5	10.5	29.1	9	5.5	26	10	1.2	0	-	2	1.0	16	1.6	23	1.6	0	-	19	1.0	233	1.1	17		
VII	14.7	21.4	18.5	16.1	10.4	27.5	5	1.8	15	9	1.7	1	1.0	0	-	163	1.5	29	1.8	1.5	1.5	19	1.0	113	1.7	23		
IX	8.2	13.2	9.9	9.3	5.9	17.4	17	-2.2	29	113	1.7	1	1.0	1	2.0	85	1.7	103	2.0	0	-	0	-	153	1.8	44		
X	3.2	8.5	5.4	5.0	1.8	19.2	7	-3.9	2	203	1.5	1.5	0	-	10	1.6	22	1.9	0	-	1	1.0	243	1.4	14			
XI	-2.9	-0.6	-2.4	-2.4	-5.5	10.2	5	-19.8	26	273	1.7	2	2.0	0	-	7	1.4	83	1.6	0 <sub>9</sub>	2.0	1	1.0	403	1.6	3		
XII	-2.6	-1.2	-2.2	-2.2	-5.1	5.2	2	-16.9	14	21	1.7	0	-	0	-	113	1.7	173	1.9	0	-	43	1.0	223	1.4	16		
1944					3.2	8.4	5.7	4.4	-0.6	29.1	-24.4	250	2.0	12	1.7	103	1.3	1443	1.7	201	1.9	7	1.4	26	1.3	272	1.6	175

## Kongsberg

 $\varphi = 59^\circ 40' N$   $\lambda = 9^\circ 30' E$   $g =$   $\Delta G = +1^h$ 

Monat	Mittlerer Luftdruck P <sub>a</sub> 700 hPa	Perpetuum T <sub>a</sub> °C	Mittlere Lufttemperatur T <sub>a</sub>				Lufttemperatur T						Windverteilung nD, F <sub>n</sub>															
			8	14	19	Dies	Max	Min	Max	Dec	Min	Dec	N	NE	E	SE	S	SW	W	NW	C							
			1	-4.3	-1.9	-3.9	-3.9	0.6	-8.2	7.7	-20.7	11	153	1.5	0	-	0	-	15	1.3	15	2.3	7	3.3	16	1.7	38	
I	-5.4	0.4	-2.6	-3.5	-1.4	-8.3	6.7	23	-19.7	29	16	1.8	0	-	0	-	15	1.7	153	1.5	1	2.5	4	3.0	10	1.4	41	
II	-3.6	4.2	0.1	-0.9	5.1	-6.0	9.6	18	-12.4	5	7	1.4	3	1.0	5.0	0	-	15	1.7	12	1.1	43	1.2	6	1.5	24	1.8	33
III	1.3	7.5	5.8	3.1	8.7	-2.4	14.9	27	-12.2	1	5	1.5	3	1.3	2	1.0	-	283	1.2	153	1.5	7	1.7	213	1.9	15		
IV	7.8	13.7	11.2	8.5	14.7	2.4	22.9	12	-4.1	7	293	1.5	73	1.7	0	-	0	-	15	1.3	5	1.8	2	2.5	143	1.3	19	
V	12.0	16.1	14.8	12.4	17.5	7.6	26.6	19	4.0	24	59	2.0	59	1.5	4	1.8	53	1.8	313	1.7	3	2.0	15	1.5	133	1.6	20	
VI	16.4	21.6	19.4	17.1	22.7	11.9	29.4	24	7.2	16	6	1.4	1	1.0	1	3.0	73	1.5	36	1.4	15	1.7	2	1.8	8	1.8	30	
VII	15.0	22.1	19.0	16.9	22.5	12.1	26.1	5	4.8	15	53	1.1	1.5	1.3	1.7	43	1.5	37	1.4	7	1.7	23	1.8	105	1.6	23		
IX	8.8	13.2	10.7	10.0	15.8	7.2	17.5	17	0.8	29	7	3.1	13	4.5	2													



Monats- und

1944

As

$\varphi = 59^{\circ} 40' N$   $\lambda = 10^{\circ} 46' E$   $g =$   $\Delta G = + 1h$

Monat	Mittlerer Luftdruck P <sub>a</sub> Std. P <sub>0,000</sub>	Mittlere Lufttemperatur $T_m$				Lufttemperatur T						Windverteilung nD, F <sub>n</sub>																		
		8	14	19	Dies.	Max	Min	Max	Das	Min	Das	N	NE	E	SE	S	SW	W	NW	C										
I	- 2.4	- 0.6	- 2.3	- 2.2		- 6.4	7.9	30	- 19.1	11	7.5	1.4	4	1.5	103	1.3	69	2.0	153	2.2	83	1.8	139	2.0	8	1.5	19			
II	- 4.0	1.0	- 2.1	- 2.2		- 5.9	8.1	23	- 16.8	28	153	1.4	9	1.4	8	1.2	53	2.5	93	2.3	1	1.0	6	1.8	163	1.7	6			
III	- 3.2	3.2	0.1	- 0.8		- 5.2	8.8	18	- 13.1	5	153	2.6	33	1.1	4	1.8	89	1.6	193	1.5	13	1.0	39	2.0	16	2.0	21			
IV	2.5	7.6	5.2	5.4		- 1.1	15.6	27	- 7.5	2	6	1.9	33	1.7	5	1.2	7	1.9	263	1.8	73	1.9	123	2.2	11	1.5	11			
V	8.0	12.4	10.8	8.4		3.0	19.4	19	- 3.8	7	17	2.6	13	2.9	1	3.0	69	1.9	22	2.1	85	1.5	8	1.6	12	2.0	5			
VI	11.9	15.5	14.0	12.3		8.5	23.8	9	5.5	9	5	3.0	14	2.5	73	2.5	173	2.7	273	3.0	53	2.7	43	1.6	63	1.6	2			
VII	17.0	21.1	20.1	17.5		12.4	29.4	9	5.9	26	73	1.8	7	2.0	83	2.3	213	1.9	21	2.0	85	1.5	79	1.7	73	1.4	4			
VIII	16.2	20.8	18.4	16.9		12.3	26.2	1	4.9	15	2	2.5	2	1.5	33	1.0	123	2.2	353	2.9	9	2.4	10	2.4	103	1.9	8			
IX	9.7	13.8	11.1	10.4		6.9	18.3	19	0.2	29	8	1.6	8	1.1	12	1.5	16	2.1	10	2.2	6	1.8	8	1.8	5	1.3	17			
X	5.4	9.5	7.1	6.8		3.8	20.0	7	- 2.4	31	4	1.2	16	1.5	12	1.9	133	2.6	15	2.7	75	1.7	2	1.0	1	1.0	22			
XI	0.1	2.0	0.6	0.6		- 1.5	10.4	5	- 10.4	28	19	2.4	173	2.2	11	2.5	85	2.5	10	2.2	15	2.3	39	1.7	13	1.5	6			
XII	- 0.4	0.7	0.0	- 0.1		- 2.1	6.8	2	- 9.6	13	63	83	1.6	15	2.1	103	1.8	183	2.7	43	2.1	3	1.3	93	1.9	7				
1944						5.1	8.9	6.9	5.9		2.0	29.4	- 19.1	1133	2.1	106	2.0	98	1.8	144	2.1	2303	2.3	693	1.9	82	1.9	1163	1.7	136

Eidsberg

$\varphi = 59^{\circ} 30' N$   $\lambda = 11^{\circ} 17' E$   $g =$   $\Delta G = + 1h$

I	- 2.2	- 0.3	- 1.7	- 1.8		- 6.0	5.5	30	- 19.4	14	22	1.5	25	2.6	1	1.0	14	1.8	44	2.1	2	1.0	23	3.2	3	2.5	2			
II	- 3.5	0.5	- 1.8	- 2.0		- 5.3	7.0	24	- 12.4	6	403	1.9	143	2.3	1	2.5	9	1.9	20	2.4	0	-	0	-	2	3.0	0			
III	- 2.5	2.8	- 0.5	- 0.8		- 4.9	8.3	18	- 11.6	5	41	2.6	4	2.8	0	-	3	1.7	42	2.3	0	-	0	-	3	2.7	0			
IV	2.7	6.8	4.7	3.0		- 1.5	15.2	27	- 10.8	1	193	2.1	2	1.5	0	-	7	2.6	563	2.6	33	2.9	0	-	3	4.3	0			
V	7.8	12.4	9.4	7.8		2.4	19.5	13	- 4.9	7	313	2.7	8	2.4	0	2.0	3	2.3	42	2.4	3	2.3	19	2.0	33	2.9	0			
VI	12.2	15.1	13.3	11.8		7.5	23.7	19	3.4	24	125	2.6	49	2.4	0	-	10	2.3	539	2.4	43	2.7	1	2.0	4	2.2	0			
VII	16.6	20.3	19.4	16.9		11.8	29.7	9	5.4	26	18	2.2	73	2.0	0	2.0	143	2.0	47	2.2	5	2.6	09	2.0	39	1.9	0			
VIII	16.0	20.6	18.0	16.6		12.0	27.1	2	5.6	15	103	1.8	0	2.0	0	-	5	2.4	623	2.5	63	2.8	1	2.0	6	2.7	1			
IX	9.1	13.5	10.7	10.1		6.6	18.9	2	0.4	29	153	1.6	5	2.5	0	-	15	2.2	42	2.1	0	-	0	-	43	2.9	8			
X	5.7	9.4	6.7	6.8		4.0	20.0	7	- 1.7	2	193	1.7	2	2.2	0	3.0	253	2.3	40	2.2	0	-	0	-	43	1.8	1			
XI	0.7	1.8	0.7	0.8		- 1.5	13.5	5	- 10.4	28	37	2.5	7	3.6	0	3.0	22	2.2	23	2.9	05	1.0	0	-	0	-	0			
XII	0.0	0.8	0.1	0.2		- 1.6	6.7	2	- 9.3	13	21	2.1	0	-	0	-	385	2.4	323	2.4	1	2.5	0	-	0	-	0			
1944						5.2	8.6	6.6	5.8		2.0	29.7	- 19.4	2883	2.2	52	2.5	4	2.1	1663	2.2	505	2.4	26	2.5	63	2.5	373	2.5	12

Røde (Tomb)

$\varphi = 59^{\circ} 19' N$   $\lambda = 10^{\circ} 49' E$   $g =$   $\Delta G = + 1h$

I	- 1.4	0.9	- 0.5	- 0.6		- 5.2	6.8	28	- 19.7	11	35	1.6	123	2.0	11	2.4	65	1.8	8	3.6	34	3.4	9	2.6	53	1.4	3			
II	- 2.8	1.6	- 0.9	- 1.2		- 4.8	8.0	22	- 11.8	29	12	2.1	293	2.5	85	1.5	19	1.0	4	5.1	12	3.3	5	2.3	93	1.9	5			
III	- 1.7	3.6	1.2	0.2		- 3.7	8.2	19	- 9.5	6	163	3.5	22	2.0	23	1.8	33	2.8	13	2.7	7	2.6	9	2.2	73	3.2	12			
IV	3.6	7.3	4.9	3.6		- 0.7	14.7	27	- 9.5	1	10	3	2.6	13	0	-	103	2.1	24	3.6	10	3.6	73	2.9	11					
V	8.9	12.0	10.7	8.4		2.9	18.9	30	- 4.7	7	18	2.9	14	4.2	3	1.7	1	1.0	95	3.4	28	2.9	103	3.4	8	2.1	1			
VI	12.5	15.1	14.2	12.5		8.8	22.7	27	3.4	4	53	3.0	173	2.9	4	2.8	4	1.8	163	3.3	303	3.4	59	2.8	53	1.7	1			
VII	17.4	20.4	19.5	17.4		12.8	27.5	9	7.0	26	83	2.2	73	2.9	13	2.3	0	-	2	2.2	273	2.2	203	2.3	2	1.5	5			
VIII	17.2	20.4	18.6	17.2		13.0	25.8	1	4.9	15	1	1.0	33	1.6	5	2.0	2	2.8	213	2.5	363	2.9	7	1.9	63	2.4	10			
IX	10.2	13.9	11.9	10.9		7.3	17.9	19	- 0.1	29	53	2.8	13	2.2	8	2.5	15	4.7	133	3.0	15	2.6	83	2.9	5	2.5	20			
X	6.2	9.9	7.9	7.5		4.6	16.9	7	- 1.8	2	25	3.0	14	2.6	14	2.5	3	3.3	11	3.0	9	2.6	3	1.0	13	3.5	35			
XI	0.8	1.9	1.1	1.1		- 1.2	11.1	2	- 9.7	28	14	3.7	153	4.0	43	2.7	1	3.0	15	2.5	53	4.8	2	2.0	6	2.3	51			
XII	0.5	1.1	0.2	0.5		- 1.4	7.1	2	- 8.9	29	1	1.0	7	1.4	14	2.4	23	2.4	153	2.6	15	3.3	2	3.5	0	-	23			
1944						6.0	9.1	7.5	6.6		2.8	27.5	- 19.7	1033	2.9	1803	2.6	873	2.3	343	2.3	161	2.8	257	3.1	733	2.7	633	2.3	157

Brekke Sluse

$\varphi = 59^{\circ} 9' N$   $\lambda = 11^{\circ} 34' E$   $g =$   $\Delta G = + 1h$

I	- 2.4	0.1	- 2.0	- 1.7		- 6.2	6.1	6	- 21.0	11	4	1.0	14	1.1	6	1.2	8	1.1	2	1.0	0	-	9	1.0	18





</tbl\_r



1944

## Gvarv

 $\varphi = 59^\circ 24' N$   $\lambda = 9^\circ 10' E$   $g =$   $\Delta G = + 1^h$ 

Monat	Mittlerer Luftdruck $P_m$ hPa	Niedriger Luftdruck $P_d$ hPa	Mittlere Lufttemperatur $T_m$				Lufttemperatur $T$						Windverteilung $nD, F_n$															
			8	14	19	Dies	Max	Min	Max	Dec	Min	Dec	N	NE	E	SE	S	SW	W	NW	C							
I	-	- 4.4	- 1.9	- 4.5	- 4.1		- 9.2	7.8	6	- 18.7	11	25	1.0	2	1.5	6	2.8	0	-	5	1.7	1	2.5	4	1.2	73	2.7	55
II		- 5.9	1.2	- 2.5	- 3.2		- 8.2	7.0	2	- 23.0	28	25	2.2	0	-	1	1.0	0	1.0	8	1.7	13	2.0	5	1.6	133	2.2	55
III		- 3.7	4.5	0.9	- 0.6		- 6.1	9.6	18	- 14.9	5	2	3.5	23	1.4	1	3.0	1	1.5	11	1.5	0	1.0	13	1.7	233	2.6	50
IV		2.6	6.8	6.3	3.9		- 1.7	14.9	27	- 10.0	1	33	2.7	0	-	3	1.5	32	1.5	1	1.5	2	1.5	133	2.4	32		
V		8.3	14.7	12.0	8.9		1.7	21.8	29	- 4.8	7	7	2.4	63	2.1	39	1.9	0	-	223	1.4	23	1.0	13	1.7	263	2.2	25
VI		12.9	16.7	15.3	12.7		7.2	25.0	19	0.6	17	2	2.0	5	2.0	3	1.7	23	1.4	48	2.0	1	2.0	53	2.2	2	2.0	18
VII		17.0	21.9	19.7	17.2		11.1	29.2	8	6.2	26	0	-	4	1.8	2	1.5	59	2.0	423	1.6	2	1.2	0	-	0	-	37
VIII		15.5	22.1	18.4	16.4		9.5	27.5	5	2.2	30	0	-	0	-	1	1.0	2	1.2	42	1.8	0	-	53	2.5	29	3.8	40
IX		8.8	14.9	12.4	10.7		6.7	18.7	19	- 1.4	29	13	1.5	1	2.0	1	3.0	0	2.0	193	1.2	0	-	7	2.1	43	1.8	55
X		4.6	9.6	6.8	6.4		3.2	17.4	8	- 3.6	31	0	-	2	1.5	13	1.0	23	1.4	183	1.9	29	2.0	5	1.0	213	2.5	39
XI		- 0.9	1.6	- 0.6	- 0.4		- 3.5	10.2	5	- 17.6	28	7	2.6	33	2.1	9	2.4	0	-	11	1.5	0	-	2	2.0	43	2.8	33
XII		- 1.4	- 0.2	- 1.1	- 1.1		- 3.6	6.1	2	- 11.7	14	0	-	1	1.0	0	-	2	1.5	15	1.7	3	1.8	43	1.3	43	2.7	63
1944							0.6	29.2		- 23.0		28	2.3	303	1.9	32	2.1	173	1.6	273	1.7	15	1.7	433	1.8	1063	2.4	550

## Dalen i Telemark

 $\varphi = 59^\circ 27' N$   $\lambda = 8^\circ 0' E$   $g = 9.810$   $\Delta G = + 1^h$ 

Monat	Mittlerer Luftdruck $P_m$ hPa	Niedriger Luftdruck $P_d$ hPa	Mittlere Lufttemperatur $T_m$				Lufttemperatur $T$						Windverteilung $nD, F_n$																
			8	14	19	Dies	Max	Min	Max	Dec	Min	Dec	N	NE	E	SE	S	SW	W	NW	C								
I	-	- 2.5	- 1.1	- 1.4	- 1.9		- 5.0	8.4	30	- 12.7	11	0	-	0	-	3	1.5	2	1.8	0	-	0	-	233	2.0	233	2.1	41	
II		- 3.8	- 0.5	- 1.7	- 2.4		- 5.1	4.8	2	- 14.6	29	2	0	-	0	-	33	1.1	25	1.2	0	-	0	-	34	1.9	17	2.3	30
III		- 2.5	3.5	1.4	- 0.1		- 5.8	7.5	18	- 11.7	2	0	-	0	-	63	1.9	25	2.6	0	-	0	-	42	2.1	17	2.1	23	
IV		2.5	6.8	6.8	4.0		0.0	12.6	27	- 11.6	1	0	-	0	-	103	1.6	63	1.9	0	-	0	-	373	2.5	14	2.6	22	
V		7.3	12.6	12.5	8.8		4.0	20.0	29	- 0.6	7	0	-	0	-	8	1.8	8	1.8	0	-	0	-	493	2.8	103	2.3	17	
VI		11.4	15.6	14.9	12.2		7.8	25.0	19	4.0	4	12	0	-	0	-	13	1.7	9	1.7	0	-	0	-	303	2.3	103	2.0	27
VII		15.6	19.9	19.7	16.8		12.3	26.7	7	10.0	12	0	-	0	-	193	1.9	6	2.1	0	1.0	1	2.0	123	1.9	53	1.7	48	
VIII		14.8	20.2	19.3	16.7		12.5	25.4	5	6.4	30	0	-	0	-	323	1.8	33	1.7	0	-	0	-	183	2.5	93	1.9	29	
IX		9.1	12.9	11.7	10.4		7.6	18.2	9	- 2.4	29	2	2.0	0	-	15	1.4	1	2.0	0	-	0	-	24	1.6	17	1.9	31	
X		5.0	8.0	6.3	6.0		4.0	16.0	8	- 0.6	31	0	-	0	-	183	2.0	13	3.0	0	-	0	-	313	1.6	93	1.4	32	
XI		- 1.5	0.1	- 0.5	- 0.8		- 2.4	6.2	5	- 10.0	28	0	2.0	0	-	73	2.5	0	5.0	4	3.5	113	1.7	63	1.2	34			
XII		- 1.5	- 1.0	- 1.1	- 1.2		- 2.8	6.4	29	- 10.3	14	0	1.0	2	1.5	123	1.5	63	1.9	0	-	0	-	17	2.0	223	1.7	32	
1944							2.4	26.7		- 14.6		3	1.8	2	1.5	150	1.8	493	1.9	0	1	2.0	3463	2.1	1773	2.0	368		

## Vefall i Drangedal

 $\varphi = 59^\circ 0' N$   $\lambda = 9^\circ 13' E$   $g =$   $\Delta G = + 1^h$ 

Monat	Mittlerer Luftdruck $P_m$ hPa	Niedriger Luftdruck $P_d$ hPa	Mittlere Lufttemperatur $T_m$				Lufttemperatur $T$						Windverteilung $nD, F_n$															
			8	14	19	Dies	Max	Min	Max	Dec	Min	Dec	N	NE	E	SE	S	SW	W	NW	C							
I	-	- 1.7	0.7	- 1.0	- 1.1	3.1	- 6.3	9.8	30	- 19.8	11	3	1.7	2	2.5	0	-	3	1.5	73	1.7	63	1.8	7	2.5	27	2.2	37
II		- 4.9	1.5	- 2.0	- 2.5	2.7	- 7.3	8.8	7	- 25.1	29	8	2.2	15	1.0	13	1.0	0	33	1.5	25	1.2	13	4	21	2.1	35	
III		- 3.7	4.6	0.8	- 0.5	5.9	- 5.9	10.2	10.2	- 16.2	9	73	3.0	2	2.0	0	-	83	1.8	25	1.2	17	1.7	33	2.1	23		
IV		2.8	8.2	5.5	3.7	9.1	- 1.7	15.1	27	- 13.3	1	95	1.6	63	1.5	0	-	15	1.9	14	1.7	83	1.4	9	2.3	12		
V		9.4	13.6	11.7	9.2	15.0	2.9	22.5	12	- 5.2	7	23	2.1	63	1.9	43	2.3	143	2.1	153	1.8	3	1.7	5	2.6	17	2.0	4
VI		12.6	16.1	14.5	12.6	17.3	8.3	23	19	3.8	9	53	1.5	73	1.9	4	1.9	143	2.1	163	1.8	3	2.4	9	2.4	27	2.4	9
VII		17.2	20.7	19.4	17.1	22.3	11.7	28.1	9	6.7	26	143	1.2	43	1.4	23	2.2	193	2.0	25	1.7	8	2.2	1	1.0	15	16	
VIII		16.5	21.5	18.6	17.0	22.5	11.4	27.4	2	4.1	30	43	1.2	13	1.3	0	-	11	2.0	263	1.7	133	2.3	6	2.4	14	2.3	16
IX		10.6	14.4	11.9	11.2	15.2	7.7	20.2	17	0.8	29	16	1.5	4	1.9	23	2.0	13	2.2	14	1.8	10	1.6	10	2.2	10	2.2	10
X		5.5	10.3	7.5	7.1	11.0	3.4	20.4	20	7	3.2	31	16	1.8	113	3.2	1	23	1.4	133	2.4	75	1.6	89	1.2	16		
XI		0.1	2.7	0.9	0.9	3.5	- 1.9	11.1	5	- 13.2	28	23	2.															

## Jahresübersichten

194

$$H_0 = 26 \quad H_0 = \quad h_0 = 1.9 \quad h_0 = \quad h_0 = 15.8 \quad h_0 = 1.8$$

Gvary

$$B_1 = 77 \quad B_2 = 79.1 \quad B_3 = 2.9 \quad B_4 = - \quad B_5 = 3.9 \quad B_6 = 1.6$$

Dalen i Telemark

$$H_0 = 68 \quad H_b = \quad h_0 = 2.0 \quad h_0 = \quad h_4 = 12.3 \quad h_r = 1.6$$

Vefall i Drangedal

$$H_1 = 15 \quad H_2 = \quad h_t = 1.8 \quad h_s = \quad h_u = 22 \quad h_v = 1.7$$

Jomfruland

I	7.7	6.5	4.4	68	16	14	19		0	13	9	3	3	0	0	9	6	2	0	0	0	0	0	1	2	16	4	7	4			
II	6.7	6.2	5.8	13	4	17	25		0	13	7	3	0	0	0	3	6	2	0	0	0	0	0	1	2	15	4	6	12			
III	6.7	5.9	6.5	8	3	19	24		0	13	7	3	0	0	0	3	6	2	0	0	0	0	0	1	2	15	3	5	8			
IV	6.5	6.9	6.6	15	6	21	7		0	13	8	3	0	0	0	4	4	1	0	0	0	0	0	1	2	15	3	5	13			
V	5.3	6.5	6.9	17	8	16	1		0	13	9	5	0	2	0	8	1	0	0	0	0	0	0	1	2	21	6	12	12			
VI	7.2	6.5	6.9	98	34	5			0	13	11	3	4	1	0	13	0	0	1	0	0	0	0	1	2	21	3	13	12			
VII	6.5	5.8	4.6	90	33	26	0		0	12	5	3	2	1	0	12	5	0	0	0	0	0	0	1	2	26	7	7	7			
VIII	5.5	5.7	5.6	42	17	29	0		0	12	5	3	2	1	0	12	5	0	0	0	0	0	0	1	2	23	8	7	7			
IX	7.5	7.1	6.2	155	30	1	0		0	15	13	6	5	0	0	15	18	0	0	0	0	0	0	1	2	17	1	11	11			
X	7.5	7.2	7.3	125	22	17	11		0	18	16	6	5	0	0	18	0	0	0	0	0	0	0	1	2	12	3	18	18			
XI	7.6	7.1	6.3	114	20	20	11		0	22	19	3	10	1	0	20	5	3	3	1	2	0	0	0	0	2	3	8	3	16	17	
XII	7.4	7.5	7.7	115	24	9	16		0	21	15	4	4	0	0	15	15	6	1	2	0	0	0	0	0	2	4	5	3	3	17	
1944					6.8	6.6	6.2	860	34		101	0	150	115	30	42	2	0	129	29	9	10	0	1	0	7	10	22	199	90	141	19

$$H_0 = 2 \quad H_0 = \quad h_0 = 2.0 \quad h_0 = \quad h_0 = \quad h_0 = 1.3$$

**Lyngør**

I	82	75	77	78	7.4	3.9	4.6	73	28	26	13	0	0	13	10	2	0	0	0	11	5	3	4	0	0	0	1	0	20	3	10	
V	82	75	77	78	6.7	6.3	5.5	9	4	28	3	21	0	0	7	4	2	0	0	7	4	2	1	0	0	0	3	1	21	5	9	
V	82	75	77	78	6.6	6.2	5.1	12	3	21	2	6	0	0	8	3	9	5	0	0	5	2	0	0	0	3	3	3	25	5	11	
V	82	75	77	78	6.3	6.2	6.5	12	0	21	0	0	0	0	10	6	0	0	0	10	0	0	0	0	0	0	3	0	26	4	9	
V	82	75	77	78	6.9	5.9	5.8	17	4	16	0	0	0	0	15	11	2	0	0	14	6	0	0	0	0	0	4	4	26	4	12	
V	82	75	77	78	7.3	6.6	6.3	91	30	25	0	0	0	0	12	5	1	4	0	16	0	0	0	0	0	0	5	5	26	6	10	
V	82	75	77	78	6.5	5.5	4.3	62	28	28	0	0	0	0	6	5	1	2	0	12	6	0	0	0	0	0	1	1	22	2	11	
V	82	75	77	78	6.2	5.0	5.9	37	18	21	0	0	0	0	16	11	6	5	0	16	6	0	0	0	0	0	0	0	0	14	2	17
V	82	75	77	78	7.6	6.8	6.2	153	33	24	0	0	0	0	16	14	5	8	0	23	19	5	2	0	0	0	1	1	14	5	16	
V	82	75	77	78	7.8	7.4	7.2	144	30	27	0	0	0	0	16	18	5	7	0	23	19	5	4	0	0	0	0	0	0	14	4	17
V	82	75	77	78	6.8	6.8	7.3	122	22	20	9	15	0	0	22	15	2	7	0	0	2	2	0	0	0	0	0	0	0	22	5	16
1944	79	70	75	77	7.0	6.4	6.0	825	33	29	85	0	0	156	109	22	65	0	0	142	26	11	35	0	5	0	13	26	262	45	138	



## Jahresübersichten

1944

 $H_e = 12$   $H_b =$   $H_c = 2.0$   $H_d =$   $H_r = 1.4$ 

Torungen Fyr

Monat	Mittlere Relative Feuchte U. <sub>m</sub>		Mittlere Bewölkung N. <sub>m</sub>		Niederschlag R		Lufttemperatur T			Niederschl. R			Windstärke F			Zahl der Tage n																								
	8	14	19	Dauer	8	14	19	Σ	Max	Dec	5	10	15	20	25	30	●	*	§	9	*	△	▲	R	=	≡	○	◎	○	■										
	8	14	19	Dauer	8	14	19	Σ	Max	Dec	5	10	15	20	25	30	●	*	§	9	*	△	▲	R	=	≡	○	◎	○	■										
I					6.5	4.8	4.5	74	21	26	13	22	3	21	22	0	15	11	2	8	1	1	14	6	5	0	0	0	12	1	24	6	7							
II					6.3	5.9	5.4	7	3	17	4	21	0	0	0	0	8	3	0	0	0	0	0	0	0	0	0	0	0	0	0	22	5	8						
III					5.5	5.4	4.6	21	5	31	4	21	0	0	0	0	7	6	3	1	5	1	0	5	5	6	0	0	0	0	0	7	27	5	3					
IV					5.7	4.9	4.9	16	11	21	4	0	0	0	0	6	3	1	5	1	0	0	0	0	0	0	0	0	0	0	0	26	5	3						
V					5.7	4.9	4.5	7	3	2	0	0	0	0	0	0	8	2	0	9	1	0	0	8	1	1	4	0	0	0	0	0	29	4	5					
VI					5.4	5.4	5.6	86	37	5	0	0	0	0	0	0	11	11	2	2	2	0	0	11	0	0	0	0	0	0	0	0	2	5						
VII					5.9	4.5	3.5	69	28	28	0	0	0	0	0	0	10	7	2	2	2	0	0	10	0	0	0	0	0	0	0	0	30	10	4					
VIII					5.1	4.0	4.3	35	17	21	0	0	0	0	0	0	6	4	1	4	0	0	0	14	0	0	0	0	0	0	0	0	22	7	4					
IX					6.8	4.9	5.1	139	24	24	0	0	0	0	0	0	14	13	4	6	0	0	0	15	0	0	0	0	0	0	0	0	18	5	9					
X					6.8	6.9	7.1	106	25	29	0	0	0	0	0	0	15	15	4	11	3	1	0	15	0	0	0	0	0	0	0	0	15	3	13					
XI					6.8	6.4	6.7	185	25	20	7	10	0	0	0	0	23	20	9	14	7	4	0	17	9	6	2	0	0	0	0	0	10	4	19					
XII					7.6	7.6	7.1	127	21	2	10	0	0	0	0	0	143	110	32	85	14	6	1	131	38	24	20	0	0	8	0	0	15	92	18	282	63	103		
1944					6.2	5.5	5.3	872	37	77	0	0	0	0	0	0																								

 $H_e = 7$   $H_b =$   $H_c = 1.8$   $H_d =$   $H_r = 1.4$ 

Grimstad

Monat	Mittlere Relative Feuchte U. <sub>m</sub>		Mittlere Bewölkung N. <sub>m</sub>		Niederschlag R		Lufttemperatur T			Niederschl. R			Windstärke F			Zahl der Tage n																				
	8	14	19	Dauer	8	14	19	Σ	Max	Dec	5	10	15	20	25	30	●	*	§	9	*	△	▲	R	=	≡	○	◎	○	■						
	8	14	19	Dauer	8	14	19	Σ	Max	Dec	5	10	15	20	25	30	●	*	§	9	*	△	▲	R	=	≡	○	◎	○	■						
I					6.2	5.3	3.8	117	29	14	18	0	0	0	0	0	18	13	3	2	0	0	0	16	6	4	0	0	0	0	0	18	7	6		
II					7.0	6.3	4.9	10	2	17	23	0	0	0	0	0	13	5	0	9	1	0	0	16	8	1	0	0	0	0	0	20	2	6		
III					6.1	5.4	4.8	28	9	31	22	0	0	0	0	0	11	7	0	9	0	0	0	16	8	0	1	0	0	0	0	24	4	3		
IV					6.2	5.9	6.1	26	15	21	8	0	0	0	0	0	9	5	1	0	0	0	0	9	0	2	0	0	0	0	0	0	0	31	5	
V					5.9	5.9	4.5	10	4	2	1	0	0	0	0	0	10	3	0	11	0	0	0	10	0	0	0	0	0	0	0	0	29	4	6	
VI					6.2	6.5	6.0	117	43	5	0	0	0	0	0	0	17	14	2	6	0	0	0	17	0	0	0	0	0	0	0	0	25	3	0	
VII					6.0	5.1	3.7	78	26	28	0	0	0	0	0	0	16	8	2	4	0	0	0	16	0	0	0	0	0	0	0	0	29	7	0	
VIII					5.5	4.5	5.0	50	24	21	0	0	0	0	0	0	21	14	9	9	0	0	0	21	0	0	0	0	0	0	0	0	27	0	0	
IX					6.8	6.7	5.5	161	30	6	0	0	0	0	0	0	21	16	9	9	0	0	0	21	0	0	0	0	0	0	0	0	23	1	0	
X					7.1	7.5	6.7	130	22	18	11	0	0	0	0	0	18	13	2	1	0	0	0	18	0	0	0	0	0	0	0	0	23	4	0	
XI					6.4	6.0	6.5	218	33	20	11	0	0	0	0	0	23	21	9	5	1	0	0	24	7	6	0	0	0	0	0	0	23	4	0	
XII					7.8	7.8	7.1	165	25	18	15	0	0	0	0	0	23	18	5	11	1	0	0	22	10	7	3	0	0	0	0	0	21	1	2	
1944					6.4	6.1	5.4	1110	43	8	98	0	0	0	0	0	187	128	38	110	9	0	0	168	40	18	10	0	0	0	0	0	12	263	33	119

 $H_e = 207$   $H_b =$   $H_c = 1.9$   $H_d =$   $H_r = 1.4$ 

Byglandsfjord

Monat	Mittlere Relative Feuchte U. <sub>m</sub>		Mittlere Bewölkung N. <sub>m</sub>		Niederschlag R		Lufttemperatur T			Niederschl. R			Windstärke F			Zahl der Tage n																				
	8	14	19	Dauer	8	14	19	Σ	Max	Dec	5	10	15	20	25	30	●	*	§	9	*	△	▲	R	=	≡	○	◎	○	■						
	8	14	19	Dauer	8	14	19	Σ	Max	Dec	5	10	15	20	25	30	●	*	§	9	*	△	▲	R	=	≡	○	◎	○	■						
I	87	81	81	83	7.5	6.1	4.9	142	19	28	26	3	1	0	0	0	24	17	5	2	0	0	0	0	15	7	1	0	0	0	0	0	0	18	2	8
II	76	65	72	72	6.9	5.9	5.9	20	5	8	29	0	0	0	0	0	11	6	0	2	0	0	0	0	0	0	0	29	1	9						
III	50	58	65	70	6.5	6.4	5.8	34	9	30	26	0	0	0	0	0	11	7	0	2	0	0	0	0	0	0	24	2	6							
IV	80	58	63	72	6.8	6.8	6.2	21	8	21	17	0	0	0	0	0	1																			

Monats- und

1944

Mandal

$\varphi = 58^\circ 2' \text{N}$

$\lambda = 7^\circ 27' \text{E}$

$\delta =$

$\Delta G = + 1^h$

Monat	Mittlerer Luftdruck $P_a$	Abstand $P_a - P_s$	$P_s$	Mittlere Lufttemperatur $T_m$				Lufttemperatur $T$								Windverteilung $nD.F_m$															
				8	14	19	Dien.	Max	Min	Max	Dat	Min	Dat	N	NE	E	SE	S	SW	W	NW	C									
I				2.4	3.9	2.8	2.8	-0.1	8.4	2	-9.2	10	0	-	25	1.4	63	2.7	3	1.0	6	1.5	345	3.1	15	2.4	25				
				0.0	3.2	0.7	0.9	-2.3	9.4	22	-9.0	29	45	1.8	219	2.5	153	2.4	2	3.2	5	2.6	63	2.9	7	2.9	15				
				0.0	4.6	2.0	1.7	-1.9	8.9	18	-8.1	5	24	4.6	6	2.6	5	1.3	2	3.0	5	1.8	14	3.1	13	2.7	18				
				4.9	8.3	5.9	5.5	2.1	14.0	25	-8.2	1	05	1.0	113	2.6	19	3.6	2	2.0	7	2.1	4	1.5	245	2.1	99	2.6	12		
				9.1	12.7	10.4	9.4	5.3	22.6	30	-1.1	7	4	2.5	8	2.4	11	2.6	15	1.0	135	1.7	16	1.7	265	1.6	98	2.7	3		
				12.7	15.1	13.0	12.5	9.3	25.3	20	-4.1	4	05	2.0	95	2.3	15	2.0	45	1.8	23	2.2	125	1.8	15	2.0	27				
				17.3	19.5	17.7	16.9	12.9	25.4	9	-8.1	26	0	-	16	2.5	135	2.0	3	2.3	65	1.9	185	1.6	18	1.9	35				
				16.5	19.9	17.6	16.9	12.7	24.4	4	7.0	30	0	-	9	1.7	12	2.0	05	1.0	65	1.3	175	1.7	25	1.8	35				
				11.3	14.6	12.1	12.0	8.8	17.9	19	-4.9	25	0	-	11	1.5	215	2.2	25	2.4	1	1.0	3	2.0	185	2.4	35	2.5	29		
				7.6	10.7	9.0	8.7	5.8	16.9	7	-0.9	31	0	-	17	1.9	22	2.5	9	2.1	6	3.0	85	1.1	13	1.0	21				
				2.5	4.3	3.3	3.1	0.1	8.5	5	-4.4	28	05	4.0	275	3.0	12	2.8	2	2.5	5	3.0	3	2.7	75	1.7	13	1.0	35		
				2.5	3.2	2.2	2.5	0.3	7.3	1	-5.5	13	05	3.0	95	1.6	205	2.1	25	1.6	13	1.0	65	1.8	7	1.9	20				
1944					7.2	10.0	8.0	7.7		4.4	25.4	-	9.2		13	3.3	149	2.3	1755	2.4	335	2.0	75	2.1	1155	2.1	202	2.2	75	2.4	254

Gläben

$\varphi = 58^\circ 22' \text{N}$

$\lambda = 7^\circ 27' \text{E}$

$\delta =$

$\Delta G = + 1^h$

I	II	III	IV	5.0				7.0				10.0				13.0				16.0				19.0								
				3.0	4.0	5.0	6.0	3.0	4.0	5.0	6.0	3.0	4.0	5.0	6.0	3.0	4.0	5.0	6.0	3.0	4.0	5.0	6.0	3.0	4.0	5.0	6.0					
V				7.0	10.9	8.9	7.4	2.6	20.4	29	-2.2	8	145	2.6	115	3.4	8	2.6	29	2.4	8	2.1	19	2.4	125	2.2	15	3.2	2			
				10.5	13.0	11.9	10.3	6.1	23.2	20	-0.2	4	4	1.0	125	2.6	135	2.0	22	2.0	185	1.8	235	2.6	10	2.1	1					
				15.5	18.0	16.5	15.1	10.2	24.3	9	6.7	25	3	1.2	12	2.7	17	2.1	7	1.9	155	1.7	215	2.2	115	2.5	55	2.7	0			
				14.7	18.4	16.5	14.9	9.9	24.8	3	4.9	30	05	1.0	85	1.8	135	1.9	45	1.2	25	2.2	195	3.0	95	3.0	8	3.6	2			
				9.1	11.6	9.5	9.4	6.2	16.3	18	-1.7	29	5	1.6	135	2.5	19	2.8	35	3.3	75	2.5	95	2.1	225	3.0	75	2.6	2			
				5.2	8.1	5.9	6.0	3.1	18.9	7	-3.1	31	6	1.5	195	3.0	195	2.7	10	2.3	12	2.6	65	2.3	45	2.2	2	2	1			
				0.1	1.9	0.2	0.4	-2.5	5.8	3	-9.0	27	95	2.2	235	3.8	145	3.5	25	2.0	85	2.0	115	2.9	10	1.5	55	1.9	9	1.9	9	
				-0.5	0.3	-1.1	-0.5	-2.9	4.9	1	-10.2	14	45	1.9	15	3.1	22	2.9	7	2.3	9	2.6	75	3.5	15	3.2	6	2.8	9			
				5.0	7.7	5.8	5.3	1.6	24.8	-	13.7	855	2.1	161	2.8	1645	2.6	52	2.1	1175	2.1	185	2.5	1795	2.6	132	2.6	25				
1944					7.4	8.8	8.0	7.7	9.8	5.6	24.6	-	7.9	315	2.4	1295	3.0	137	3.7	1255	3.8	125	3.7	32	4.5	81	4.6	3605	4.8	76		

Lister

$\varphi = 58^\circ 6' \text{N}$

$\lambda = 6^\circ 34' \text{E}$

$\delta =$

$\Delta G = + 1^h$

I	II	III	IV	3.8				5.0				6.2				7.4				8.6				9.8						
				0.6	2.5	1.4	1.2	3.4	5.3	0.6	-1.1	7.1	2.2	15	-7.9	29	3.4	20	165	2.4	17	2.2	7	2.6	8	4.4	225	4.3	7	
V				7.8	11.8	10.0	8.5	3.4	20.2	29	-3.5	7	32	5.1	5	2.3	0	-	0	-	17	1.6	0	-	9	1.9	10	2.4	22	
				11.5	14.8	13.2	11.5	7.0	23.0	20	-0.4	4	15	3.3	2	1.5	0	-	0	-	36	2.1	0	-	16	2.8	5	3.0	16	
				16.0	20.0	18.3	16.5	11.3	27.0	5	6.8	25	11	2.6	0	-	1	3.0	2	2.5	41	2.4	0	-	7	2.7	2	1.9	31	
				14.8	19.9	17.6	15.8	10.6	27.8	24	3.1	30	16	1.8	1	2.0	0	-	0	-	30	2.4	0	-	14	2.4	1	4.0	31	
				10.3	14.0	11.2	10.8	7.2	18.2	19	-3.2	28	11	2.0	0	-	5	2.4	0	-	12	2.3	0	-	6	3.4	3	3.3	51	
				6.3	10.6	8.0	7.7	4.3	19.8	7	-2.6	31	12	2.8	7	4.3	1	2.0	1	4.0	9	3.7	4	4.6	2	6.0	0	5.0	0	52
				1.4	3.9	1.4	1.8	-1.4	8.4	5	-7.1	28	14	2.9	8	4.5	8	4.9	0	-	4	4.6	2	6.0	2	5.0	0	1.9	0	52
				0.9	1.4	1																								

Jahresübersichten

1944

$H_s = 6$     $H_b =$     $h_c = 2.0$     $h_o =$     $h_d = 4.4$     $h_r = 1.4$

Mandal

Monat	Mittlere Relative Feuchte $U_m$		Mittlere Bewölkung $N_m$		Niederschlag $R$		Zahl der Tage n																													
							Lufttemperatur T	Niederschl. R	Windstärke F	Regen	Schne	Regen + Schne	Nebel	Kalt. grauig.	Früh. grauig.	Hagel	Gefahr	Dunst	Nebl.	Sonne	Heiter	Wolken	Schne decke													
	8	14	19	Dien.	8	14	19	$\Sigma$	Max	Drei	b	v	b	v	b	v	b	v	b	v	b	v	b	v	b	v	b	v	b	v	b	v	b	v		
I	7.3	5.6	4.3		166	24	9	13			25	22	5	3	5	0	0	20	5	2	6	0	2	0	0	0	18	6	14	3	9					
II	6.2	6.1	4.9		41	18	7	24			9	6	0	0	4	0	0	6	3	0	4	0	0	0	0	0	28	1	17	6	9					
III	5.0	4.9	4.1		35	9	19	24			10	6	0	0	4	0	0	6	2	0	4	0	0	0	0	0	27	4	21	4	8					
IV	6.2	5.4	5.4		11	6	24	24			12	11	2	0	2	0	0	10	0	0	0	0	0	0	0	0	27	2	23	4	8					
V	6.3	4.5	4.5		56	18	2	2			10	8	3	0	0	0	0	10	0	0	0	0	0	0	0	0	29	2	22	6	7					
VI	6.6	6.3	6.4		150	93	34	28			12	10	2	0	0	0	0	12	0	0	0	0	0	0	0	0	27	3	23	5	6					
VII	5.3	5.4	4.4		75	24	28	0			12	9	2	0	0	0	0	12	0	0	0	0	0	0	0	0	25	1	26	9	7					
VIII	5.0	5.0	4.6		47	10	21	0			18	15	9	0	0	0	0	18	0	0	0	0	0	0	0	0	22	0	4	17	3					
IX	6.6	5.8	4.8		240	36	6	0			21	19	10	3	0	0	0	21	2	0	1	0	0	0	0	0	24	3	14	8	11					
X	6.2	6.6	5.8		164	45	29	1			22	20	9	0	0	0	0	19	8	0	10	0	0	0	0	0	26	3	13	3	19					
XI	5.4	6.0	5.4		198	25	29	5			172	149	49	17	0	0	0	160	24	4	41	0	9	0	11	306	34	240	64	117						
1944	6.2	5.7	5.2		1398	93	98	0																												

$H_s = 264$     $H_b =$     $h_c = 1.8$     $h_o =$     $h_d = 6.0$     $h_r = 1.8$

Gläben

I	83	80	83	83	7.9	7.3	5.4	175	22	14	20	3	2	25	10	9	7	9	2	0	17	17	5	6	0	0	0	0	1	10	2	14			
II	79	66	74	74	6.6	7.0	5.7	33	7	8	25	0	0	3	15	8	0	2	4	0	0	15	8	1	0	0	0	0	2	17	5	12			
III	78	62	70	74	6.3	5.8	5.9	15	1	1	28	2	0	0	15	8	1	2	4	0	0	15	8	2	0	0	0	0	2	23	4	14			
IV	80	62	70	74	7.1	7.1	6.6	29	11	21	14	2	0	0	16	9	3	1	4	0	0	16	9	2	0	0	0	0	2	23	3	12			
V	72	55	60	60	7.4	6.6	6.1	26	8	3	25	5	0	0	16	9	6	0	4	0	0	16	9	1	0	0	0	0	0	27	1	9			
VI	76	68	73	76	7.6	7.9	7.3	143	39	5	28	0	0	0	18	10	9	3	4	0	0	18	10	2	0	0	0	0	0	27	1	15			
VII	77	67	73	76	5.3	7.1	5.3	134	54	26	29	0	0	0	16	8	9	1	4	0	0	16	8	1	0	0	0	0	0	23	3	7			
VIII	82	65	76	78	5.8	6.5	6.5	48	21	29	0	0	0	0	21	18	8	5	5	0	0	21	18	1	0	0	0	0	0	24	2	9			
IX	86	73	84	84	7.5	8.1	7.0	191	29	24	0	0	0	0	21	19	9	5	5	0	0	21	19	3	0	0	0	0	0	20	1	13			
X	90	79	85	85	8.1	7.6	7.4	229	48	15	23	0	0	0	21	18	9	5	5	0	0	21	18	3	0	0	0	0	0	18	0	19			
XI	93	84	84	84	8.1	6.8	6.6	207	35	29	23	0	0	0	21	18	8	7	7	0	0	21	18	3	0	0	0	0	0	16	4	13			
XII	90	86	88	88	8.4	8.8	8.8	230	39	2	25	0	0	0	26	25	7	7	7	0	0	26	25	4	0	0	0	0	0	11	6	23			
1944	82	70	77	79	7.0	7.3	6.5	1504	58	143	0	0	0	0	213	167	50	64	5	3	169	77	17	45	5	0	1	19	23	68	234	27	158		

$H_s = 13$     $H_b =$     $h_c = 2.1$     $h_o = 6.2$     $h_d = 5.7$     $h_r = 1.6$

Liste

I	90	87	88	89	8.5	7.8	7.6	192	36	14	10	0	0	0	27	22	7	21	13	8	24	10	7	4	0	0	0	0	11	2	18	0	15			
II	79	72	78	78	6.5	6.9	6.1	29	9	7	17	3	0	0	0	12	6	0	7	3	2	0	6	2	1	0	0	0	0	13	0	11	3	9		
III	84	77	80	81	6.2	6.4	6.6	50	14	3	14	0	0	0	0	18	8	1	12	2	0	14	1	1	0	0	0	0	2	26	2	11	10	10		
IV	84	76	82	82	6.7	5.8	6.2	39	14	3	5	0	0	0	0	14	9	2	14	1	0	14	1	1	0	0	0	0	2	24	2	12	1	12		
V	82	78	82	82	6.7	5.8	6.4	134	56	5	28	0	0	0	0	14	11	3	11	1	0	14	1	1	0	0	0	0	2	24	2	14	0	0		
VI	86	86	88	88	6.9	7.2	7.4	77	19	28	0	0	0	0	14	11	3	7	1	0	14	1	1	0	0	0	0	0	2	24	2	14	0	0		
VII	86	86	88	88	6.3	6.7	6.5	77	19	28	0	0	0	0	16	15	2	12	5	0	16	15	0	0	0	0	0	0	2	24	2	12	0	0		
VIII	88	88	88	88	7.1	7.4	7.1	103	40	29	0	0	0	0	15	11	3	7	1	0	14	1	1	0	0	0	0	0	2	24	2	12	0	0		
IX	86	76	82	82	7.2	7.0	7.0	221	26	24	0	0	0	0	19	17	10	19	4	0	19	2	0	0	0	0	0	0	2	24	1	10	0	0		
X	88	83	87	87	8.0	7.4	7.7	131	19	18	0	0	0	0	21	16	4	17	2	0	21	0	0	0	0	0	0	0	2	24	1	10	0	0		
XI	88	77	76	79	6.3	6.4	6.7	136	18	20	6	0	0	0	0	18	15																			

Monats- und

1944

Stavanger

Monat	Mitterer Luftdruck P <sub>0</sub>	Fest. Luftdruck Hausdruck P <sub>0</sub>	Mittlere Lufttemperatur T <sub>m</sub>				Lufttemperatur T				Windverteilung nD.F <sub>m</sub>																		
			8	14	19	Dies	Max	Min	Max	Dat	Min	Dat	N	NE	E	SE	S	SW	W	NW	C								
			3.2	3.8	3.5	3.4	5.1	1.4	7.8	15	-3.7	10	3	3.2	2	2.8	2	1.5	11.5	4.4	16	3.7	15.5	4.6	16.5	4.8	11		
I	0.7	1.7	1.3	1.0	4.0	-0.8	7.7	1	-4.6	28	10.5	2.6	5.9	1.5	5.5	1.5	12.5	3.6	12	4.1	10	3.2	4	4.1	16	4.2	11		
II	1.9	3.3	2.4	2.2	4.8	0.2	8.6	26	-3.0	2	20	3.2	8.5	1.2	3	1.2	3	2.0	7.5	3.3	7.5	3.3	9	3.7	21.5	3.8	13		
III	5.2	7.4	6.0	5.6	8.7	3.3	13.9	14	-2.6	1	5	3.9	1.0	1.3	2.3	17	14	4.6	8.5	3.0	17	3.5	14.5	4.2	10				
IV	8.0	10.3	9.2	8.4	12.2	5.7	19.8	19	1.8	22	11	4.0	6.5	2.6	1.9	2.3	4	3.0	9.5	2.7	12	3.0	8.5	2.2	30	4.2	10		
V	11.2	13.2	12.0	11.2	14.7	8.6	18.6	27	4.7	4	8.5	3.1	1	1.0	1	3.0	6.5	3.1	9.5	4.3	15	3.5	10	2.2	29.5	3.9	9		
VI	14.9	17.6	16.1	15.4	18.7	12.9	26.8	5	8.8	25	6	5.8	4	1.1	3	2.8	6	4.0	7	2.7	8.5	2.6	13	2.0	30.5	3.2	15		
VII	14.9	17.5	15.8	15.4	18.4	12.8	28.7	24	9.1	30	4	2.2	0	-	3	1.3	4	1.5	19	3.2	11.5	3.7	18	3.0	22.5	2.7	11		
IX	11.0	13.0	11.7	11.5	14.4	9.6	18.0	21	5.8	28	5	3.4	3	1.0	6	2.2	8	4.8	8	4.7	5.5	2.3	11.5	3.5	27	4.0	16		
X	8.8	10.1	8.9	9.1	11.0	7.3	13.8	13	4.8	31	5.5	2.7	7.5	1.3	3	2.2	12.5	4.1	19.5	4.2	12	2.7	25	2.2	9.5	2.0	21		
XI	4.0	5.2	4.6	4.4	6.7	2.5	10.9	5	-0.1	27	8	3.1	5.5	1.5	1.7	1.5	17.5	3.5	17.5	4.4	9.5	4.1	8	4.1	5.5	3.3	6.5	2.8	12
XII	3.2	3.4	3.4	3.2	5.0	1.6	8.4	2	-1.7	31	5.5	4.0	6	1.8	6.5	3.1	26	3.3	24	3.9	7.5	4.3	5	4.6	4.5	3.8	8		
1944											90	3.2	52	1.5	55	2.5	130.5	3.6	155.5	3.8	121.5	3.4	119.5	3.2	228.5	3.7	147		

Sauda

Monat	Mitterer Luftdruck P <sub>0</sub>	Fest. Luftdruck Hausdruck P <sub>0</sub>	Mittlere Lufttemperatur T <sub>m</sub>				Lufttemperatur T				Windverteilung nD.F <sub>m</sub>																		
			0.0	0.8	0.7	0.5	3.4	-2.4	9.9	15	-13.1	12	0	-	5	3.0	4	1.5	2	1.5	1	1.0	4	3.5	11	3.4	2	1.5	64
			-3.1	1.4	-0.6	-1.2	2.6	-4.9	8.2	2	-12.0	28	4	1.2	1	2.0	15	1.7	2	1.5	0	-	3	2.3	6	3.0	2	1.3	56
I	-2.7	2.8	1.0	-0.2	4.0	-4.0	8.0	26	-11.2	5	7	2.0	1	2.0	1	2.1	1.6	0	-	0	-	16	1.8	3	2.5	4	1.5	41	
II	3.1	8.2	6.6	4.9	9.7	0.7	14.9	16	-8.9	1	14.5	1.9	1	1.0	9	1.8	0	-	1	1.0	25	2.2	1	2.0	23	1.2	38		
III	6.9	11.3	10.6	8.2	13.0	3.9	20.4	19	-2.4	7	5	1.6	5	2.8	11	2.0	0	-	2	2.0	21	1.9	7	2.3	6	2.2	36		
IV	10.6	14.8	14.7	11.8	16.8	7.5	23.2	19	2.6	4	7	2.1	1	2.0	1	2.0	1.8	0	-	2	2.0	27	1.9	11	2.5	4	2.2	32	
V	14.5	19.4	18.6	16.0	21.4	11.9	28.0	5	7.2	25	1	2.0	1	3.0	3	1.3	0	-	0	-	47	2.1	2	1.5	0	-	39		
VI	14.2	18.4	17.9	15.6	20.3	11.7	28.8	24	4.6	30	0	-	0	-	3	2.0	0	-	0	2.0	27.5	2.2	6	2.7	1	1.0	55		
VII	8.9	13.0	11.8	10.6	14.4	7.8	19.5	22	3.5	12	5	2.0	0	-	6	1.2	1	4.0	0	3.0	19.5	1.9	5	2.8	1	3.0	52		
IX	6.7	9.3	7.6	7.5	10.8	4.7	15.4	13	-0.2	21	2	1.5	18	2.9	2	2.0	0	3	0.5	19.5	3.0	3	2.7	0	-	58			
X	1.3	3.6	1.3	1.8	4.9	-1.0	11.1	5	-6.5	27	3	3.3	3	3.0	21	2.2	1	1.0	0	-	4	2.2	5	3.4	2	2.0	51		
XI	1.4	1.5	0.8	1.1	3.8	-1.3	7.6	2	-8.1	14	1	2.0	3	2.7	18	1.9	1	2.0	0	3.0	6.5	2.9	0	-	1	4.0	62		
1944											49.5	1.9	21	2.7	13.5	2.0	9	1.9	8	2.0	206	2.1	60	2.8	25.5	1.9	584		

Skudenes H.

Monat	Mitterer Luftdruck P <sub>0</sub>	Fest. Luftdruck Hausdruck P <sub>0</sub>	Mittlere Lufttemperatur T <sub>m</sub>				Lufttemperatur T				Windverteilung nD.F <sub>m</sub>																			
			1004.8	1005.9	4.2	4.5	4.1	4.2	-1.9	8.3	15	-4.1	10	6.5	4.5	7	2.6	25	4.2	8.5	5.6	13.5	4.8	11.5	3.1	20.5	5.4	3		
			14.2	15.4	1.1	3.2	2.0	1.9	-0.4	7.5	7	-5.7	28	16.5	4.7	22	3.4	1.5	3.7	14.5	5.3	9	3.9	11	4.7	13.5	5.6	4		
I	10.6	11.8	2.0	4.2	5.6	2.6	5.6	5.6	0.5	7.9	26	-5.6	31	28.5	4.5	9.5	2.9	5	2.2	19	5.0	6	4.0	9.4	11	4.6	18.5	5.1	4	
II	14.0	15.2	5.2	7.4	5.6	5.6	5.6	5.6	3.4	10.5	9	-3.4	1	12.5	5.9	11	3.4	11	4.5	18.5	5.2	9.5	4.1	17	4.1	10.5	5.0	0		
III	15.1	16.3	8.2	9.6	8.6	8.1	8.6	8.6	5.7	17.7	18	1.6	8	21	6.0	4	3.3	45	3.9	3.6	21.5	3.9	8.5	4.5	11	3.7	19	5.6	0	
IV	0.7	0.7	11.0	12.6	11.4	10.9	10.9	10.9	8.8	16.6	27	4.4	4	27	4.9	0	-	5	3.2	6	4.2	20.5	4.3	8.5	3.8	4	3.0	19	4.4	0
V	10.8	11.9	15.6	16.6	15.5	15.0	15.0	15.0	12.7	24.0	5	12.7	24	8.5	4.5	4	3.0	10.5	3.1	6.5	2.4	11.5	2.4	24.5	4.1	1	1.3	1.5	0	
VI	12.8	14.0	14.8	16.5	15.2	14.8	14.8	14.8	12.5	21.1	24	7.5	30	20.5	3.5	1	3.0	2	3.5	5.5	3.0	19.5	3.5	16	5.2	6	22.5	3.5	0	
VII	10.1	11.2	11.9	13.6	12.3	12.2	12.2	12.2	10.1	17.0	22	7.3	30	13	4.0	6	2.7	4	4.3	12	4.5	15	3.1	12.5	2.8	4	6.3	21.5	2	
IX	0.9	1.0	9.3	10.6	9.3	9.5	9.5	9.5	7.9	15.1	4	4.0	31	8	2.6	0	-	3.5	2.5	25	5.0	14.5	5.0	12.5	4.9	2	2.0	7	3.4	0
X	0.1	0.1	0.2	0.4	4.8	4.7	4.7	4.7	2.7	9.8	13	-1.1	27	23	9.5	3.5	18	3.3	11.5	6.0	23	5.1	6	4.8	6	4.4	6	4.1	0	
XI	0.6	0.6	3.9	5.9	3.8	4.3	4.3	4.3	1.9</td																					

## Jahresübersichten

1944

## **Stavanger**

Monat	Mittlere Relative Feuchte U <sub>m</sub>		Mittlere Bewölkung N <sub>m</sub>		Niederschlag R		Zahl der Tage n																																						
	Lufttemperatur T		Niederschl. R		Windstärke F		Regen	Schneefall	Häufigkeit	Frostscheine	Dauer	Nebel	Sonne	Heiter	Bewölkt	Schlecht																													
	6	14	19	Dien.	8	14	19	Σ	Max	Dec	°	V	%	°	V	%	h	%	kg	%	km/h	%	km/h	%	km/h	%	Regen	%	Schneefall	%	Häufigkeit	%	Frostscheine	%	Dauer	Std	Nebel	%	Sonne	%	Heiter	%	Bewölkt	%	Schlecht
I	84	84	84	84	8.3	7.8	8.3	109	13	6	10	3	0	0	0	26	24	2	10	3	0	22	15	11	3	0	5	0	1	20	8	11	1	20	9										
II	80	74	77	78	4.6	5.1	6.1	39	16	7	21	0	0	0	0	11	6	1	8	1	1	7	6	2	0	0	2	0	0	11	0	21	5	7	6	6									
III	81	76	80	80	7.1	6.5	7.0	51	8	13	13	0	0	0	0	22	12	0	0	0	0	18	14	10	2	4	3	0	0	11	4	22	1	15	0	0									
IV	78	74	75	75	7.5	6.5	6.2	38	9	11	2	0	0	0	0	16	9	0	6	2	2	15	3	2	2	0	1	0	0	9	6	25	1	9	0										
V	80	70	72	77	7.2	5.7	6.4	45	10	2	0	0	0	0	0	18	10	0	8	0	0	18	0	0	4	0	0	0	0	8	7	24	4	15	0										
VI	82	77	78	81	6.5	6.0	5.7	70	27	28	0	0	0	0	0	16	11	2	8	0	0	16	0	0	0	0	1	1	12	3	19	6	10	0											
VII	88	76	80	85	7.2	6.1	6.8	163	25	11	0	0	0	0	2	16	13	7	4	0	0	16	0	0	3	0	0	0	0	16	4	16	3	14	0										
VIII	87	76	82	84	6.4	5.7	6.2	110	36	29	0	0	0	0	2	16	11	4	2	1	1	16	0	0	0	0	1	1	14	3	25	5	9	0											
IX	86	75	81	82	7.1	6.5	7.6	193	31	30	0	0	0	0	0	23	17	9	7	2	0	23	0	0	4	0	1	0	0	9	1	20	1	10	0										
X	84	78	82	82	7.6	6.7	7.2	121	23	15	0	0	0	0	0	21	15	4	5	1	0	21	0	0	5	0	1	0	0	10	5	15	0	10	0										
XI	80	74	75	77	6.4	6.1	6.7	113	22	2	0	0	0	0	0	16	13	4	8	4	4	16	2	2	3	0	0	1	0	19	4	12	2	2	0										
XII	84	82	80	82	8.6	7.8	8.0	93	16	2	10	0	0	0	0	23	18	2	7	1	0	23	8	7	3	0	2	0	0	17	11	6	0	21	1										
1944	83	76	79	81	7.0	6.4	6.8	1145	36	58	3	0	4	224	159	35	77	15	8	211	48	34	36	0	19	0	5	156	56	219	29	146	21												

H <sub>0</sub> = 7		H <sub>0</sub> = 9.2		h <sub>0</sub> = 2.0		h <sub>0</sub> =		h <sub>0</sub> = 3.0		h <sub>0</sub> = 1.8		Skudesnes II.																									
I				8.6	7.5	7.4	155	16	14	7		27	24	5	18	1	23	13	5	3	0	0	0	23	3	11	1	14	0								
II				5.6	5.2	5.4	50	17	7	16		11	8	2	12	1	21	7	3	4	0	0	0	13	13	8	1	10	0								
III				6.6	6.4	6.6	80	11	19	15		15	11	1	14	3	0	14	7	3	4	0	0	0	18	5	5	2	11	0							
IV				6.8	5.4	5.7	54	14	11	2		12	9	1	20	3	0	12	0	3	3	0	0	0	10	4	4	27	5	9	0						
V				80	73	78	80	6.0	5.0	5.1	43	13	2	0	0	0	0	0	0	3	3	0	0	0	2	4	4	28	6	6	4	0					
VI				84	79	84	86	5.5	4.1	4.9	82	31	5	0	0	0	0	0	0	3	3	0	0	0	2	4	6	6	4	28	7	12	0				
VII				86	80	84	86	6.4	4.8	5.6	92	30	10	0	0	0	0	0	0	3	3	0	0	0	2	4	6	6	4	28	7	12	0				
VIII				85	80	83	84	5.5	5.8	5.9	136	60	19	0	0	0	0	0	0	3	2	0	0	0	0	3	10	4	4	26	5	10	0				
IX				89	74	81	81	7.0	6.3	7.3	139	23	30	0	0	0	0	0	0	1	0	0	0	0	0	1	9	2	25	0	12	0					
X				88	76	82	82	7.0	6.9	7.2	125	21	18	0	0	0	0	0	0	20	0	20	0	0	0	1	8	0	20	1	13	0					
XI				79	74	77	77	6.2	5.9	6.3	123	29	3		0	0	0	0	0	18	16	6	17	3	1	1	18	2	20	1	9	0					
XII				84	82	84	84	9.2	8.2	8.0	116	15	2	5		0	0	0	23	20	4	24	1	0	22	4	3	9	0	0	0	0	1				
1944								6.7	6.0	6.3	1195	60	48		0	0	0	214	165	36	168	21	3	202	43	69	54	0	0	0	10	114	32	252	40	132	0

## **Monats- und**

1944

$$\Phi = 60^\circ 25' N \quad \lambda = 7^\circ 20' E$$

$$\Delta G = +14$$

Maurset

Monat	Mittlerer Luftdruck Pa	Mittel. Luftdruck Höhenlage Pa	Mittlere Lufttemperatur T <sub>m</sub>				Lufttemperatur T						Windverteilung nD, F <sub>m</sub>															
			8	14	19	Dies	Max	Min	Max	Dec	Min	Dec	N	NE	E	SE	S	SW	W	NW	C							
I			-4.4	-3.8	-4.3	-4.5	-8.5	3.2	31	-23.5	10	10	1.2	65	1.7	8	2.0	65	3.8	45	2.1	11	1.8	335	2.2	13	2.3	0
II			-7.5	-5.4	-7.5	-7.2	-12.1	2.6	1	-22.4	10	95	1.1	165	1.2	8	1.6	8	1.7	35	1.0	8	3.4	165	2.2	17	2.2	0
III			-6.6	-3.3	-6.6	-6.3	-10.7	1.9	26	-17.2	4	65	1.5	10	1.1	75	1.3	2	1.0	45	1.0	10	1.2	34	1.7	125	1.1	6
IV			-2.0	1.1	-1.0	-1.7	-5.4	6.5	14	-22.4	1	65	1.1	95	1.2	10	1.7	12	1.2	65	1.9	6	1.0	175	1.8	9	1.3	13
V			2.0	4.4	2.5	1.8	-1.4	10.9	19	-10.5	7	75	1.1	15	1.6	105	1.2	1	1.0	95	1.6	10	1.2	21	1.5	65	1.3	12
VI			7.2	9.8	8.2	6.9	3.1	15.4	19	-2.2	1	15	2.7	13	2.6	13	2.9	9	3.0	35	1.7	8	1.9	245	2.2	105	1.8	2
VII			15.2	15.6	15.6	12.5	8.5	25.3	5	2.8	26	45	1.2	105	2.8	10	2.0	75	1.5	7	1.3	9	3.1	185	1.7	16	1.6	10
VIII			12.5	14.6	12.2	11.6	7.6	24.8	24	0.8	30	1	1.0	25	1.4	75	3.3	3	2.5	4	2.0	305	3.1	185	2.6	9	2.5	17
IX			6.3	8.1	6.1	6.3	4.1	14.2	2	-1.2	26	05	1.0	105	3.4	185	4.0	8	3.6	5	3.3	145	2.1	21	2.8	5	3.1	7
X			3.0	4.2	3.3	3.1	1.0	9.4	12	-4.6	22	1	3.0	10	3.8	285	4.0	14	4.1	4	2.5	2	3.8	165	2.3	20	2.0	14
XI			-4.5	-3.4	-5.0	-4.6	-0.5	4.0	4	-15.9	8	1	1.0	55	2.6	285	4.2	155	4.0	4	3.4	95	1.7	5	1.7	19		
XII			-3.1	-3.5	-3.6	-3.5	-6.1	4.0	18	-15.9	14	3	1.3	6	3.3	35	3.9	11	5.0	3	3.0	4	2.1	155	2.2	35	1.4	14
1944			1.3	3.2	1.5	1.2	-2.3	25.3	-23.5	525	1.2	1155	2.2	185	3.2	975	3.1	59	2.0	115	2.3	2515	2.1	110	1.9	114		

Ullensvang

$$\varphi = 60^\circ 19' \text{ N} \quad \lambda = 6^\circ 40' \text{ E} \quad g = 9.8$$

$$\Delta G = +1^h$$

I	1003.4	1005.0	- 1.2	2.0	- 1.9	1.5		- 1.0	7.8	31	- 7.4	12	2	1.8	8	1.6	28 <sup>a</sup>	1.5	20 <sup>a</sup>	1.9	25	2.8	45	2.9	23	2.2	53	3.2	19
II	13.8	15.4	- 0.4	1.9	- 0.2	0.1		- 2.7	7.4	1	- 9.1	28	0	-	8	1.0	26	1.3	33	1.4	19	3.3	35	2.9	2	2.7	6	2.4	7
III	09.5	11.1	0.5	2.9	0.9	0.9		- 1.8	6.6	18	- 4.2	31	0	-	6	1.2	19	1.4	25 <sup>a</sup>	1.5	33	2.1	3	1.5	23	2.2	25	1.7	10
IV	15.3	14.8	3.8	7.8	6.2	5.0		1.9	11.4	10	- 5.8	1	5	1.7	0	-	15	1.4	20	2.1	8	1.9	7	2.4	2	2.0	30	2.1	3
V	14.3	15.8	7.7	11.1	10.3	8.5		5.1	19.6	19	- 0.4	7	6	1.6	3	2.6	9	2.1	19	1.8	45	2.1	45	1.3	13 <sup>a</sup>	1.	29 <sup>a</sup>	1.9	4
VI	06.7	08.2	11.4	14.7	13.8	11.7		7.5	19.8	20	3.0 <sup>a</sup>	4	13	1.7	0	-	65	1.5	45 <sup>a</sup>	1.6	75	1.8	13	1.7	03	1.0	26	1.6	3
VII	09.9	11.4	15.1	19.6	18.0	16.0		11.8	25.2	4	8.8	3	13	1.7	13	1.5	05	0.2	42	1.4	33	1.7	5	2.4	03	2.0	22	1.8	5
VIII	11.9	15.3	14.4	18.2	16.0	15.4		15.0	24.0	3	7.5	30	33	1.7	45	1.9	15	1.7	50	1.1	3	1.2	6	2.0	13	2.7	23	1.5	0
IX	09.8	11.4	9.1	12.4	10.5	10.1		7.8	16.6	22	4.6	29	23	2.2	0	2.0	7	1.5	67	1.1	65	1.6	1	1.0	0	-	53	1.5	0
X	09.5	11.0	6.8	9.6	7.4	7.5		5.0	16.0	15	0.0	22	05	1.0	0	2.0	4	2.1	78	1.7	45	2.8	05	1.0	13	2.3	05	1.0	3
XI	02.8	04.4	2.6	3.5	2.3	2.5		- 0.5	10.3	13	- 9.7	16	0	-	0	-	2	3.5	81	2.0	13	2.0	23	4.8	0	-	2	3.0	1
XII	08.9	10.4	2.5	2.5	2.3	2.3		0.0	7.4	21	- 3.9	14	0	-	15	1.7	45	1.4	85 <sup>a</sup>	1.7	05	1.0	1	2.0	0	-	0	-	0
1944	1009.5	1011.0	6.2	8.8	7.4	6.8		3.8	25.2		- 9.7	22 <sup>a</sup>	1.7	45	1.5	123 <sup>a</sup>	1.6	565	1.6	47	2.0	40	2.3	26 <sup>a</sup>	2.0	2.0	175 <sup>a</sup>	1.9	55

Slir

$$\varphi = 60^\circ \text{ } 37' \text{ N} \quad \lambda = 7^\circ \text{ } 25' \text{ E}$$

$$\Delta G = +1$$

Myrdal

$$\varphi = 60^\circ 44' \text{ N} \quad \lambda = 7^\circ 7' \text{ E}$$

$$\Delta G = +1^{\circ}$$

I		- 3.9	- 3.3	- 3.7	- 3.8		- 6.6	3.7	16	-18.0	10	8	3.1	0	-	5	5.2	6	3.3	55	4.2	0	-	2	2.0	0	-	17		
II		- 7.2	- 4.9	- 6.5	- 6.5		- 9.3	1.3	1	-18.9	26	55	5.0	15	1.7	1	1.0	4	3.3	529	2.7	39	1.6	15	2.0	15	2.7	18		
III		- 6.0	- 2.8	- 5.7	- 5.4		- 8.5	3.9	8	-15.6	31	8	3.5	15	3.7	0	-	5	2.2	41	2.3	35	1.3	65	2.5	85	2.5	19		
IV		- 2.0	1.8	- 0.9	- 1.2		- 4.3	5.5	12	-16.1	1	89	1.9	15	3.3	15	1.7	84	3.9	42	2.7	4	1.9	3	1.3	1	4.0	20		
V		1.3	5.0	2.5	1.9		- 0.9	11.0	19	-10.9	6	10	1.8	3	3.0	3	1.5	1	3.0	33	2.2	1	2.0	35	1.9	85	1.6	30		
VI		5.9	9.2	7.1	6.3		3.3	16.5	19	-1.0	4	69	2.3	0	-	1	1.0	1	3.0	48	2.1	1	3.5	2	2.0	05	4.0	30		
VII		10.6	15.2	12.9	11.6		8.1	21.8	18	2.7	25	4	1.6	15	1.3	39	1.0	1	1.5	29	3.7	2	2.5	7	2.3	3	1.3	1	55	
VIII		10.3	14.6	12.0	11.3		8.1	25.0	24	1.4	30	1	1.0	1	1.0	0	-	05	1.0	355	3.0	0	-	0	-	0	-	0	-	55
IX		5.2 <sup>a</sup>	8.4 <sup>a</sup>	7.1 <sup>a</sup>	6.3 <sup>a</sup>		3.7 <sup>a</sup>	15.0 <sup>a</sup>	22 <sup>a</sup>	-2.0 <sup>a</sup>	13 <sup>a</sup>	20 <sup>a</sup>	2.2 <sup>a</sup>	0 <sup>a</sup>	-	0 <sup>a</sup>	-	2 <sup>a</sup>	4.0	27 <sup>a</sup>	3.2 <sup>a</sup>	4 <sup>a</sup>	2.4 <sup>a</sup>	0 <sup>a</sup>	-	2 <sup>a</sup>	1.8 <sup>a</sup>	35		
X		2.2	4.4	5.1	2.9		0.9	8.9	10	-3.9	21	5	1.4	1	2.0	0	-	85	2.6	61 <sup>a</sup>	3.5 <sup>a</sup>	2	4.0	3	4.0	0	-	17		
XI		- 4.1	- 3.7	- 4.1	- 4.2		- 6.7	2.1	13	-12.7	27	6	2.3	0	-	1	3.0	0	-	52	3.2	8	4.6	35	5.0	25	1.8	17		
XII		- 3.2	- 3.3	- 3.8	- 3.5		- 5.7	3.5	18	-12.8	4	5	1.8	1	2.0	0	-	05	5.0	74	3.9	15	1.0	0	-	0	-	11		
1944		0.8	3.4	1.7	1.3		- 1.5	25.0	-18.9		85	2.3	12	2.4	16	2.6	36	3.0	550 <sub>a</sub>	3.0	30 <sub>a</sub>	2.8	32	2.6	27 <sub>a</sub>	2.1	306			

Voss

$$\varphi = 60^\circ \text{ } 30' \text{ N} \quad \lambda = 60^\circ 26' \text{ E}$$

$$\Delta G = +1^\circ$$

I		-1.9	-1.1	-0.7	-1.4		-3.9	5.4	29	-21.1	12	1	1.0	27	1.8	13	2.6	0	-	5	3.0	18 <sup>a</sup>	2.5	0	-	20 <sup>b</sup>			
II		-4.2	-0.3	-1.9	-2.5		-6.1	6.7	1	-15.9	28	2	1.8	30	1.8	12	1.4	1	-	5 <sup>a</sup>	1.4	21	2.7	0	-	9			
III		-4.2	1.6	-0.2	-1.3		-5.1	7.5	26	-14.6	27	1	2.0	20	1.4	8	1.1	1	-	45	1.0	23	2.1	13	-	2.4			
IV		1.8	6.8	5.7	3.7		-0.1	10.7	13	-11.0	1	1 <sup>a</sup>	2.7	30 <sup>a</sup>	2.0	8	1.9	1	-	20	0.5	30 <sup>a</sup>	1.7	7	3.2	1	-	10 <sup>b</sup>	
V		6.7	11.3	10.1	7.7		3.2	18.1	18	-3.4	6	0 <sup>a</sup>	4.0	25	2.8	8 <sup>a</sup>	2.9	0	-	7 <sup>a</sup>	1.9	24 <sup>a</sup>	1.9	19	2.1	1	-	8	
VI		10.8	15.8	14.1	11.8		7.2	22.7	19	2.1	24	0 <sup>a</sup>	-	20 <sup>a</sup>	2.4	7 <sup>a</sup>	2.4	1	-	19	1.7	23	1.5	26 <sup>a</sup>	2.1	0	-	10 <sup>b</sup>	
VII		14.8	21.2	19.5	16.5		11.5	27.7	4	4.9	25	1	3.0	16 <sup>a</sup>	2.2	4 <sup>a</sup>	2.0	0	-	5 <sup>a</sup>	1.7	36	1.8	12 <sup>a</sup>	2.4	9	-	17	
VIII		13.7	19.7	17.3	15.3		10.7	26.4	3	4.1	30	0	-	18	1.8	4	2.0	0	-	6 <sup>a</sup>	1.7	32 <sup>a</sup>	1.5	21	2.6	0	-	11 <sup>b</sup>	
IX		8.4	12.9	11.1	9.8		6.7	17.6	22	-1.2	13	0	-	35 <sup>a</sup>	2.0	11 <sup>a</sup>	1.7	0	-	0 <sup>a</sup>	2.0	12 <sup>a</sup>	1.5	18 <sup>a</sup>	2.1	0 <sup>a</sup>	-	20 <sup>b</sup>	
X		5.7	8.7	7.0	6.7		4.1	15.1	12	-1.3	21	1	3.0	30	2.3	19	2.3	3	-	3 <sup>a</sup>	1.6	13 <sup>a</sup>	2.1	0 <sup>a</sup>	-	15 <sup>b</sup>			
XI		-0.4	1.5	0.4	0.2		-2.4	9.1	15	-8.9	27	1 <sup>a</sup>	1.0	35 <sup>a</sup>	2.9	35	2.2	0	-	0	-	8 <sup>a</sup>	2.7	55	1.5	0	-	6	
XII		-0.2	0.3	0.1	0.0		-2.3	5.7	11	-11.5	14	1 <sup>a</sup>	1.0	25 <sup>a</sup>	2.4	31 <sup>a</sup>	2.3	1 <sup>a</sup>	1.0	0 <sup>a</sup>	3.0	15	1.9	10	1.6	0 <sup>a</sup>	2.0	9	
1944		4.2	8.2	6.9	5.5		1.9	26.4		-21.1		11	2.0	312	2.2	155 <sup>a</sup>	2.1	8 <sup>a</sup>	2.4	40 <sup>a</sup>	1.8	255 <sup>a</sup>	1.9	161 <sup>a</sup>	2.2	53	2.5	-	148

Jahresübersichten

1944

	H <sub>e</sub> = 778				H <sub>e</sub> =				h <sub>e</sub> = 2.0				h <sub>e</sub> =				h <sub>d</sub> = 12.7				h <sub>r</sub> = 2.0				Mauren											
Monat	Mittlere Relative Feuchte U <sub>m</sub>				Mittlere Bewölkung N <sub>m</sub>				Niederschlag R				Zahl der Tage n																							
	8	14	19	Dm	8	14	19	S	Max	Dec	Lufttemperatur T	Niederschl. R	Windstärke F	Regen	Schne	Regen schne	Niede	Regen gruppe	Frost gruppe	Hagel	Ganzt	Dunst	Nebel	Sonne	Heiter	Bewöl	Schne	durc								
I	88	84	85	86	8.6	8.8	7.6	182	32	6	30	24	7	2	1	1	8	26	0	5	0	0	15	5	6	0	22	31								
II	80	71	75	77	6.4	5.9	5.4	53	14	8	29	8	3	0	0	0	3	8	1	0	0	0	4	2	4	9	29									
III	82	70	79	79	7.9	6.7	6.7	44	8	1	31	10	0	0	0	0	17	0	0	0	0	0	5	8	15	2	15	31								
IV	81	70	77	79	7.2	6.6	7.8	58	18	23	25	16	8	1	1	0	5	15	2	1	0	0	0	5	8	15	2	15	30							
V	76	67	71	73	7.1	6.4	7.0	54	8	1	17	15	12	0	0	0	9	10	0	9	0	0	0	6	6	21	3	12	27							
VI	72	67	71	74	7.4	7.1	7.3	74	37	15	5	47	12	1	0	0	16	0	0	14	0	0	4	6	4	18	1	14	0							
VII	77	67	76	78	6.5	7.1	6.1	80	17	12	0	16	14	6	1	0	16	0	0	10	0	0	2	6	10	19	4	14	0							
VIII	74	67	76	76	6.0	6.6	7.3	144	27	21	0	22	19	4	5	2	22	4	4	14	0	0	0	7	10	8	0	23	0							
IX	85	78	85	82	8.4	8.9	8.4	121	20	1	4	17	11	2	10	9	2	2	16	0	0	0	0	13	4	11	4	21	31							
X	84	76	85	82	8.6	8.5	7.5	72	16	4	29	9	6	1	0	17	11	2	11	0	0	0	0	10	1	14	4	21	30							
XI	81	73	79	79	7.0	6.9	6.4	68	21	6	29	19	10	2	0	2	2	18	0	1	0	0	0	14	1	11	4	20	31							
XII	80	80	80	80	8.4	7.9	7.8	65	15	26	30	205	148	29	50	13	1	116	113	9	87	0	0	6	106	51	166	20	194	209						
1944	80	72	78	78	7.4	7.3	7.1	1007	37	213	65	205	148	29	50	13	1	116	113	9	87	0	0	6	106	51	166	20	194	209						
	H <sub>e</sub> = 15				H <sub>e</sub> = 12.3				h <sub>e</sub> = 2.4				h <sub>e</sub> = 0.5				h <sub>r</sub> = 1.0				Ullensvang															
I	7.9	8.2	7.8	7.8	280	60	6	17	0	0	24	23	9	2	0	0	19	11	1	0	0	0	3	0	0	6	0	5	0	18	16					
II	6.7	4.8	4.9	77	25	8	24	0	0	15	12	2	0	0	0	6	10	1	0	0	0	0	0	0	0	0	15	4	11	0						
III	7.1	6.7	7.3	87	12	19	23	0	0	10	9	2	0	0	0	6	10	0	1	0	0	0	0	0	0	0	12	1	17	0						
IV	7.1	7.0	7.1	85	20	28	5	0	0	14	14	3	0	0	0	14	1	1	0	0	0	0	0	0	0	0	0	0	0	0						
V	86	73	73	82	7.8	6.7	7.0	81	20	3	1	13	13	2	0	0	13	0	0	0	0	0	0	0	0	0	0	0	0	0						
VI	92	74	79	87	91	6.4	5.9	5.2	53	15	14	0	13	10	2	0	13	0	0	0	0	0	0	0	0	0	0	0	0	0						
VII	94	79	87	91	5.2	5.7	6.6	201	26	19	0	16	14	8	0	16	0	0	0	0	0	0	0	0	0	0	0	0	0	0						
VIII	98	84	93	94	8.0	8.2	8.0	148	23	27	0	21	19	4	0	0	21	0	0	2	0	0	0	0	5	0	9	2	20	0						
IX	91	78	88	87	8.5	7.8	7.5	57	12	14	0	16	11	2	0	16	0	0	2	0	0	0	0	4	0	9	2	20	0							
X	79	76	78	78	7.6	6.3	4.8	90	27	5	13	12	7	3	0	12	0	0	0	0	0	0	0	0	4	0	9	7	11	0						
XI	78	78	78	78	7.1	7.9	7.0	123	20	26	11	17	13	6	0	13	4	0	1	0	0	0	0	0	4	0	4	3	17	0						
XII					7.1	6.9	6.6	1345	60	94	0	178	156	47	8	1	1	159	29	4	6	0	2	69	4	34	157	33								
1944	88	84	85	87	7.5	7.5	7.3	851	30	258	96	262	145	22	133	41	17	106	186	35	56	0	3	0	2	45	123	212	37	216	260					
	H <sub>e</sub> = 1300				H <sub>e</sub> =				h <sub>e</sub> = 3.2				h <sub>e</sub> = 11.5				h <sub>d</sub> = 10.0				Slirk															
I	93	93	93	93	8.4	8.3	9.1	75	11	23	31	30	17	1	24	8	0	30	0	0	0	0	0	9	10	1	23	31								
II	87	86	87	87	7.0	5.6	5.2	16	6	8	29	15	6	0	13	7	3	14	0	1	0	0	0	6	19	2	26	2	31							
III	88	86	87	87	7.5	6.9	7.0	28	10	1	31	21	5	0	15	5	2	24	0	1	0	0	0	8	22	1	16	30								
IV	88	85	85	86	7.5	6.9	7.6	22	4	22	30	21	7	0	11	3	1	21	1	1	0	0	0	5	10	0	15	2	30							
V	82	77	80	80	7.2	6.5	6.8	42	9	29	25	20	11	0	12	3	1	13	16	9	8	0	0	0	0	0	0	7	17	31						
VI	85	79	84	84	7.4	7.5	6.8	76	23	5	10	20	10	3	12	8	2	20	0	9	9	0	0	0	0	0	0	24	4	30						
VII	86	75	78	84	5.6	6.8	6.2	86	16	12	0	19	13	2	0	0	19	0	0	0	0	0	0	0	0	0	0	0	0	0						
VIII	83	73	79	82	6.3	6.9	7.0	225	30	13	2	16	15	8	0	10	3	1	23	14	7	13	0	0	0	0	0	0	0	0	0					
IX	83	86	90	90	8.4	8.9	8.8	137	16	1	12	27	0	0	24	13	0	10	0	0	0	0	0	0	0	0	0	0	0	0	0					
X	82	89	91	91	8.5	8.6	8.4	46	8	14	27	24	13	2	10	0	0	12	18	5	7	0	0	0	0	0	0	0	0	0	0					
XI	89	88	88	88	7.3	8.0	6.5	53	12	2	31	22	12	2	13	4	0	0	24	0	0	0	0	0	0	0	0	0	0	0	0					
XII	91	91	91	91	8.8	8.6	7.8	45	10	2	31	24	14	0	15	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0					
1944	88	84	85	87	7.5	7.5	7.3	851	30	258	96	262	145	22	133	41	17	106	186	35	56	0	3	0	2	45	123	212	37	216	260					
	H <sub>e</sub> = 870				H <sub>e</sub> =				h <sub>e</sub> = 1.9				h <sub>e</sub> = 9.6																							

1944

## Bergsdal

 $\varphi = 60^\circ 32' N$  $\lambda = 6^\circ 3' E$  $g =$  $\Delta G = + 1^h$ 

Monat	Mittlerer Luftdruck P <sub>a</sub>	Relative Feuchtigkeit P <sub>r</sub> %	Mittlere Lufttemperatur $T_m$				Lufttemperatur T				Windverteilung nD.F <sub>m</sub>																	
			8	14	19	Dies	Max	Min	Max	Des	N	NE	E	SE	S	SW	W	NW	C									
			-2.1	-1.9	-2.4	-2.4	-6.4	4.7	15	-22.1	12	25	1.4	4	1.2	5	1.8	75	2.9	55	3.7	95	4.1	31	3.8	12	2.8	16
I			-8.4	-5.0	-6.7	-6.5	-11.9	4.0	7	-25.8	28	1	1.5	75	1.0	11	1.7	9	2.6	45	4.2	65	3.0	10	4.2	95	2.8	28
II			-7.1	-1.0	-4.2	-4.8	-9.9	4.3	26	-20.5	22	85	1.5	6	1.1	12	2.4	1	3.0	1	2.0	1	2.0	155	3.3	14	2.9	34
III			-1.3	3.3	1.5	0.2	-3.6	7.7	15	-19.7	1	5	1.3	125	2.1	5	2.8	35	1.3	15	1.7	6	2.3	145	2.3	10	3.2	32
IV			3.5	6.7	5.5	4.0	-0.1	14.7	19	-9.6	7	6	1.8	05	1.0	14	2.0	9	1.5	1	1.5	7	2.4	155	2.2	14	3.2	26
V			8.5	11.0	10.2	8.2	4.0	16.1	19	-1.4	1	1	2.0	1	12	2.8	14	1.9	25	1.0	55	2.2	21	2.4	7	2.8	26	
VI			13.2	16.8	15.6	15.4	7.8	24.0	7	-0.2	25	25	1.8	0	-	5	3.4	5	2.0	2	1.0	10	1.4	185	2.2	14	2.2	36
VII			11.2	15.9	14.2	12.4	7.7	26.7	24	0.2	30	1	1.0	1	1.0	1	3.5	125	2.0	9	2.6	135	2.4	19	2.9	11	1.6	25
IX			6.4	10.1	8.3	7.6	3.9	16.9	18	-1.2	13	4	1.2	0	-	9	2.7	8	2.8	35	2.9	115	2.5	185	2.4	65	1.8	29
X			3.9	6.6	4.6	4.6	1.8	10.2	13	-4.3	21	05	1.0	45	1.4	105	2.7	19	2.9	75	2.5	65	2.6	11	2.4	35	2.0	30
XI			-2.6	-0.7	-2.6	-2.3	-6.1	6.6	13	-16.9	27	55	1.2	8	1.9	145	3.1	9	3.7	3	4.2	105	3.5	2	2.5	21		
XII			-2.5	-2.0	-3.1	-2.6	-6.1	5.3	18	-16.6	31	25	1.0	45	1.2	135	3.1	22	2.7	12	3.0	55	3.6	15	3.7	4	2.8	14
1944				1.8	5.2	3.4	2.6	-1.6	26.7	-25.8	40	1.4	495	1.5	1125	2.6	127	2.5	55	2.9	655	2.6	200	3.0	1075	2.6	317	

## Bergen (Fredriksberg)

 $\varphi = 60^\circ 24' N$  $\lambda = 5^\circ 19' E$  $g = 9.819$  $\Delta G = + 1^h$ 

Monat	1004.3	3.2	4.2	3.4	3.5	5.4	-1.1	9.0	15	5.4	12	115	2.0	2	3.2	4	2.5	27	3.4	205	4.2	35	2.6	35	2.4	14	2.5	7	
I	998.8	1004.3	3.2	4.2	3.4	3.5	5.4	-1.1	9.0	15	5.4	12	115	2.0	2	3.2	4	2.5	27	3.4	205	4.2	35	2.6	35	2.4	14	2.5	7
II	1009.1	14.6	1.2	3.0	1.9	1.8	4.1	-0.1	8.2	1	6.5	28	255	2.2	145	2.7	155	2.4	3	2.7	45	3.7	21	3.4	45	4.2	0	2	2.5
III	05.5	11.1	1.2	4.0	2.7	2.5	4.8	0.1	9.6	26	4.2	31	285	2.4	45	2.2	4	2.2	185	2.8	65	2.6	05	2.0	5	1.2	135	2.3	10
IV	09.0	14.5	4.7	7.6	6.1	6.0	8.6	0.2	14.9	9	-3.0	1	9	2.8	15	1.7	4	2.0	195	3.0	21	3.3	35	2.4	25	3.0	16	2.5	13
V	10.8	16.2	8.3	10.9	9.4	8.6	12.0	5.6	21.2	18	1.0	7	205	2.9	35	2.9	05	2.0	65	3.0	205	3.0	55	2.5	45	1.7	215	2.6	8
VI	03.6	08.9	11.0	13.8	12.9	11.7	15.4	9.1	20.2	27	1	105	2.3	1	2.0	2	1.5	55	3.3	18	3.2	9	2.6	22	2.4	14			
VII	06.9	12.2	14.7	18.7	17.5	16.0	20.6	12.9	28.2	5	8.3	25	9	2.4	15	1.7	05	3.0	55	2.2	85	2.4	75	1.8	9	1.3	265	1.7	25
VIII	08.9	14.2	15.5	17.1	15.4	14.6	18.2	11.9	25.7	24	7.2	30	10	1.8	1	1.0	03	1.0	7	2.9	145	3.5	9	2.3	95	1.6	225	1.7	19
IX	06.0	11.4	10.8	13.5	11.8	11.6	14.6	9.2	19.8	22	5.0	27	11	2.0	0	-	2	2.5	125	2.9	195	2.8	3	3.0	65	1.5	165	2.0	19
X	04.9	10.4	8.5	10.5	8.8	9.0	11.3	7.0	15.3	13	-1.4	27	145	2.2	5	3.5	25	2.1	30	3.0	175	3.2	05	1.0	3	1.3	5	1.8	23
XI	997.7	03.1	3.9	5.6	4.4	4.4	6.6	2.1	12.4	13	-1.4	27	145	2.2	5	3.5	25	2.2	185	3.2	155	3.4	5	1.9	3	1.8	11	1.7	15
XII	1003.9	09.4	3.3	3.7	3.4	3.4	5.5	1.7	9.2	18	-3.7	16	95	2.9	45	2.8	10	2.2	28	3.5	21	4.2	0	-	2	2.0	6	2.2	12
1944	1005.4	1010.9	7.0	9.4	8.1	7.7	10.6	5.3	28.2	-	-6.5	165	2.4	31	2.6	385	2.1	202	3.1	2005	3.4	475	2.3	605	1.8	182	2.1	171	

## Syfteland

 $\varphi = 60^\circ 14' N$  $\lambda = 5^\circ 27' E$  $g =$  $\Delta G = + 1^h$ 

Monat	1.3	1.8	1.4	1.3	-1.8	7.3	29	-10.9	4	35	3.0	35	2.4	4	2.5	2	2.5	265	3.2	85	2.9	1	3.0	1	2.0	45	4.2	
-------	-----	-----	-----	-----	------	-----	----	-------	---	----	-----	----	-----	---	-----	---	-----	-----	-----	----	-----	---	-----	---	-----	----	-----	--



Monats- und

1944

Fjærland

$\varphi = 61^\circ 26' N$   $\lambda = 6^\circ 46' E$   $g =$   $\Delta G = +1^h$

Monat	Mittlerer Luftdruck Pa	Nied. Höhenaus- satz Pa	Mittlere Lufttemperatur $T_m$				Lufttemperatur $T$				Windverteilung nD.F.m																
			8	14	19	Dies	Max	Min	Max	Dat	Min	Dat	N	NE	E	SE	S	SW	W	NW	C						
I	- 1.5	- 0.8	- 0.9	- 1.2	1.9	- 3.9	9.0	16	- 18.0	10	55	1.0	59	1.0	2	2.0	1	1.0	59	2.6	49	2.3	2	2.5	67		
II	- 4.5	- 0.3	- 2.9	- 3.0	1.2	- 7.1	5.8	22	- 19.0	28	75	1.0	88	1.1	25	1.4	13	3.0	6	3.2	29	2.2	49	1.9	33	2.7	51
III	- 3.0	2.0	- 0.9	- 1.0	3.1	- 4.8	6.5	24	- 14.7	31	75	1.7	29	1.0	1	1.0	0	-	1	2.0	4	2.0	5	2.1	6	1.8	66
IV	0.0	4.5	2.2	1.5	5.6	- 2.0	9.0	23	- 13.6	1	7	1.6	4	1.1	1	2.0	0	-	2	3.5	0	-	2	2.5	3	2.7	71
V	6.0	9.9	8.0	6.8	11.0	2.4	18.9	18	- 5.5	6	235	1.9	12	1.3	8	1.5	93	2.0	4	2.8	3	1.3	4	1.9	6	2.4	32
VI	11.3	15.0	13.8	11.9	16.4	6.9	21.2	30	0.7	24	95	2.2	69	1.2	2	1.0	0	-	3	2.7	12	1.4	3	1.0	3	1.7	51
VII	14.5	20.5	17.8	15.6	21.6	9.0	27.4	5	2.2	25	4	1.0	2	1.0	1	1.0	0	-	12	1.2	4	1.0	05	1.0	83	2.5	61
VIII	11.4	17.3	14.5	13.1	18.5	8.4	26.4	2	3.2	22	0	-	1	1.0	0	-	0	-	135	1.4	45	2.0	0	-	4	1.2	70
IX	8.2	12.6	10.1	9.8	13.6	6.4	18.8	22	0.7	27	0	-	19	1.3	19	1.3	19	2.7	6	1.7	5	1.0	5	1.6	1	3.0	68
X	6.1	8.9	6.5	6.8	10.0	3.6	16.1	12	- 2.9	10	0	-	1	1.0	7	3.3	7	3.7	6	1.5	1	1.0	1	2.0	1	1.0	69
XI	0.5	2.2	0.4	0.8	3.7	- 2.2	12.6	13	- 7.5	27	11	1.3	4	1.0	3	2.0	5	3.2	8	2.6	1	4.0	0	-	8	1.9	50
XII	- 0.1	0.2	- 0.5	- 0.2	2.5	- 2.8	8.0	8	- 10.2	31	7	1.1	8	1.0	6	1.8	1	2.0	3	3.5	7	- 2.3	2	1.5	0	-	59
1944											82	1.6	56	1.1	35	1.9	17	3.1	65	2.0	49	1.8	31	1.9	46	2.1	715

Lærdal

$\varphi = 61^\circ 6' N$   $\lambda = 7^\circ 29' E$   $g = 9.819$   $\Delta G = +1^h$

I	1003.0	1003.5	0.2	0.7	- 1.0	0.4	- 2.1	8.6	15	- 11.7	5	2	1.0	0	-	2	1.0	3	5.0	0	-	26	1.5	23	2.3	12	1.3	25
II	14.4	14.9	- 2.1	- 0.4	- 1.4	- 1.6	- 4.6	5.4	16	- 12.9	28	2	0.5	1	1.0	11	0.9	5	4.6	0	-	13	1.8	2	1.0	22	1.4	31
III	0.9	10.4	- 1.6	1.7	0.4	- 0.3	- 2.7	6.4	10	- 9.5	7	0.4	7	1.0	3	1.3	0	-	0	-	5	0.8	9	1.6	19	1.7	45	
IV	15.9	14.4	3.5	6.6	5.7	4.5	1.8	13.3	20	- 7.2	1	0	-	10	1.0	0	-	2	4.0	0	-	14	1.1	12	1.1	30	1.2	22
V	15.4	15.9	7.9	11.7	10.5	8.7	5.3	17.6	18	- 0.2	7	0	-	8	1.1	21	1.1	0	-	0	-	0	-	17	1.	39	1.4	8
VI	07.9	08.4	12.6	15.6	15.1	13.0	9.3	20.8	19	4.6	4	1.0	9	1.1	5	2.8	10	2.1	4	1.0	1.0	0	165	1.1	225	1.0	16	
VII	11.0	11.5	16.6	19.4	19.2	16.8	12.4	24.4	21	7.8	26	2	1.0	8	1.0	11	2.5	1	1.0	0	-	18	1.3	7	1.3	38		
VIII	12.7	13.2	14.4	17.8	16.7	15.1	11.5	23.4	4	7.7	23	0	-	0	-	5	1.0	6	1.5	2	1.0	25	0.9	16	1.0	14	1.6	25
IX	11.0	11.4	9.1	12.2	10.9	10.1	7.8	17.6	22	3.6	14	0	-	0	-	0	-	19	2.2	0	-	19	0.9	22	1.1	8	1.1	22
X	10.8	11.2	7.1	9.1	8.1	7.7	5.2	16.2	13	- 2.0	22	0	-	0	-	6	2.7	30	3.7	2	1.0	0	-	3	1.0	8	1.0	44
XI	04.7	05.2	1.4	2.7	1.9	1.8	- 0.8	11.1	13	- 6.9	28	0	-	2	1.0	13	3.8	21	3.0	0	-	10	1.3	0	-	5	1.0	39
XII	09.8	10.3	1.9	2.1	2.1	1.9	- 0.8	11.2	1	- 7.8	14	0	-	0	-	4	1.0	27	3.5	4	1.8	18	1.2	5	1.2	8	1.5	27
1944	1010.4	1010.9	5.9	8.5	7.5	6.5	3.5	24.4	- 12.9	12	0.7	45	1.0	78	1.7	134	3.1	13	1.2	136	1.2	143	1.3	1945	1.3	342		

Leikanger

$\varphi = 61^\circ 11' N$   $\lambda = 6^\circ 52' E$   $g =$   $\Delta G = +1^h$

I	1.2	1.8	- 1.6	- 1.3	- 0.8	- 2.6	8.3	15	- 8.0	10	35	1.6	3	1.2	7	1.0	24	1.7	139	1.7	123	2.6	17	2.8	103	2.2	2		
II	- 1.2	1.8	- 0.2	- 0.1	- 0.4	- 2.9	2.9	1.1	0.8	28	15	1.7	95	1.2	105	1.4	305	1.4	133	1.4	123	1.8	205	2.7	3	2.2	1		
III	- 0.4	6.3	5.7	4.7	2.5	10.2	23	- 5.7	1	15	2.0	65	2.0	123	1.7	123	1.1	263	1.1	3	1.5	7	1.4	15	2.2	25	1		
IV	7.0	10.8	10.1	8.2	5.4	18.8	18	- 0.2	6	25	2.0	35	2.0	11	2.0	13	1.6	215	1.3	14	1.7	9	2.3	175	2.7	1			
V	11.7	15.3	14.7	12.6	9.2	19.6	19	5.3	25	33	2.4	15	1.0	05	1.0	12	2.1	245	1.4	123	1.6	23	2.3	123	2.4	0			
VI	15.1	20.1	19.5	16.8	15.0	24.3	22	8.2	25	0	2	1.0	33	1.0	12	1.2	385	1.4	19	1.5	14	2.1	5	1.9	1				
VII	15.3	18.1	16.7	14.9	11.6	25.2	4	7.5	15	05	2.0	2	12.5	5	1.1	123	1.5	245	1.7	175	2.5	1	2.1	1					
IX	9.7	13.1	11.0	10.7	8.4	17.2	5	3.6	27	35	1.5	03	1.0	43	1.6	20	1.3	345	1.3	7	1.6	8	2.9	8	2.2	2			
X	7.7	9.8	7.9	8.2	5.9	15.6	13	0.7	21	3	1.5	15	1.3	6	1.7	30	2.2	22	2.1	125	1.9	83	2.5	6	2.5	3			
XI	2.6	3.8	2.7	2.8	0.5	10.6	13	- 3.5	27	65	1.6	103	1.9	25	1.9	25	1.7	105	2.0	53	2.8	59	2.7	13	2.0	0			
XII	2.8	2.8	2.6	2.6	0.7	8.4	24	- 4.0	31	5	1.7	3	2.5	1.2	25	1.2	295	2.3	45	1.5	53	2.1	7	3.1	10	2.6	2		
1944										4.4	25.2	- 9.5	395	1.8	57	1.7	99	1.5	249	1.7	258	1.5	132	1.8	153	2.5	97	2.4	13

Luster Sanat.

$\varphi = 61^\circ 26' N$   $\lambda = 7^\circ 25' E$   $g =$   $\Delta G = +1^h$

I	- 2.6	- 1.8	- 2.2	- 2.4	- 4.4	5.3	15	- 13.2	10	14	1.2	1	2.0	13	1.0	1	2.0	29	2.0	95	2.9	27	1.9	243	1.3	12



<tbl



# Monats- und

1944

## Fanaråken<sup>1)</sup>

Monat	Mittlerer Luftdruck hPa	Luftfeuchtigkeit %	Windrichtung Winkel °	Mittlere Lufttemperatur $T_m$				Lufttemperatur $T$				Windverteilung nD.F. <sub>n</sub>																		
				8	14	19	Dies	Max	Min	Max	Dat	Min	Dat	N	NE	E	SE	S	SW	W	NW	C								
I	769.7	773.2	-12.0	-11.1	-11.5	-11.6	-9.0	-14.3	-3.3	15	-21.4	10	8	4.5	0.9	3.0	1	3.0	45	4.1	4	2.9	21	5.3	195	5.6	283	6.1	6	
II	78.4	82.0	-12.0	-11.0	-11.9	-11.7	-8.9	-14.4	-2.4	23	-21.3	28	175	4.7	59	4.2	3	2.5	12	2.9	3	4.0	14	6.9	133	5.3	11			
III	75.0	78.5	-12.4	-10.3	-12.3	-12.0	-8.6	-14.5	0.4	23	-19.1	4	30	4.9	49	4.5	0.9	1.0	1	1.0	0.9	7.0	25	4.6	145	6.7	275	5.5	12	
IV	90.9	84.4	-8.5	-7.7	-9.0	-8.8	-5.8	-11.2	1.0	10	-19.1	1	45	5.0	2	3.0	13	3.7	85	4.9	45	4.4	28	4.4	255	5.1	75	3.5	7	
V	84.6	88.1	-6.3	-5.2	-6.1	-6.3	-3.8	-8.8	1.0	27	-16.1	6	7	3.0	2	1.5	85	2.7	8	4.6	22	4.7	115	4.0	10	3.9	16			
VI	82.5	86.0	-2.0	-1.0	-1.3	-2.0	0.5	-3.8	2.9	19	-9.0	23	13	3.5	0.9	3.0	113	4.4	113	3.5	12	2.8	135	3.4	14	3.6	45			
VII	89.5	92.9	5.0	6.2	5.2	4.6	7.4	2.2	11.9	8	-5.0	25	13	2.3	3	2.2	1	1.5	93	3.1	205	3.1	2	2.5	59	2.0	7	1.5	43	
VIII	89.6	95.0	4.3	5.3	4.5	4.0	6.8	0.4	15.1	24	-7.0	30	13	2.3	0	-	3	4.0	7	2.2	135	4.9	23	4.7	275	4.1	35	4.3	14	
IX	84.5	87.9	-2.0	-0.7	-2.2	-2.0	0.3	-4.1	9.0	19	-9.0	27	3	3.3	29	2.6	85	3.3	185	3.6	7	3.6	75	3.5	13	3.9	10	3.8	20	
X	81.9	85.3	-5.3	-4.0	-5.3	-5.0	-2.9	-7.0	1.1	11	-12.4	31	0	-	1	1.0	0	-	265	4.8	185	5.4	14	4.2	155	5.2	115	6.4	6	
XI	72.6	76.1	-10.5	-10.3	-11.1	-10.7	-8.7	-12.8	-1.8	15	-16.1	17	85	3.1	5	3.2	135	4.4	115	5.3	25	4.4	8	4.0	11	-	-	-	-	-
XII	75.2	79.7	-10.5	-10.2	-10.7	-10.6	-8.7	-12.8	-4.2	2	-18.9	17	3	3.7	1	4.0	95	5.0	155	5.1	14	5.8	65	4.9	6	-	-	-	-	-
1944	780.4	785.9	-6.0	-5.0	-6.0	-6.0	-3.5	-8.4	15.1	-21.4	86	4.2	275	3.2	615	3.9	1495	4.0	112	4.3	1725	4.6	178	5.0	138	4.9	173			

## Førde i Sunnfjord

Monat				Mittlere Lufttemperatur $T_m$				Lufttemperatur $T$				Windverteilung nD.F. <sub>n</sub>																
				8	14	19	Dies	Max	Min	Max	Dat	Min	Dat	N	NE	E	SE	S	SW	W	NW	C						
I	-0.2	0.7	0.5	0.2	-2.9	7.6	29	-16.0	10	2	2.2	3	2.8	37	1.8	0	-	0	-	75	3.9	245	2.6	9	2.3	10		
II	-1.7	1.0	0.1	-0.8	-3.1	7.1	22	-11.3	28	4	4.5	59	3.9	455	1.5	0	-	3	2.3	8	4.1	89	2.9	25	6.6	10		
III	-2.0	1.2	0.7	-0.4	-3.3	8.0	26	-9.3	21	13	2.3	11	1.7	43	1.3	1	2.0	1	1.0	29	3.0	255	2.8	03	3.0	7		
IV	2.1	6.9	5.3	3.9	0.2	11.0	14	-6.7	1	75	2.5	185	2.0	36	2.0	3	1.3	1	2.0	3	1.7	8	2.1	10	3.4	3		
V	6.8	11.4	9.5	7.9	3.4	20.0	18	-4.3	6	4	4.9	3	3.0	445	1.9	3	2.3	0	-	3	1.3	145	3.1	16	3.4	5		
VI	10.9	15.0	13.6	11.7	7.3	19.7	7	1.0	1	4	3.6	5	2.4	21	2.1	6	4.7	0	-	27	3.0	21	3.0	6	-	6		
VII	14.7	20.6	19.0	16.3	10.9	27.9	5	5.2	25	0	-	0	-	19	1.9	22	3.5	6	3.3	6	2.0	45	2.5	6	3.7	11		
VIII	12.2	17.5	15.7	13.8	9.6	25.1	24	3.1	22	2	2.8	1	2.0	24	2.1	2	2.0	1	4.5	11	2.8	19	2.8	63	2.7	26		
IX	8.8	15.2	11.1	10.3	6.7	17.8	20	2.0	27	1	3.0	2	2.5	25	2.2	0	-	0	-	1	3.0	11	1.4	7	2.0	45		
X	6.3	9.5	7.7	7.4	4.5	14.9	12	-1.6	21	0	-	7	2.8	41	2.4	0	-	0	-	0	-	3	1.7	4	3.0	56		
XI	0.9	2.3	1.1	1.2	-1.1	11.0	13	-6.8	27	2	6.0	1	3.0	48	2.7	0	-	0	-	0	-	0	-	0	3.3	5	2.8	31
XII	0.6	1.6	0.8	0.9	-2.5	9.7	18	-11.2	17	13	3.3	0	-	57	2.4	2	4.5	0	-	0	-	1	1.0	105	3.7	21		
1944	5.0	8.4	7.1	6.0	2.4	27.9	-16.0	30	3.5	57	2.4	439	2.0	19	3.2	12	2.9	42	3.0	188	2.5	98	3.1	213				

## Kinn

Monat			Mittlere Lufttemperatur $T_m$				Lufttemperatur $T$				Windverteilung nD.F. <sub>n</sub>																	
			8	14	19	Dies	Max	Min	Max	Dat	Min	Dat	N	NE	E	SE	S	SW	W	NW	C							
I	1001.2	1002.2	5.8	4.1	4.2	3.9	1.8	8.2	29	-4.5	9	133	4.7	4	4.8	9	4.2	75	6.2	13	5.5	11	5.4	85	5.2	0		
II	12.8	15.9	2.6	3.1	2.9	2.7	1.0	7.5	7	-3.1	28	11	5.8	22	5.3	35	3.0	113	3.8	25	6.5	75	6.3	23	5.2	3		
III	09.6	12.7	2.0	3.6	3.5	2.7	0.7	7.0	26	-2.9	4	175	5.2	21	4.4	45	1.5	6	3.5	24	4.6	9	4.3	39	4.0	75	3.8	0
IV	13.2	14.3	4.4	6.0	5.5	4.9	3.2	9.4	9	-0.6	5	11	4.7	93	5.1	10	2.6	14	3.8	235	4.9	14	3.5	69	4.2	15	5.0	0
V	15.7	16.7	7.0	8.2	7.4	7.0	5.2	12.4	17	1.1	6	235	4.9	265	6.2	35	3.4	6	3.5	145	4.5	1	5.0	2	4.0	1		
VI	8.3	0.9	10.7	11.9	11.4	10.7	8.8	19.2	27	5.5	4	33	4.3	93	3.9	45	3.6	95	2.8	135	4.2	135	3.3	0	-	55	2.5	11
VII	11.8	12.6	14.7	15.7	14.8	14.4	12.2	22.4	5	7.8	26	405	4.1	13	6.5	75	2.6	21	85	2.5	95	3.0	0	9	3.0	75	3.5	1
VIII	12.8	13.8	13.5	14.5	13.8	13.3	11.4	18.6	25	6.7	15	185	3.0	113	5.2	05	4.0	6	2.1	235	5.3	195	3.9	5	4.4	85	2.7	0
IX	10.0	11.0	11.2	12.3	11.6	11.4	9.6	16.8	22	4.2	29	95	4.2	195	5.4	6	3.5	125	4.6	11	3.9	5	3.9	55	4.5	0		
X	08.6	0.9	9.2	9.8	9.6	9.3	7.6	14.2	12	3.7	31																	

## Jahresübersichten

1944

$$H_1 = 2064 \quad H_2 = 2070.3 \quad h_1 = 4.2 \quad h_2 = 9.7$$

$$h_0 = 9.7 \quad h_r = 2.5$$

Fanariken

Monat	Mittlere Relative Feuchte U <sub>m</sub>		Mittlere Bewölkung N <sub>m</sub>		Niederschlag R		Zahl der Tage n																																
							Lufttemperatur T																																
	8	14	19	Dien	8	14	19	Σ	Max	Dec	°	V	%	V	%	V	%	V	%	V	%	V	%	V	%	V	%	V	%	V	%	V	%	V	%	V	%	V	%
	8	14	19	Dien	8	14	19	Σ	Max	Dec	°	V	%	V	%	V	%	V	%	V	%	V	%	V	%	V	%	V	%	V	%	V	%	V	%	V	%		
I	8.8	8.6	8.5	175	19	28	31	31	28	0	29	27	6	28	22	15	0	29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	26	4	1	22	31	
II	6.6	7.0	6.0	76	14	1.	29	29	26	0	21	17	2	24	13	11	0	18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	25	14	6	15	29		
III	8.1	8.3	7.9	70	9	4	31	31	28	0	26	15	0	27	19	10	0	24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	29	14	1	19	31		
IV	8.0	7.8	8.1	73	27	28	30	29	17	0	24	14	1	24	13	3	0	24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	26	12	4	22	31		
V																																							
VI	7.1	7.2	7.7	61	13	29	31	27	15	0	18	14	0	21	6	3	0	18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	24	13	6	21	31	
VII	8.2	8.4	8.7	60	14	15	29	13	0	0	21	13	2	17	17	1	0	19	1	2	0	0	0	0	0	0	0	0	0	0	0	0	25	16	0	20	30		
VIII	5.6	7.2	6.6	57	13	12	8	0	0	0	12	11	2	3	0	0	0	6	6	6	0	0	0	0	0	0	0	0	0	0	0	0	0	19	19	6	15	31	
IX	6.1	7.3	7.3	156	24	21	14	3	0	0	18	14	8	20	10	6	0	14	8	5	3	0	0	0	0	0	0	0	0	0	0	0	2	21	18	5	18	6	
X																																							
XI	8.7	9.1	9.3	94	21	17	29	13	0	0	23	17	3	15	2	0	6	23	2	2	0	0	0	0	0	0	0	0	0	0	0	0	0	28	6	1	23	28	
XII	8.5	8.8	8.5	46	8	14	51	28	1	0	21	11	0	26	15	1	2	20	1	1	0	0	0	0	0	0	0	0	0	0	0	0	28	7	3	24	31		
XIII	8.0	7.5	6.8	61	1	30	30	26	0	0	25	15	0	22	8	5	0	25	0	0	0	0	0	0	0	0	0	0	0	0	0	29	3	1	16	31			
XIV	8.4	9.4	8.8	114	16	30	31	31	23	0	23	22	2	24	11	5	0	23	0	0	0	0	0	0	0	0	0	0	0	0	0	31	3	0	22	31			
1944																																							
	7.7	8.0	7.8	1043	27		324	265	164	0	263	190	26	252	121	65	37	239	13	16	0	0	0	0	0	0	0	0	0	0	2	3	313	134	34	239	329		

$H_2 = 3$        $H_{23} = 1.3$        $H = 14.8$        $H = 17$

Førde i Sunnfjord

$$H_1 = 0 \quad H_2 = 0.2 \quad h_3 = 1.0 \quad h_4 = \quad h_5 = \quad h_6 = 1.4$$

Kinn

$$H_1 = 19 \quad H_2 = \quad H_3 = 3.8 \quad H_4 = \quad H_5 = \quad H_6 = 2.2$$

Brandsby i Kinn

$$B_0 = 7.1 \quad B_0 = \quad B_0 = 1.9 \quad B_0 = \quad B_0 = \quad B_0 = 1.7$$

Nordfjordeld

I	9.2	9.5	8.7	378	43	6	16	1	27	25	14	0	0	0	19	16	6	0	0	3	0	0	0	1	0	0	29	31			
II	8.3	9.1	7.9	176	45	8	20	1	18	15	7	0	0	0	10	15	3	0	0	0	0	0	0	1	0	3	20	28			
III	8.2	7.9	7.1	192	35	11	25	0	25	19	8	0	0	0	11	21	2	0	0	0	0	0	0	1	1	2	19	31			
IV	8.0	8.0	8.3	148	42	27	7	0	20	19	3	0	0	0	20	5	3	0	0	0	0	0	0	1	1	12	21	14			
V	7.2	7.0	7.6	94	20	14	2	0	15	14	4	0	0	0	14	6	2	0	0	1	0	0	0	0	16	4	18	1			
VI	6.5	8.3	7.0	69	17	9	0	0	15	10	2	0	0	0	15	6	0	0	0	0	0	0	0	1	15	2	19	0			
VII	5.5	5.4	5.3	48	29	12	0	0	8	7	1	0	0	0	8	8	0	0	0	0	0	0	0	0	23	7	10	0			
VIII	7.0	6.6	6.6	113	22	11	0	0	13	12	4	0	0	0	13	0	0	0	0	0	0	0	0	0	3	17	6	17	0		
IX	87	74	84	84	7.0	6.6	6.6	0	16	16	6	0	0	0	16	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
X	87	82	86	86	9.3	9.0	8.8	125	15	26	0	0	0	0	16	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
XI	82	75	78	79	7.5	8.5	8.3	113	26	2	1	0	0	0	16	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
XII	77	75	78	76	7.6	7.0	5.7	137	23	7	19	0	0	0	16	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
XIII	77	75	78	76	7.5	6.5	5.8	190	23	26	16	0	0	0	16	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
1984					7.8	7.7	7.3	1745	45	106	2	206	186	42	2	0	0	169	78	18	0	2	5	0	3	1	9	111	39	224	130

## Monats- und

1944

Opstryn

$$\varphi = 61^\circ 56' \text{ N}$$

$\lambda = 7^{\circ} 13' E$        $g =$

$$\Delta G = +1^h$$

Monat	Mittlerer Luftdruck P <sub>a</sub> hPa	Mittel. Luftdruck Normalwerte P <sub>a</sub> , hPa	Mittlere Lufttemperatur T <sub>m</sub>				Lufttemperatur T						Windverteilung nD, F <sub>m</sub>													
			8	14	19	Dies	Max	Min	Max	Dat	Min	Dat	N	NE	E	SE	S	SW	W	NW	C					
I			0.4	0.4	0.6	0.4	-2.1	7.0	15	-9.7	10	0	-	29	1.6	4	1.6	05	3.0	3	2.8	55				
II			-1.6	-0.9	-1.2	-1.4	-3.5	5.9	16	-10.8	28	0	-	35	2.4	7.9	2.3	25	3.6	15	4.7	39				
III			-1.3	0.8	-0.7	-1.5	-3.1	4.8	26	-8.8	31	0	-	35	1.7	53	1.4	5	1.5	0	-	2				
IV			2.1	4.4	2.8	2.5	0.7	10.2	19	-4.4	2	1	2.5	7.9	2.5	8	2.2	3	2.0	29	1.8	70				
V			5.4	8.2	6.1	5.6	2.9	14.6	28	-1.9	5	05	2.0	13	2.3	225	2.0	4	2.0	2	2.0	5	2.2	40		
VI			10.3	13.3	11.5	10.6	7.7	17.9	19	3.1	4	05	2.0	7	2.1	13	1.7	10	2.6	65	2.3	75	1.2	39		
VII			15.2	19.9	16.2	15.7	11.9	25.5	8	6.1	25	05	1.0	53	2.1	18	1.4	4	2.2	2	2.2	2	3.0	19		
VIII			12.9	17.8	15.2	14.2	10.9	26.6	3	6.5	15	0	-	1	2.5	35	2.0	3	1.8	25	1.6	6	2.3	4		
IX			9.4	12.6	10.5	10.1	7.3	19.2	19	2.1	27	0	-	19	1.3	45	1.3	09	1.0	7.9	2.4	95	3.2	8		
X			7.8	9.5	8.1	8.1	5.5	15.0	15	-0.4	21	0	-	0	-	53	1.8	65	2.5	10	2.7	125	2.2	45		
XI			2.0	2.3	1.9	1.9	-0.5	14.8	13	6.1	9	0	-	6	1.9	18	1.9	75	2.7	53	2.7	45	3.1	25		
XII			2.4	2.1	1.6	1.9	-0.7	11.2	1	-5.6	16	0	-	5	2.5	195	2.3	7	2.5	53	2.3	5	2.5	1.7		
1944			5.4	7.5	6.0	5.7	3.1	26.6	-10.8	29	2.0	98	2.2	1295	1.9	515	2.5	485	2.5	655	2.5	955	2.1	26	2.2	661

Kråkenes Fyr

$$\Phi = 62^\circ \text{ N}$$

$\lambda = 4^{\circ} 39' \text{ E}$

$$\Delta G = +1^b$$

## Tafjord

$$\Phi = \Phi^0 + \Psi^0 N$$

$$\lambda = 7^{\circ} \text{ E}$$

$$\Delta G = + 1^h$$

I	997.6	1001.0	1.1	2.1	1.7	1.5		-1.0	10.0	18	-7.8	4	15	2.8	4	3.2	9	4.1	159	3.2	5	2.6	29	4.0	7	3.3	5	2.6	32	
II	1010.0	15.5	0.4	1.8	0.9	0.8		-1.6	11.2	7	-10.2	23	12	3.1	0	-	3	5.3	24	4.3	7	2.7	5	4.6	1	4.0	5	5.0	32	
III	06.1	09.6	-0.4	2.5	0.8	0.7		-1.5	5.6	10	-7.8	31	11	3.6	0	-	4	5.0	10	3.4	7	2.4	6	1.7	6	3.3	42			
IV	09.9	13.4	3.4	6.8	4.8	4.3		1.5	12.4	20	5.3	1	15	3.4	1	3.0	75	5.0	129	4.2	6	3.0	1	2.0	4	2.2	10	2.4	33	
V	12.7	16.2	6.4	10.3	8.4	7.4		4.4	18.2	27	-0.8	6	413	2.9	43	2.8	89	4.2	9	3.2	2	2.5	15	3.0	5	2.0	5	2.0	16	
VI	05.1	08.5	10.4	15.0	13.5	11.8		8.5	21.2	27	-4.1	4	11	2.5	1	4.0	3	2.7	5	3.2	59	2.5	69	2.0	1	1.0	15	2.1	48	
VII	09.0	12.4	13.3	19.2	17.1	15.2		11.5	24.0	8	7.2	25	18	2.2	3	2.7	0	-	6	3.7	19	3.0	23	1.4	49	1.7	95	1.8	48	
VIII	09.3	12.7	13.0	18.2	15.4	14.4		11.1	30.2	24	7.2	22	16	2.5	5	2.4	0	-	6	4.5	8	2.8	5	3.3	3	2.0	2	3.5	50	
IX	07.3	10.7	10.1	13.5	11.4	11.1		8.6	19.4	16	4.2	27	6	2.7	0	-	0	-	119	3.4	8	3.1	15	2.7	4	2.0	8	2.9	51	
X	06.2	09.6	8.5	10.5	9.3	9.1		6.5	17.2	13	0.0	21	10	2.4	1	4.0	4	4.0	28	3.5	16	3.2	0	-	1	1.0	2	3.5	31	
XI	00.6	04.1	3.0	4.2	3.7	3.5		1.2	14.9	13	-4.4	6	2.7	0	-	123	3.9	30	3.7	123	3.5	0	-	0	-	1	2.0	20		
XII	05.3	08.8	5.6	4.2	3.7	3.7		1.1	11.8	1	-3.7	17	2	3.0	1	4.0	5	4.4	369	3.6	243	2.9	3	4.7	2	3.0	7	2.3	12	
1944	1006.6	1010.0	6.1	9.0	7.6	7.0		4.2	30.2	-10.2	1613	2.8	209	3.0	263	3.9	202	3.7	103	2.9	273	3.2	389	2.2	733	2.5	415			

Runde

$\Theta = 62^\circ 24' N$

2 - 5° E

$$\Delta G = \pm 1^{\circ}$$

I			3.6	4.1	3.9	*3.8		1.9	9.7	16	-3.3	10	43	4.3	1	5.5	2	1.8	9	3.1	
II			2.4	3.2	2.7	2.6		0.9	7.0	1	-3.8	27	63	4.3	8	4.4	4	1.8	23	3.2	
III			1.9	3.7	2.8	2.6		0.6	7.2	27	-3.4	31	63	4.7	129	3.8	43	2.4	59	2.0	
IV			4.6	5.9	5.2	4.7		2.9	10.7	20	-1.5	1	5	4.2	13	4.7	133	2.6	63	3.0	
V			6.8	7.9	6.9	6.6		4.8	13.1	8	-1.0	22	8	3.8	205	5.4	9	2.6	2	3.3	
VI			13.8	12.1	10.9	10.7		6.9	16.5	6	-5.5	4	101	2.3	205	2.4	133	1.8	1	1.0	
VII			14.0	15.8	14.0	13.9		11.8	25.1	5	-2.5	23	35	2.7	413	3.5	18	1.8	15	2.0	
VIII			15.4	14.5	15.0	15.1		11.3	20.4	24	-8.5	30	5	2.0	143	3.5	43	1.8	73	2.5	
IX			10.8	12.0	11.0	11.0		9.3	17.4	15	-5.0	28	63	3.5	203	4.8	4	1.9	6	3.1	
X			9.0	10.4	9.4	9.5		7.8	16.1	12	-2.7	31	2	3.0	43	3.0	113	1.6	73	2.5	
XI			4.3	5.2	4.5	4.6		2.6	10.3	13	-0.5	18	43	3.9	10	4.0	113	1.7	22	2.0	
XII			3.7	4.2	4.1	3.9		2.1	9.4	1	-2.9	17	63	6.0	0	-	133	1.2	193	1.5	
1944					7.1	8.2	7.4	7.2		5.4	25.1	-3.8		63	3.5	173	4.0	1093	1.9	903	2.3
																		116	3.2	230	1.1
																		127	3.1	643	4.4
																		102			

Orsta

$$\Phi = 62^\circ \text{ to } N$$

$$\lambda = 6^\circ \text{ } 7' \text{ E}$$

$\Delta G = \pm 1^{\circ}$

I			1.4	2.1	1.4	1.5		-1.9	9.4	16	-13.3	10	0	-	13	1.7	83	2.5	6	1.7	11	2.2	8	2.2	24	3.5	4	1.2	30
II			0.2	2.5	0.9	0.9		-2.3	6.2	1	-14.3	28	2	2.5	1	2.0	15	2.4	2	4.0	5	2.8	10	2.3	10	2.5	9	2.0	35
III			-0.4	3.7	0.7	0.8		-2.7	7.4	25	-11.4	31	2	2.5	6	1.8	12	2.2	0	-0.9	2.0	23	3.2	20	2.2	5	2.6	45	
IV			3.3	6.2	4.3	3.7		0.4	11.3	20	-8.0	1	1	2.0	16	2.2	19	1.9	3	4.0	2	2.0	7	2.1	16	2.2	0	-26	
V			7.2	10.3	8.6	7.5		3.6	16.5	28	-2.9	6	3	3.7	7	2.0	12	2.1	4	2.0	4	1.5	15	1.9	12	2.2	15	2.3	21
VI			11.7	14.9	13.0	11.8		7.8	20.4	8	2.6	24	39	2.9	23	1.2	2	2.0	6	2.5	0	-	25	2.0	33	2.1	7	3.1	13
VII			15.8	19.4	17.6	16.0		11.4	25.9	5	3.5	25	4	3.5	3	1.9	73	1.5	13	2.5	43	1.4	31	2.1	173	2.0	2	3.0	22
VIII			15.5	16.7	14.7	13.7		9.6	27.8	24	4.2	22	0	-	11	1.6	17	1.4	1	1.0	3	2.0	16	2.1	153	1.6	0	3.0	19
IX			9.4	13.4	11.0	10.6		7.2	19.1	16	2.6	28	0	-	1	2.0	8	1.1	1	2.0	22	1.8	7	1.1	15	1.5	4	2.2	32
X			6.8	9.8	7.5	7.7		4.7	15.8	13	-1.3	21	0	-	5	1.4	12	1.6	12	2.5	11	2.1	11	1.9	113	2.0	43	2.1	21
XI			1.3	2.8	1.5	1.7		-1.3	7.7	23	-7.4	18	0	-	1	0.1	24	2.0	0	-	11	3.5	9	2.7	10	2.8	3	2.0	21
XII			1.4	2.6	1.6	1.8		-0.9	10.1	18	-8.3	17	0	-	15	1.7	10	1.7	6	2.7	16	2.6	6	2.7	11	2.7	8	2.8	21
1944			6.0	8.7	6.9	6.5		3.0	27.8	-14.5		153	3.0	70	1.8	145	1.9	423	2.5	95	2.3	145	2.1	203	2.2	62	2.4	317	



1944

## Ona

 $\varphi = 62^\circ 52' N$  $\lambda = 6^\circ 55' E$  $g = 9.821$  $\Delta G = + 1^h$ 

Monat	Mittlerer Luftdruck P <sub>m</sub> Hectopascals	Mittel. Luftdruck P <sub>0.8</sub>	Mittlere Lufttemperatur T <sub>m</sub>				Lufttemperatur T				Windverteilung nD, F <sub>n</sub>																		
			8	14	19	Dies	Max	Min	Max	Dat	Min	Dat	N	NE	E	SE	S	SW	W	NW	C								
I	997.3	999.1	3.6	4.0	4.0	3.8	5.9	1.7	9.1	15	-2.5	10	6	5.1	1	5.0	0	-	7	3.2	133	3.5	333	6.1	213	6.4	103	5.8	0
II	1010.2	1012.0	3.0	3.2	3.0	3.0	5.0	1.2	7.3	1	-4.6	27	73	5.5	43	4.6	1	1.0	13	2.3	223	4.1	22	4.9	133	4.0	113	5.2	3
III	106.8	108.6	2.3	3.1	2.6	2.5	4.4	0.7	7.9	26	3.6	30	9	4.3	79	4.1	4	2.1	173	2.7	19	5.2	12	5.8	12	5.2	11	5.2	3
IV	11.2	13.0	4.3	4.9	4.8	4.3	6.3	2.7	10.5	19	-0.1	3	5	4.5	143	4.1	113	3.6	63	2.9	12	2.2	133	4.4	19	4.6	7	3.9	1
V	14.8	16.7	6.3	6.9	6.5	6.2	8.1	4.8	13.5	8	0.9	22	133	3.9	243	5.3	7	3.6	13	1.7	53	2.9	7	4.9	20	4.0	12	3.9	2
VI	07.2	09.0	10.3	11.0	10.7	10.3	12.2	9.1	16.0	8	6.4	4	93	5.4	243	3.5	9	3.4	23	5.0	2	2.0	2	3.8	24	3.6	113	3.4	5
VII	11.8	13.5	12.0	12.7	12.5	12.1	13.7	11.1	18.1	10	8.5	25	83	1.9	493	3.7	143	3.7	3	1.8	03	2.0	1	1.0	5	3.2	5	1.4	6
VIII	11.1	12.9	12.4	13.4	12.8	12.5	14.7	11.2	19.1	24	9.5	22	4	3.0	14	4.3	7	2.9	43	2.2	5	2.4	213	4.3	23	4.4	10	3.3	4
IX	06.8	10.6	10.6	11.1	10.8	10.6	12.1	9.5	16.1	22	6.5	28	63	4.1	183	5.5	5	4.2	12	2.3	9	1.8	123	4.0	163	4.8	7	3.7	3
X	06.7	08.4	9.3	10.1	9.6	9.6	11.3	8.0	16.6	13	3.0	31	5	3.5	83	4.2	14	4.1	123	3.1	20	3.5	143	5.7	153	6.7	6	4.2	7
XI	00.4	02.2	4.6	5.6	5.1	5.1	6.8	3.3	11.3	13	0.3	18	5	4.5	83	4.2	14	4.1	123	3.1	21	5.6	23	6.8	6	4.9	1	4.9	2
XII	04.8	06.6	4.2	4.8	4.6	4.4	6.3	2.8	10.0	2	-1.7	31	33	5.9	1	4.0	5	3.4	24	3.3	15	2.6	233	5.2	12	7.3	7	6.5	2
1944	1007.6	1009.4	6.9	7.6	7.2	7.0	8.9	5.5	19.1	-	-4.6		813	4.0	170	4.3	863	3.4	1013	2.8	135	3.0	191	5.1	192	5.0	105	4.4	35

## Molde

 $\varphi = 60^\circ 44' N$  $\lambda = 7^\circ 10' E$  $g =$  $\Delta G = + 1^h$ 

Monat																															
I																															
II	0.0	1.7	0.5	0.4	3.6	-2.2	7.2	1	-9.2	20	0	-	14	1.1	26	1.2	1	1.0	2	1.5	33	2.0	11	2.0	0	-	0				
III	0.3	2.5	0.6	0.8	3.8	-2.0	8.2	26	-11.2	31	0	-	13	1.0	32	1.1	0	-	1	2.5	41	2.0	6	2.8	0	-	0				
IV	2.5	5.5	3.7	3.1	6.9	0.3	13.6	20	-7.0	1	0	-	23	1.2	353	1.2	13	1.0	33	1.7	203	1.9	6	2.2	0	-	0				
V	6.0	8.6	7.4	6.2	10.2	2.9	15.4	27	-3.0	6	0	-	223	1.6	41	1.4	03	1.0	15	1.0	213	2.3	5	2	0	-	0	-1			
VI	11.1	14.0	12.8	11.5	16.0	7.9	21.0	27	-2.5	1	0	-	133	1.5	283	1.3	2	1.0	33	1.1	343	1.7	7	2.2	1	3.0	0				
VII	14.7	18.7	17.4	15.4	20.6	11.0	26.6	8	4.0	25	1	1.0	-	20	1.6	34	1.4	2	1.0	23	1.4	25	2.0	1	2.0	0					
VIII	13.0	16.1	14.4	13.3	18.1	9.9	25.6	3	6.2	22	0	-	20	1.2	353	1.3	23	1.2	43	1.2	27	1.9	33	2.4	0	-	0				
IX	9.3	12.6	10.5	10.2	14.1	7.2	19.0	21	-2.0	27	0	-	28	1.4	313	1.3	03	1.0	19	1.0	25	2.2	33	3.1	0	-	0				
X	6.3	9.9	7.0	7.4	11.3	4.5	17.2	13	-0.2	21	0	-	263	1.2	423	1.2	2	1.8	03	4.0	203	2.2	1	3.0	0	-	0				
XI	1.5	4.0	2.0	2.3	5.4	-1.0	13.4	13	-7.0	23	1	0	-	293	1.2	363	1.3	03	0	2.5	03	3.0	183	2.4	3	2.8	0	-	0		
XII	1.5	2.7	1.7	1.8	4.6	-0.8	10.2	2	-7.2	17	0	-	253	1.1	353	1.2	03	1.0	3	2.3	223	2.3	63	3.1	0	-	0				
1944																															

## Gjermundnes

 $\varphi = 62^\circ 57' N$  $\lambda = 7^\circ 10' E$  $g =$  $\Delta G = + 1^h$ 

Monat																													
I																													
II	0.6	2.0	1.0	1.0	3.9	-1.5	9.0	27	-17.4	28	0	-	0	-	113	1.2	93	1.3	7	2.0	3	1.7	6	1.7	2	1.5	48		
III	0.3	2.1	0.6	0.7	4.0	-1.8	9.1	9	-10.1	31	0	-	13	1.7	5	1.2	43	1.4	0	2	3.5	5	1.8	10	1.7	20	55		
IV	3.3	5.1	4.1	3.4	6.8	0.6	15.0	20	-5.7	4	3	2.8	53	2.2	15	1.4	9	1.2	25	1.4	153	2.5	5	2.3	2	2.0	10		
V	6.2	8.0	6.9	6.0	9.8	3.1	17.1	27	-3.6	6	113	3.0	14	2.8	153	1.9	33	1.3	113	1.5	23	75	1.7	43	1.9	12	35		
VI	10.9	12.8	11.8	10.7	14.6	7.8	20.0	7	-2.5	4	9	2.3	4	2.0	123	2.0	10	1.4	143	1.7	10	2.0	8	2.6	8	2.6	11	2.8	
VII	14.4	17.0	15.4	14.5	18.9	11.5	26.5	8	4.9	25	59	3.7	13	2.8	33	1.4	15	1.3	39	1.0	63	1.9	17	2.1	313	1.9	11	2.1	11
VIII	12.9	15.2	13.8</td																										

## Jahresübersichten

194

$$H_s = 12 \quad H_b = 14.6 \quad h_0 = 1.8 \quad h_0 = 6 \quad H_M = \quad h_r = 1.1$$

$$H_1 = 50 \quad H_2 = \dots \quad H_3 = 1.9 \quad H_4 = \dots \quad H_5 = 17.3 \quad H_6 = 1.7$$

I	80	80	79	80	8.3	8.3	9.2	276	35	7	15	0	0	25	25	10	2	1	15	16	5	0	0	0	0	6	0	20	22					
II	80	75	82	80	7.7	8.2	8.1	140	19	8	20	1	0	0	17	16	12	1	1	10	11	1	0	0	0	0	9	0	19	22				
III	84	73	79	80	5.7	7.8	7.8	194	26	4	21	0	0	0	23	21	7	8	0	12	20	5	0	0	0	0	16	0	31	31				
IV	80	68	74	78	7.8	7.4	7.6	141	22	9	9	0	0	0	19	19	5	2	0	15	6	0	0	0	0	15	0	17	18					
V	77	65	63	71	7.6	7.2	7.1	94	18	1	6	0	0	0	18	18	3	2	0	0	17	4	3	1	0	0	19	2	17	0				
VI	77	64	70	77	7.8	7.6	7.4	84	34	16	0	0	0	0	13	13	2	1	0	0	13	0	0	0	0	22	0	13	0					
VII	82	65	71	79	6.8	6.2	5.5	26	11	15	0	0	0	0	6	6	1	0	0	0	6	0	0	0	0	29	0	11	0					
VIII	82	71	77	80	7.1	6.5	6.7	81	18	14	0	0	0	0	12	11	4	3	0	0	12	0	0	0	0	2	0	15	0					
IX	88	73	82	88	8.2	7.6	7.9	114	30	28	0	0	0	0	14	12	3	4	0	0	14	0	0	0	0	0	0	12	0	18	0			
X	78	70	77	76	7.0	7.3	6.8	98	45	2	1	0	0	0	0	12	10	3	4	0	0	12	0	0	0	0	0	0	11	0	11	0		
XI	76	67	73	74	6.3	6.4	5.4	111	10	16	0	0	0	0	14	14	5	4	0	0	9	9	4	0	0	0	0	14	0	3	7			
XII	70	67	70	70	6.9	7.5	6.5	78	16	31	16	2	0	0	0	11	11	4	6	0	0	10	7	5	0	0	0	0	8	0	12	3		
1944	80	70	75	77	7.5	7.3	7.1	1437	45	106	7	3	0	0	184	176	54	52	3	2	145	73	23	3	0	2	0	1	4	0	185	11	170	106

$$H_0 = 51 \quad H_0 = \quad h_0 = 1.0 \quad h_0 = \quad h_0 = 5.6 \quad h_r = 1.4$$

I	77	79	76	78	8.3	7.9	7.1	276	45	6	14	4	0	0	27	23	10	11	4	0	21	18	9	6	0	0	0	1	5	10	1	0	15	18		
II	78	72	78	78	7.9	7.2	7.4	152	32	8	20	4	2	0	0	20	15	4	9	3	0	16	13	6	8	0	0	0	0	5	12	9	2	15	22	
III	80	73	73	73	8.1	7.5	6.2	150	18	3	22	0	0	0	25	18	7	6	0	0	17	21	11	5	0	0	1	2	1	19	12	9	2	15	22	
IV	78	72	76	77	7.9	7.3	7.6	125	21	9	12	0	0	0	22	16	6	2	0	0	20	7	6	6	0	0	1	0	6	8	12	5	16	26		
V	76	71	69	73	7.2	7.1	6.9	84	22	14	7	0	0	0	20	16	2	4	0	0	19	7	3	3	0	0	4	0	3	5	14	4	15	18		
VI	80	73	76	80	7.1	6.7	7.2	93	16	12	0	0	0	21	15	4	0	0	0	21	0	7	0	0	4	0	0	6	0	6	16	0	10	0		
VII	83	75	80	84	5.5	4.8	6.1	43	10	15	0	0	0	13	7	2	2	0	0	13	0	0	0	0	0	0	0	2	4	23	5	7	0			
VIII	85	75	80	82	7.3	6.5	7.2	66	13	16	0	0	0	20	11	3	1	0	0	19	0	0	0	0	0	0	0	10	5	14	3	17	0			
IX	88	76	80	85	6.9	7.3	7.7	105	23	10	0	0	0	20	16	5	3	0	0	20	0	0	0	0	0	0	0	7	1	10	2	18	0			
X	77	69	74	74	6.5	7.2	6.4	63	27	2	1	0	0	0	15	9	2	6	0	0	15	1	0	0	0	0	0	0	3	0	15	1	14	0		
XI	74	70	71	72	5.7	6.1	5.5	99	20	11	16	0	0	0	14	12	5	3	0	0	11	9	5	1	0	0	0	0	0	0	0	0	6	9	10	
XII	69	68	71	70	6.3	6.4	6.1	84	18	28	16	2	0	0	13	10	4	7	1	0	11	7	3	1	2	2	0	0	0	0	0	0	0	4	11	5
1944	79	73	75	77	7.1	6.8	6.8	1320	45	108	8	1	0	230	168	54	56	8	0	203	82	47	41	2	8	0	3	56	64	134	37	164	85			

$$H_1 = 135 \quad H_2 = \quad h_1 = 2.0 \quad h_2 = \quad h_3 = \quad h_4 = 1.6$$

$$H_0 = 51 \quad H_0 = \quad h_0 = 1.8 \quad h_0 = \quad h_0 = 9.7 \quad h_0 = 1.6$$

1944

## Sula Fyr

 $\varphi = 63^\circ 51' N$  $\lambda = 8^\circ 28' E$  $g = 9.822$  $\Delta G = +1^h$ 

Monat	Mittlerer Luftdruck $P_m$	Mittl. Luftdruck Höhenlage $P_a$	Mittlere Lufttemperatur $T_m$				Lufttemperatur $T$						Windverteilung nD, F <sub>m</sub>															
			8	14	19	Dies	Max	Min	Max	Dat	Min	Dat	N	NE	E	SE	S	SW	W	NW	C	1	2	3	4			
			1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24		
I	994.1	997.8	3.1	2.9	3.2	3.0	1.4	8.5	15	-3.7	10	8	4.6	25	2.8	0	-	22	3.8	59	4.0	115	5.4	33	5.7	10	5.7	0
II	1006.9	1010.6	2.6	3.1	2.6	2.7	1.1	6.8	7	-3.8	28	85	4.6	3	4.8	1	3.0	9	2.2	95	3.2	185	4.8	20	5.0	145	4.9	3
III	973.0	973.1	1.6	3.0	2.4	2.1	0.8	7.0	26	-5.3	51	13	5.3	105	3.2	6	3.5	75	2.9	69	3.6	17	4.1	19	4.4	135	4.6	0
IV	953.3	15.0	3.5	4.3	4.0	3.5	2.1	8.0	20	-0.5	1	10	3.0	14	3.8	8	3.1	9	2.9	25	2.5	154	4.0	16	4.2	73	3.7	7
V	12.6	16.4	5.6	6.7	6.1	5.6	4.3	11.0	9	1.9	2	155	3.8	19	3.9	5	4.0	65	2.2	6	2.2	14	3.8	165	4.6	75	4.2	3
VI	55.8	69.4	9.9	11.3	10.4	10.1	8.7	15.7	7	5.1	1	105	2.4	21	3.1	18	4.1	49	3.2	25	3.4	8	4.1	185	4.1	4	3.4	3
VII	10.6	14.2	11.9	13.2	12.1	12.1	11.0	19.3	24	8.6	24	11	1.9	42	2.8	11	2.1	2	2.2	1	2.0	4	1.8	6	2.7	8	1.9	0
VIII	09.2	12.9	11.8	13.1	12.5	12.1	11.1	17.7	24	8.6	31	3	3.0	115	3.1	65	3.0	6	2.1	25	1.8	295	3.6	285	3.9	59	3.5	0
IX	07.1	10.7	9.8	11.3	10.2	10.1	8.6	16.5	20	5.6	28	9	3.2	145	4.8	75	2.7	18	2.3	9	2.3	8	3.1	205	4.0	35	2.7	0
X	04.8	08.4	8.9	9.0	8.6	8.6	7.3	14.0	12	2.6	31	1	3.5	25	2.8	75	3.1	31	2.8	15	2.3	145	5.1	19	4.8	45	4.6	0
XI	999.2	02.9	3.9	4.2	3.8	3.9	2.4	8.0	25	-1.7	22	6	4.5	4	3.2	6	2.8	395	4.2	9	3.9	16	5.3	3	3.3	69	4.2	0
XII	1002.5	06.2	3.3	3.7	3.4	3.5	1.9	7.6	2	-3.1	17	25	5.2	2	1.5	0	-	35	3.2	175	2.8	125	5.4	145	6.1	8	5.8	1
1944	1005.5	1009.2	6.3	7.2	6.6	6.4	5.1	19.3	-5.3	98	3.7	1465	3.4	765	3.2	192	3.2	90	2.9	169	4.3	215	4.6	95	4.3	18		

## Vallorsund

 $\varphi = 63^\circ 51' N$  $\lambda = 9^\circ 44' E$  $g =$  $\Delta G = +1^h$ 

Monat			2.1	1.7	2.0	1.9	0.9	8.0	15	-9.6	4	2	3.0	4	3.2	35	2.0	28	3.6	8	3.1	21	3.4	12	5.6	145	6.5	0	
			1.8	2.2	1.9	1.9	0.0	5.4	24	-8.6	27	4	2	4.0	59	3.4	0.3	1.0	26	3.2	10	2.9	145	3.3	7	4.1	215	4.5	0
			0.4	2.3	1.2	1.0	-1.1	6.8	31	-8.5	31	49	4	4.8	6	3.2	25	2.2	155	1.8	10	2.4	25	3.3	12	4.2	153	4.4	1
IV			2.6	4.8	3.9	3.1	0.6	8.2	20	-5.1	5	75	3.1	13	2.5	65	2.2	15	1.9	115	2.0	125	2.7	13	4.2	8	2.6	3	
V			6.3	7.8	6.8	6.1	3.5	13.7	9	-2.7	5	9	2.8	20	3.4	6	3.5	7	2.1	7	2.3	89	2.8	12	4.5	225	3.4	1	
VI			11.6	13.1	12.2	11.2	8.4	20.1	7	4.2	4	75	2.3	155	2.9	59	1.4	245	3.3	3	1.8	8	2.6	105	3.4	15	3.2	1	
VII			13.5	15.3	14.0	13.4	10.7	23.0	10	5.9	24	135	2.2	40	2.7	1	2.0	11	3.0	3	2.8	1	1.0	115	2.2	8	2.1	4	
VIII			12.5	14.4	13.2	12.4	10.1	20.7	27	7.1	31	5	2.2	10	2.8	59	1.6	7	2.1	49	2.1	185	2.9	225	3.3	10	2.8	10	
IX			9.9	12.5	10.8	10.5	7.7	19.6	19	3.0	5	13	5.7	95	3.1	13	1.9	185	2.6	95	2.5	135	2.9	125	3.1	8	2.8	4	
X			7.9	9.5	8.1	8.2	6.1	14.8	12	2.2	21	1	4.0	1	2.0	39	2.0	445	3.5	9	2.5	135	3.8	85	3.2	8	2.8	4	
XI			2.4	5.2	2.8	2.7	0.5	7.4	6	-2.6	17	39	5.0	0	-	16	3.5	405	3.0	15	2.0	85	2.8	1	4.0	63	3.9	1	
XII			3.1	3.6	2.9	3.1	0.9	9.2	2	-4.5	17	1	6.0	0	3.0	3	2.0	47	3.5	75	2.9	19	4.7	6	5.7	85	5.1	0	
1944			6.2	7.5	6.6	6.3	4.0	23.0	-9.6	38	3.1	125	2.9	75	2.3	284	3.1	96	2.4	165	3.2	125	4.0	146	4.0	29			

## Ørland

 $\varphi = 63^\circ 41' N$  $\lambda = 9^\circ 40' E$  $g =$  $\Delta G = +1^h$ 

Monat			1.7	1.3	2.0	1.6	-0.3	7.8	15	-9.6	4	2	5.2	35	3.0	3	3.5	195	4.7	175	4.7	14	3.8	19	4.5	12	5.6	0
			1.1	1.8	1.4	1.3	-0.6	6.2	1	-7.7	27	35	3.6	29	3.0	2	2.0	185	4.5	185	4.6	8	3.7	155	3.7	189	4.5	0
			0.2	2.0	0.8	0.8	-1.2	7.4	9	-7.4	31	6	4.7	29	3.4	3	2.8	18	3.8	16	3.8	125	3.7	155	4.4	1		
IV			2.5	4.7	3.7	3.1	-1.0	9.0	20	-12.8	1	11	2.0	1	2.0	1	2.5	25	3.3	8	2.3	15	4.2	3				
V			5.8	8.1	7.1	6.2	3.7	13.0	9	-2.6	6	11	4.0	9	3.8	6	3.7	13	3.5	45	4.3	105	3.9	245	4.0	3		
VI			11.1	15.7	12.2	11.5	8.5	20.0	27	3.8	1	115	5.2	35	2.7	4.7	27	4.2	25	2.9	125	3.7	19	3.8	1	1.0	26	
VII			14.1	17.3	15.3	14.5	10.8	22.0	26	5.9	25	135	3.2	65	2.8	3	1.0	115	3.8	65	3.8	8	2.5	125	3.7	1	1.0	26
VIII			12.0	14.9	15.3	12.5	10.1	22.2	3	6.7	31	75	2.1	39	2.9	49	1.4	13	2.5	9	3.8	135	3.2	195	3.5	5		
IX			9.6	12.0	10.1	10.1	7.8	16.2	22	-2.																		

## Jahresübersichten

194

$$H_s = 27 \quad H_b = 30.0 \quad h_c = 2.0 \quad h_a = 5.4 \quad h_d = 12.2 \quad h_r = 1.6$$

Sula Fyr

Monat	Mittlere Relative Feuchte U <sub>m</sub>		Mittlere Bewölkung N <sub>m</sub>		Niederschlag R		Zahl der Tage n																																						
									Lufttemperatur T			Niederschl. R			Windstärke F			Regen		Schnee		Regen- schneie		Nebel		Rauch- grasgrün		Frost- grasgrün		Hagel		Ganzer		Durst		Nebel		Sonne- schneie		Heiter		Bewölkt		Schne- decke	
	8	14	19	Dien.	8	14	19	$\Sigma$	Max	Dad	b	v	$v^0$	$v^{10}$	$v^{20}$	$v^{30}$	$R_{0,1}$	$R_{10}$	$R_{50}$	F5	F50	F500	•	*	+	9	+	Δ	▲	R	=	○	○	○	○	○	○								
I					7.9	8.6	8.3	151	16	30	7	0	0	0	0	26	24	6	21	4	3	20	18	9	3	0	4	0	2	0	0	0	2	0	0	19									
II					9.0	8.7	8.9	86	19	2	7	0	0	0	0	25	19	2	14	3	0	16	10	1	2	0	5	0	0	0	0	0	0	0	0	22									
III					8.6	7.5	8.0	119	16	9	10	0	0	0	0	28	22	4	10	1	1	19	20	10	2	0	2	0	0	0	0	0	0	0	0	17									
IV					7.9	8.1	7.7	89	19	27	1	0	0	0	0	23	18	2	5	0	0	17	8	2	1	0	2	0	0	0	0	0	0	0	0	11									
V					8.7	7.8	7.4	36	7	13	0	0	0	0	0	17	9	0	7	0	0	15	6	0	5	0	1	0	0	0	0	0	0	0	0	18									
VI					7.4	6.8	7.2	30	6	30	0	0	0	0	0	13	11	0	1	0	0	13	0	0	3	0	1	0	0	0	0	0	0	0	0	18									
VII					7.6	7.6	7.8	5	3	24	0	0	0	0	0	4	2	0	0	0	0	4	0	0	3	0	1	0	0	0	0	0	0	0	0	14									
VIII					8.7	8.5	8.2	94	21	16	0	0	0	0	0	15	12	4	8	0	0	15	0	0	3	0	0	0	0	0	0	0	0	0	0	20									
IX					8.5	7.5	8.1	46	8	9	0	0	0	0	0	15	13	0	5	0	0	15	0	0	3	0	0	0	0	0	0	0	0	0	0	15									
X					7.7	8.4	7.1	57	11	7	0	0	0	0	0	15	10	1	9	1	1	15	0	0	3	0	0	0	0	0	0	0	0	0	0	19									
XI					6.5	7.5	5.6	74	24	7	4	0	0	0	0	17	9	2	15	2	2	14	3	0	4	0	0	0	0	0	0	0	0	0	0	9									
XII					6.1	7.4	6.5	82	23	26	4	0	0	0	0	16	12	1	13	5	3	15	4	2	2	0	0	0	0	0	0	0	0	0	0	7									
1944					7.9	7.9	7.6	869	24	33	0	0	0	0	0	214	161	22	108	16	9	178	69	24	30	0	22	0	4	4	15	116	8	205											

$$H_0 = 4 \quad H_0 = \quad H_0 = 2.9 \quad H_0 = \quad H_0 = 7.8 \quad H_0 = 1.4$$

Vallensund

$$H_2 = 12 \quad H_3 = \quad h_2 = 1.9 \quad h_3 = \quad H_4 = 11.1 \quad h_4 = 1.5$$

**Orland**

I				9.0	8.8	8.9	132	19	6	15	0	28	23	5	15	5	1	16	22	6	2	0	0	1	0	24				
II				8.2	8.1	9.0	103	12	1	15	0	23	21	1	9	1	0	17	16	6	2	0	0	1	1	21				
III				7.7	7.4	7.5	156	27	9	20	0	28	23	4	9	2	1	16	20	5	3	0	0	10	3	19				
IV				9.0	8.0	7.8	90	20	27	8	0	24	16	1	3	0	0	17	16	5	3	0	0	1	2	21				
V				8.1	7.7	7.5	60	10	14	3	0	17	12	0	5	0	0	17	4	0	5	0	0	0	1	17				
VI				7.9	6.9	6.8	60	9	10	0	0	18	12	0	3	0	0	18	0	0	3	0	0	0	0	15				
VII				8.7	6.9	6.2	22	12	30	0	0	11	5	1	1	0	0	11	0	0	5	0	0	0	1	15				
VIII				8.5	8.4	7.3	105	17	15	0	0	20	13	4	4	0	0	20	0	0	5	0	0	0	1	20				
IX				85	77	83	83	8.2	7.5	7.1	75	20	9	0	0	19	12	3	3	0	19	0	0	0	0	17				
X				80	75	78	79	7.3	7.8	6.3	85	21	7	0	0	15	12	3	14	3	1	15	0	0	1	13	15			
XI				75	72	74	74	6.3	7.0	4.9	47	14	10	11	0	11	9	1	1	6	3	0	0	0	11	8				
XII				75	72	75	75	6.5	6.9	5.8	66	13	13	9	0	16	11	2	17	6	2	15	7	1	0	0	11			
1944								8.0	7.6	7.1	999	27	81	0	0	230	169	25	97	20	5	187	88	21	38	0	4	0	1	19
																									2	149	23	203		

$$H_3 = 127 \quad H_4 = 133.0 \quad h_3 = 2.0 \quad h_4 = \quad H_5 = 11.2 \quad h_5 = 1.3$$

Trondheim (Voll)

$$H_1 = 197 \quad H_2 = \quad H_3 = 2.0 \quad h_1 = \quad h_2 = \quad h_3 = 1.4$$

Selbu

I	80	79	82	81	8.4	8.3	7.8	76	11	6	26		5	26	15	1	7	0	0	9	21	3	0	0	0	0	0	0	0	3	1	19	31
II	87	75	79	82	8.1	7.7	7.2	88	13	23	24		6	20	17	2	4	0	0	10	17	5	0	0	0	0	0	0	0	5	4	19	29
III	84	74	82	82	8.2	8.0	7.1	126	21	10	23		3	26	18	0	2	0	0	12	23	8	0	0	0	0	0	0	4	4	21	31	
IV	83	65	79	82	7.9	8.1	7.8	44	9	17	18		3	21	12	0	0	0	0	12	15	3	0	0	0	0	0	0	3	3	18	30	
V	74	59	67	74	7.5	7.5	7.5	66	21	15	14		0	15	10	1	0	0	0	9	9	3	0	0	0	0	0	0	0	10	4	20	13
VI	75	59	72	79	7.9	8.2	8.7	110	16	10	0		0	21	17	4	3	0	0	21	0	0	0	0	0	0	0	0	0	0	0	0	0
VII	76	62	70	78	7.5	7.4	7.1	56	18	11	0		0	16	10	1	2	0	0	16	0	0	0	0	0	0	0	0	0	0	0	0	0
VIII	86	62	71	80	8.5	6.4	6.2	96	22	0	0		0	17	11	4	3	0	0	17	0	0	0	0	0	0	0	0	0	0	0	0	0
IX	85	70	80	81	7.7	7.7	7.5	109	20	27	0		0	22	15	3	6	0	0	22	0	0	1	0	0	0	0	0	0	0	0	0	0
X	78	68	75	75	6.5	7.2	6.2	53	12	7	5		0	12	10	2	2	1	0	12	1	1	0	0	0	0	0	0	0	0	0	0	0
XI	78	78	74	78	6.1	6.5	6.5	37	11	11	23		0	11	6	1	5	0	0	3	10	9	2	0	0	0	0	0	0	0	0	0	0
XII	75	75	70	72	74	6.6	6.6	6.0	32	9	30	22		0	12	9	0	6	0	0	5	9	1	0	0	0	0	0	0	0	0	0	0
1944	80	68	76	79	7.5	7.5	7.1	893	22	157			29	219	150	24	47	1	0	148	105	26	9	0	2	0	6	4	3	110	34	202	172

1944

## Nordli

 $\varphi = 64^\circ 28' N$  $\lambda = 13^\circ 35' E$  $g = 9.821$  $\Delta G = + 1^h$ 

Monat	Mittlerer Luftdruck $p_0$ hPa	Mittel. Luftdruck $p_{10}$ hPa	Mittlere Lufttemperatur $T_m$				Lufttemperatur $T$						Windverteilung $nD, F_m$															
			8	14	19	Dies.	Max	Min	Max	Dec	Min	Dec	N	NE	E	SE	S	SW	W	NW	C							
	I	II	III	IV	V	VI	VII	VIII	IX	X	XI	XII	1944															
I	949.8	999.3	-8.2	-7.5	-7.9	-8.1	-13.1	2.8	15	-34.1	10	0	-	4	2.2	11	2.6	3	3.0	0	-	1	1.0	27	3.3	0	-	47
II	61.2	1011.2	-4.6	-3.8	-6.7	-6.0	-11.4	2.5	22	-31.3	27	0	-	1	1.0	11	3.2	6	1.7	2	2.0	1	3.0	29	3.4	0	-	37
III	57.5	07.2	-6.2	-1.2	-5.7	-5.3	-12.3	2.8	9	-30.4	31	2	2.5	6	3.2	22	2.9	2	2.0	2	-	2	1.5	29	3.0	26	2.6	31
IV	63.9	13.5	-2.7	2.6	-1.2	-2.0	-8.4	7.3	20	-27.2	1	1	2.0	3	3.0	13	3.1	0	-	1	3.0	4	2.0	29	2.9	3	2.7	36
V	67.0	16.4	2.6	5.2	3.5	1.6	-4.6	12.2	9	-15.6	6	0	-	0	-	15	3.6	0	-	1	2.0	3	2.5	44	3.0	4	2.5	26
VI	62.7	10.8	7.9	10.9	9.6	7.6	2.3	17.8	29	-3.7	2	0	-	29	4.2	30	3.4	2	1.5	0	-	2	2.5	24	3.0	45	3.1	24
VII	66.5	13.7	13.7	17.4	15.5	13.4	7.4	28.0	10	-0.8	25	3	3.0	5	4.2	17	3.2	3	3.0	3	2.3	3	2.7	32	3.0	2	4.5	25
VIII	65.4	12.9	10.9	14.3	12.5	11.0	6.5	24.0	25	-1.4	31	1	1.0	1	3.0	10	3.0	1	3.0	1	2.0	50	3.2	0	-	26		
IX	64.5	12.8	6.5	9.8	6.8	6.6	1.9	18.3	19	-5.8	5	4	2.2	3	2.7	27	3.2	9	2.8	0	-	2	3.0	21	3.5	4	3.1	20
X	63.1	11.9	2.9	5.3	2.9	3.3	-0.6	10.8	12	-7.1	30	0	-	6	3.2	32	3.3	6	2.8	0	-	1	3.5	24	3.8	0	-	24
XI	58.0	07.5	-4.1	-2.2	-3.1	-3.3	-7.3	2.7	3	-14.5	28	2	3.0	11	3.4	39	3.2	3	3.3	2	1.5	0	-	5	2.8	0	-	28
XII	60.8	10.5	-3.4	-3.2	-3.5	-3.5	-7.0	3.0	2	-16.5	31	1	2.0	3	3.2	34	3.7	29	3.0	0	3.0	6	4.0	16	2.8	0	-	30
1944	961.7	1010.6	1.1	4.0	1.9	1.3	-3.9	28.0	-	-34.1	14	2.4	45	3.2	261	3.2	37	2.6	10	2.2	26	2.7	327	3.2	20	3.0	356	

## Nordseyan

 $\varphi = 64^\circ 48' N$  $\lambda = 10^\circ 33' E$  $g =$  $\Delta G = + 1^h$ 

Monat			2.3	2.2	2.5	2.3	4.0	0.2	7.6	15	-4.7	13	4	5.0	43	4.2	9	3.8	16	5.8	9	4.9	18	5.8	23	5.9	9	5.9	0		
			I	II	III	IV	V	VI	VII	VIII	VIX	X	XI	XII	1944																
			2.7	3.7	3.3	2.8	4.7	1.3	6.8	21	-1.5	1	6	3.0	16	3.9	125	3.2	9	4.2	123	3.2	75	4.2	123	4.5	14	3.4	0		
I			5.3	6.5	5.9	5.5	7.4	4.1	11.7	29	0.4	5	14	4.4	6	3.7	11	2.6	5	3.3	5	4.1	17	3.9	165	3.2	17	3.5	1		
II			9.9	11.2	10.7	10.0	12.6	8.3	16.5	28	4.7	1	9	2.9	17	3.5	26	3.4	43	6.2	2	3.5	8	4.2	13	3.2	105	3.4	1	10	1
III			11.9	13.4	12.7	12.2	14.5	10.5	22.2	10	6.9	25	26	3.4	23	3.2	13	2.9	75	4.0	24	2.0	35	4.0	59	2.7	12	2.3	0		
IV			11.8	13.0	12.3	12.0	14.0	10.8	20.8	25	8.5	30	75	3.5	8	3.8	5	5.3	5	3.3	2	2.0	36	4.5	189	4.0	9	5.6	1		
V			9.9	11.0	10.5	10.1	11.9	8.7	16.7	19	5.4	29	7	3.0	12	4.2	6	3.1	17	3.8	115	3.7	12	3.7	8	2.8	0	-	0		
VI			8.0	8.7	8.4	8.3	9.9	6.8	13.3	13	2.9	31	15	3.3	1	3.5	6	4.0	23	4.6	183	4.8	145	5.2	21	5.0	63	4.7	0	-	0
VII			3.3	3.8	3.5	3.5	4.8	2.1	8.4	5	-2.1	18	2	6.0	0	-	2	1.8	48	3.4	12	2.4	11	3.5	4	4.4	63	5.0	0	-	0
VIII			5.3	5.6	5.4	5.0	6.1	8.9	-2.5	17	3.5	41	0	1.0	65	5.7	32	5.6	163	4.8	14	6.3	5	6.1	14	6.3	5	6.1	1		
IX			6.0	6.8	6.4	6.1	8.0	4.5	22.2	-	-6.0	87	3	3.6	97	3.7	132	3.6	170	4.9	125	4.4	172	4.9	171	4.5	136	4.1	6	1	6

## Leka

 $\varphi = 65^\circ 6' N$  $\lambda = 11^\circ 42' E$  $g =$  $\Delta G = + 1^h$ 

Monat			0.5	0.1	0.5	0.3	-2.7	7.0	15	-11.6	4	7	4.6	0	-	0	-	10	2.9	145	4.1	39	4.0	49	4.0	12	4.3	5				
			0.4	1.3	0.6	0.7	-1.3	4.7	24	-14.8	27	65	4.2	0	-	0	-	10	3.7	95	3.7	29	3.7	4	4.9	225	4.2	5				
			-0.6	0.9	-0.4	-0.4	-3.5	6.2	9	-13.6	31	12	3.3	10	3.2	2	2.2	145	2.8	135	3.5	265	3.8	75	4.2	55	5.1	10				
I			1.8	3.5	2.2	1.7	-1.6	7.5	20	-7.9	1	18	3.5	10	3.2	1	2.0	13	2.5	23	3.8	225	3.0	4	5.6	8	3.7	11				
II			5.8	7.1	6.0	5.4	2.5	13.0	8	-4.7	5	21	3.4	45	2.7	3	2.4	11	2.6	45	3.1	15	3.5	59	5.6	175	2.8	10	-	0		
III			10.6	12.4	11.5	10.5	7.6	18.9	28	-2.9	2	21	2.7	75	2.5	25	3.0	24	3.6	23	3.0	65	4.2	40	5.1	10	5.1	10	-	0		
IV			13.2	14.8	13.4	13.0	10.5	27.4	10	5.5	30	26	3.7	27	0.9	2.0	2.2	145	2.8	135	3.5	265	3.8	75	4.2	55	5.1	10	-	0		
V			12.3	14.0	12.6	12.1	9.7	25.4	25	3.6	21	10	2.2	7	1.8	0.5	2.0	13	2.7	38	3.4	75	4.1	11	3.0	15	3.5	13	-	0		
VI			9.7	11.7	9.7	9.8	7.0	18.8	19	-2.6	6	10	3.5	9	3.3	1	1.5	17	3.7	85	2.8	16	3.0	49	3.8	75	2.7	16	-	0		
VII			7.1	8.5	7.2	7.4	-0.5	14.0	48	-0.7	3	3	3.2	2	4.5	2	4.2	21	4.9	115	4.8	4	4.8	195	3.4	15	3.8	12	-	0		
VIII			1.5	2.6	1.9	1.9	-0.5	9.3	13	-5.6	18	4	5.0	0	-	2	1.8	48	3.4	12	2.4	11	3.5	1	2.0	3	3.0	9	4	4	4.4	16
VIX			2.4	2.5	2.3	2.4	-0.5	8.1	2	-4.8	17	6	5.3	0	-	0	-	40	4.2	12	5.1	20	4.7	4	5.6	7	5.0	4	4	4	4	4
X			5.4	6.6	5.6	5.4	-0.8	25.8	-	-23.5	95	2																				

Jahresübersichten

1944

$H_e = 401$

$H_b = 402.2$

$h_t = 1.9$

$h_a =$

$h_d = 10.1$      $h_r = 1.4$

Nordii

Monat	Mittlere Relative Feuchte $U_m$		Mittlere Bewölkung $N_m$		Niederschlag $R$		Zahl der Tage n																																						
							Lufttemperatur T			Niederschl. R			Windstärke F			Regen		Schne		Regen schne		Neuschne		Nacht graugedeckt		Frühz. graugedeckt		Hagel		Gefrier. gekälte		Dunst		Nebel		Sonne schön		Heiter		Wolkig		Schw.		Schne deckt	
	8	14	19	Dien	8	14	19	Σ	Max	Dec	8	14	19	21	24	27	8	14	19	21	24	27	8	14	19	21	24	27	8	14	19	21	24	27	8	14	19	21	24	27					
I					7.2	7.9	6.5	119	28	15	28	17	24	17	4	7	5	0	0	5	22	1	0	0	0	0	0	1	0	2	13	31													
II					8.7	7.9	6.0	63	10	1	28	15	16	15	1	1	5	0	0	6	15	3	1	0	0	0	0	2	3	14	29														
III					8.8	7.1	7.0	92	12	9	28	18	24	20	1	1	5	0	0	5	22	2	0	0	0	0	0	1	8	2	19	31													
IV					6.5	7.4	7.3	48	10	27	27	8	21	12	1	5	0	0	7	19	4	1	0	0	0	0	1	13	3	15	30														
V					6.7	6.6	6.1	40	7	15	29	9	19	14	0	2	2	0	0	9	12	2	0	0	0	0	0	1	10	6	14	31													
VI					8.1	8.1	7.2	59	14	27	9	18	11	2	2	3	0	0	17	2	1	0	0	0	0	0	1	1	17	3	0														
VII					7.2	7.3	7.3	46	10	14	23	17	10	1	4	4	0	0	19	20	14	1	0	0	0	0	1	2	1	17	3	0													
VIII					8.0	7.7	7.5	121	20	17	1	0	22	13	2	4	0	0	23	0	0	0	0	0	0	0	1	13	9	2	20	0													
IX					7.4	7.7	7.3	64	18	9	10	21	15	13	2	3	3	0	0	20	0	0	0	0	0	0	1	2	8	4	15	0													
X					7.9	7.4	7.1	52	15	7	20	18	15	13	1	3	3	0	0	17	3	1	0	0	0	0	1	1	10	1	17	0													
XI					8.5	9.0	8.0	42	14	26	30	20	18	16	1	2	2	0	0	22	13	8	1	0	0	0	0	1	1	1	1	27	0												
XII					8.0	8.7	8.3	79	12	25	30	23	20	18	1	2	2	0	0	17	5	1	0	0	0	0	1	0	1	1	22	31													
1944								7.7	7.7	7.1	825	29	244	79	244	163	20	60	2	0	134	155	17	1	0	0	0	2	1	15	80	27	201	213											

$H_e = 33$

$H_b =$

$h_t = 2.0$

$h_a =$

$h_d = 14.3$

$h_r = 1.3$

$h_v = 1.6$

Nordcyan

I	E2	81	83	82	7.5	7.8	7.3	93	11	28	14	3	0	0	27	24	1	28	9	3	21	14	7	3	0	1	7	7	0	5	3	15	12	
II	B5	83	80	83	8.1	8.4	8.1	64	15	2	8	24	1	0	25	18	0	20	4	1	19	20	14	8	3	1	12	2	19	1	18	2	7	
III	B1	81	78	80	7.6	7.9	8.0	71	9	4	13	2	0	0	25	18	0	16	5	1	19	20	14	8	3	1	16	2	19	1	18	2	7	
IV	B8	80	74	77	7.9	7.0	6.9	71	13	14	3	0	0	0	21	16	3	10	0	0	15	14	8	3	0	1	10	3	0	25	2	17	0	
V	76	75	74	75	7.8	6.9	7.3	33	7	14	0	0	0	0	17	9	0	11	0	0	17	3	2	0	0	0	1	1	0	25	2	17	0	
VI	77	72	72	72	7.7	7.2	5.9	39	12	13	0	0	0	0	17	7	1	7	0	0	17	17	0	0	0	0	0	1	1	0	25	3	11	0
VII	80	74	76	80	7.9	7.3	6.5	15	4	13	0	0	0	0	11	5	0	0	0	0	11	0	0	0	0	0	0	3	1	1	1	15	0	
VIII	B1	81	78	80	8.1	8.8	8.6	80	23	17	0	0	0	0	23	14	1	12	1	0	23	1	0	0	0	0	0	3	2	1	21	1	0	
IX	77	72	74	75	7.9	7.6	7.6	36	13	27	0	0	0	0	20	15	2	11	0	0	20	0	0	0	0	0	0	1	1	0	16	1	0	
X	73	70	70	71	7.9	8.1	7.0	52	18	7	0	0	0	0	17	14	5	4	2	1	17	1	0	0	0	0	0	1	1	0	18	1	0	
XI	70	66	70	70	6.1	7.1	5.1	39	11	5	3	0	0	0	0	15	9	0	8	4	1	12	8	3	0	0	0	1	1	0	21	3	8	
XII	74	72	72	73	7.3	6.0	6.0	43	8	26	0	0	0	0	17	13	5	14	10	6	16	12	7	4	9	1	0	1	1	0	2	15	3	
1944								7.7	7.6	7.0	1367	45	112	5	234	172	41	119	42	18	192	103	51	28	0	0	11	0	7	45	5	259	15	191

$H_e = 50$

$H_b =$

$h_t = 2.1$

$h_a =$

$h_d =$

$h_r = 1.7$

Leka

I					8.3	8.4	8.0	173	21	16	21	2	0	0	27	25	6	13	4	3	18	20	7	1	0	1	4	0	9	2	24	31						
II					8.8	8.4	8.3	154	20	7	20	4	0	0	24	20	4	12	5	0	16	18	9	4	0	1	5	2	15	1	25							
III					8.2	7.7	7.9	166	45	10	23	2	0	0	25	19	1	13	7	0	11	21	5	2	0	1	6	0	1	21	1	19						
IV					7.2	7.3	7.2	96	18	14	16	0	0	0	16	13	3	7	0	0	11	13	5															

1944

## Austahaug

 $\varphi = 65^\circ 54' N$   $\lambda = 12^\circ 33' E$   $g =$  $\Delta G = +1^h$ 

Monat	Mittlerer Luftdruck P <sub>a</sub> Std. mm Hg	Fest-Luftdruck P <sub>a</sub> , mm Hg	Mittlere Lufttemperatur T <sub>m</sub>				Lufttemperatur T						Windverteilung n.D.F <sub>m</sub>															
			8	14	19	Dies.	Max	Min	Max	Das.	Min	Das.	N	NE	E	SE	S	SW	W	NW	C							
1944			0.1	0.2	0.3	0.2	-2.2	6.9	15	-9.4	10	7	3.7	14	3.4	21	4.0	6	2.7	43	2.4	15	3.7	14	3.7	105	3.6	0
			0.9	1.3	0.8	0.8	-1.7	4.7	24	-9.9	27	8	4.6	13	2.3	19	3.7	3	3.8	2	1.5	11	4.0	9	2.4	22	3.6	0
			-0.8	0.4	-0.2	-0.4	-2.5	6.1	9	-7.9	31	13	2.6	17	3.1	27	3.5	7	2.9	1	3.0	79	3.7	16	2.9	35	4.7	0
			0.7	2.9	2.2	1.4	-1.0	7.2	20	-5.9	1	10	3.9	13	2.2	35	3.0	4	3.1	0	-	13	3.0	1	3.0	1	2.8	1
			5.3	7.0	6.2	5.4	2.9	12.4	10	-1.6	5	18	3.1	7	2.7	27	2.5	0	-	0	-	17	3.7	4	2.8	14	2.7	6
			10.8	12.8	12.1	10.9	7.8	20.2	9	3.5	1	5	2.2	6	1.5	30	2.4	12	3.6	7	3.3	79	2.6	9	2.1	13	2.2	0
			13.7	16.3	13.5	13.9	10.6	23.1	12	6.6	1	28	2.6	24	2.0	16	3.1	8	2.9	0	-	1	1.0	1	2.0	3	3.0	13
			12.0	13.5	12.9	12.0	9.7	22.0	25	6.2	21	10	2.5	10	1.6	6	2.5	5	2.9	0	5.0	16	3.8	31	2.8	125	2.6	1
			10.3	12.3	10.6	10.5	7.8	19.2	19	2.7	3	6	2.9	12	2.4	18	2.8	5	2.8	12	3.6	14	3.2	4	4.4	13	2.4	5
			7.6	8.4	7.8	7.7	5.1	13.9	12	1.4	31	4	3.5	6	2.2	33	3.1	7	3.6	10	3.4	11	3.4	95	3.5	10	3.8	2
			2.3	2.9	2.8	2.6	0.5	7.9	13	-2.3	23	4	4.2	10	3.3	37	3.7	19	4.0	11	3.8	6	5.2	15	6.0	0	-	1
			3.0	5.0	2.5	2.7	0.0	8.5	2	-5.0	17	7	4.4	3	3.0	14	3.6	24	4.4	13	3.7	135	4.0	115	4.4	59	4.5	1
			5.5	6.8	6.1	5.6	3.1	23.1	-	9.9	120	3.2	135	2.5	285	3.2	102	3.6	61	3.4	135	3.6	1115	3.1	119	3.1	30	

## Skälvær

 $\varphi = 63^\circ 52' N$   $\lambda = 12^\circ 11' E$   $g =$  $\Delta G = +1^h$ 

1944		1.2	1.1	1.3	1.2	-0.2	7.4	15	-5.5	10	45	3.7	13	1.0	25	2.8	11	2.9	17	4.4	16	3.2	12	3.3	59	3.6	0
		1.7	2.2	1.7	1.8	-0.5	5.0	13	-6.3	27	5	3.9	25	0	13	2.8	13	2.5	22	3.7	79	3.7	12	2.4	14	3.0	0
		0.2	1.2	0.6	0.5	-0.9	5.9	9	-6.9	30	105	3.5	35	2.1	36	2.8	12	2.9	11	3.7	115	2.0	8	2.3	0	4.0	0
		2.0	3.6	2.8	2.4	0.4	7.6	21	-3.6	1	135	3.0	14	2.0	24	2.2	9	1.9	85	2.8	9	3.5	65	2.8	5	2.0	0
		5.4	7.1	6.0	5.6	3.8	11.8	29	-2.6	5	21	3.1	55	2.5	16	2.3	55	1.7	12	1.8	135	3.4	11	1.8	8	2.3	0
		10.0	12.1	11.0	10.5	8.7	17.5	9	4.3	1	205	2.6	105	1.9	19	3.1	95	2.5	4	2.9	14	3.6	55	2.1	85	1.7	0
		12.5	14.1	12.8	12.6	11.0	19.8	10	6.9	25	465	3.0	105	2.1	9	2.8	3	2.0	12	1.9	29	1.4	45	1.1	35	1.3	1
		11.6	12.9	11.8	11.7	10.3	18.5	27	8.1	21	16	2.5	5	2.2	4	1.9	6	2.1	12	2.0	39	2.5	65	1.4	3	1.5	1
		9.9	11.1	9.9	10.0	8.2	15.2	15	4.3	3	164	3.0	105	2.5	6	1.5	145	2.3	14	1.9	195	2.8	31	2.4	4	1.2	1
		7.8	8.7	8.1	8.1	6.4	12.0	12	2.3	31	1	3.0	3	1.7	13	2.4	19	3.0	22	3.0	165	3.2	12	2.6	6	3.8	0
		5.1	3.6	3.4	3.4	1.9	12.1	15	-1.2	23	5	4.2	5	2.7	42	3.4	105	3.2	19	3.2	65	3.9	59	3.0	0	3.0	3
		5.3	5.5	2.9	5.2	1.1	8.7	2	-4.2	17	7	2.5	23	2.0	265	3.5	155	3.4	18	3.6	65	4.7	6	4.0	8	3.4	0
		5.7	6.8	6.0	5.9	4.2	19.8	-	6.9	167	3.0	72	2.1	235	2.8	129	2.7	173	3.1	166	2.9	86	2.5	665	2.6	3	

## Ytteren i Rana

 $\varphi = 66^\circ 21' N$   $\lambda = 14^\circ 8' E$   $g =$  $\Delta G = +1^h$ 

1944		-5.3	-5.3	-5.4	-5.4	-9.2	7.1	15	-22.8	9	185	1.7	65	1.5	25	3.0	65	2.1	2	2.2	95	3.6	125	2.4	24	2.1	11		
		-4.7	-0.3	-3.3	-2.9	-7.2	9.7	4	-21.8	27	164	1.4	2	1.5	2	2.0	1	1.5	2	2.0	135	2.4	75	2.2	275	1.5	15		
		-4.9	0.7	-1.7	-2.6	-7.8	5.4	7	-18.2	23	21	1.8	135	2.9	11	3.7	6	3.1	3	2.5	10	3.1	75	2.9	18	1.8	3		
		-1.8	2.6	0.4	-1.0	-6.8	6.3	22	-14.3	15	175	1.6	55	2.0	2	2.5	1	2.3	35	2.0	95	2.4	115	1.7	30	2.1	9		
		4.6	6.9	5.5	4.3	-0.1	12.5	10	-9.2	5	145	1.9	8	2.6	1	3.5	3	4.0	55	2.1	145	2.2	15	2.5	285	2.6	3		
		10.5	15.0	12.1	10.6	6.5	19.5	9	0.7	24	13	2.5	65	3.8	35	4.1	12	4.5	215	2.7	9	3.1	75	2.6	15	2.7	2		
		13.8	17.6	15.8	14.1	8.9	25.3	12	0.9	1	21	2.2	5	3.8	45	3.2	12	2.8	345	1.7	4	2.8	45	3.2	13	2.7	15		
		11.9	14.6	12.8	12.0	9.0	23.2	25	-3.7	2	95	1.4	1	1.5	19	2.0	4	1.6	215	1.4	185	2.9	125	2.8	65	1.8	18		
		8.1	11.5	9.1	8.8	5.0	17.8	19	-0.9	6	17	1.6	5	2.1	5	4.0	9	4.2	16	1.9	3	2.5	2	1.8	6	2.4	27	3	
		4.5	6.8	5.2	5.3	-2.5	12.1	15	-4.7	31	295	1.3	65	2.1	3	4.3	45	3.9	115	2.4	45	3.2	5	2.7	145	2.5	14		
		-1.6	-0.3	-0.6	-0.9	-3.8	5.5	3	-11.7	27	203	1.8	9	3.6	95	3.8	8	4.6	55	1.8	35	1.3	35	2.9	95	2.1	21		
		-0.2	0.2	-0.4	-0.2	-3.1	7.4	2	-10.2	17	18	1.1	55	3.7	135	4.6	13	5.0	55	3.4	9	3.5	11	3.4	45	3.1	13		
		2.9	5.7	4.1	3.5	-0.5	23.3	-	-22.8	198	1.6	74	2.8	59	3.8	805	3.7	132	2.0	1085	2.8	100	2.5	197	2.2	149			

## Tonnes i Helgeland

 $\varphi = 66^\circ 31' N$   $\lambda = 13^\circ 1' E$   $g =$  $\Delta$



1944

## Glomfjord

 $\varphi = 66^\circ 40' N$   $\lambda = 13^\circ 59' E$   $g =$   $\Delta G = +1^h$ 

Monat	Mittlerer Luftdruck P <sub>a</sub> mm Hg	Mittel. Luftdruck Parameter P <sub>a</sub> mm Hg	Mittlere Lufttemperatur T <sub>m</sub>				Lufttemperatur T								Windverteilung nD, F <sub>m</sub>																	
			8	14	19	Dies	Max	Min	Max	Dat	Min	Dat		N	NE	E	SE	S	SW	W	NW	C										
I	-	-	0.0	0.3	-0.1	0.1	-2.8	7.8	21	-11.1	4	4	1.5	17	1.2	7	1.4	7	3.9	15	2.3	15	2.6	12	2.2	0	-	16				
II			0.4	1.1	0.7	0.6	-1.9	5.2	13	-12.3	27	5	1.2	8	1.5	1	1.0	8	1.9	9	2.7	11	2.1	7	2.1	3	0	31				
III			-1.1	0.6	-1.1	-0.8	-3.8	5.4	6	-10.2	30	4	1.0	19	1.2	8	1.9	11	2.1	12	2.9	9	2.2	12	2.1	1	1.0	17				
IV			-0.7	2.1	0.4	0.0	-2.9	8.0	22	-7.4	13	4	1.0	22	1.2	13	1.8	0	-	2	1.0	3	2.3	8	2.1	5	1.4	33				
V			4.6	6.5	5.1	4.6	1.8	12.1	27	-4.7	5	11	1.1	7	1.3	10	2.0	5	2.2	5	1.8	9	2.3	13	1.8	3	1.0	30				
VI			9.2	11.2	10.5	9.5	6.7	17.5	9	3.7	1	5	1.0	15	3.1	21	2.3	1	2.0	4	1.8	4	1.5	8	2.3	29						
VII			12.4	14.6	13.7	12.8	10.0	21.1	10	3.9	1	5	1.0	5	1.2	0	-	9	1.9	9	2.8	0	-	6	1.2	7	1.7	54				
VIII			10.9	12.8	11.9	11.2	9.0	19.5	25	5.6	31	5	1.0	2	1.0	0	-	2	2.5	4	2.0	15	1.6	13	1.5	0	-	40				
IX			9.2	10.7	9.4	9.4	7.1	17.7	20	2.1	6	7	1.1	0	-	1	1.0	18	2.6	14	1.6	5	1.0	5	1.6	0	-	35				
X			7.3	7.7	7.2	7.2	5.1	12.7	12	0.1	31	0	-	2	1.0	2	1.0	6	2.1	6	1.5	12	1.8	12	2.0	0	-	31				
XI			1.7	2.4	2.0	2.0	0.0	8.6	13	-4.8	27	3	3.3	2	1.0	19	2.2	23	2.7	9	2.6	0	-	3	1.7	0	-	17				
XII			2.5	2.2	2.1	2.3	0.1	8.4	2	-5.8	17	2	2.0	6	1.3	5	2.0	30	3.8	12	2.7	3	4.0	14	2.2	6	2.0	17				
1944							4.7	6.0	5.2	4.9		2.4	21.1	-12.3		53	1.3	91	1.2	79	2.1	160	2.7	98	2.3	86	2.1	109	1.9	37	2.0	385

## Helligvær

 $\varphi = 67^\circ 24' N$   $\lambda = 13^\circ 54' E$   $g =$   $\Delta G = +1^h$ 

Monat	Mittlerer Luftdruck P <sub>a</sub> mm Hg	Mittel. Luftdruck Parameter P <sub>a</sub> mm Hg	Mittlere Lufttemperatur T <sub>m</sub>				Lufttemperatur T								Windverteilung nD, F <sub>m</sub>																	
			8	14	19	Dies	Max	Min	Max	Dat	Min	Dat		N	NE	E	SE	S	SW	W	NW	C										
I	-	-	1.0	1.1	1.3	1.1	-0.1	0.1	5.2	15	-6.0	27	7	3.9	19	2.0	45	3.2	145	3.9	6	3.2	245	4.0	20	3.8	9	4.7	0			
II			1.8	2.0	1.8	1.8	-0.1	0.1	5.4	9	-6.3	30	8	3.9	5	2.9	25	4.0	255	3.9	5	3.2	6	3.8	11	4.0	95	4.3	4			
III			-0.2	0.8	0.2	0.1	-1.8	5.4	9	-6.3	16	11	3.0	95	2.5	10	2.8	21	2.5	1	1.0	9	3.5	65	3.8	175	3.1	4				
IV			1.2	2.1	1.5	1.2	-0.7	6.4	22	-7.7	13	1	2.5	1	4.0	34	3.1	75	2.5	2.5	8	2.4	18	3.0	9	3.2	85	2.5	3			
V			5.0	6.1	5.3	4.9	3.0	10.1	10	0.0	6	105	3.3	125	3.6	8	3.8	9	3.4	15	2.7	225	4.1	155	3.8	95	2.9	4				
VI			9.5	10.4	9.9	9.5	7.1	14.9	6	4.3	21	11	3.1	16	2.8	22	3.8	9	4.2	2	1.0	6	2.3	105	3.6	95	3.3	4				
VII			12.3	13.7	12.7	12.2	9.6	16.0	25	7.0	22	155	2.9	9	2.4	85	2.0	15	2.0	45	2.5	175	4.5	17	3.6	75	2.4	4				
VIII			11.4	12.4	11.4	11.2	9.1	20.8	25	4.3	16	1	3.0	25	1.8	145	2.7	25	2.4	59	1.9	7	1.7	75	2.1	1	1.9	105	3.5	7		
IX			9.6	10.6	9.2	9.4	7.5	15.6	22	3.5	6	6	2.8	15	3.0	95	3.4	16	2.6	65	2.5	225	3.8	55	2.3	6	2.7	5				
X			7.8	8.1	7.8	7.8	6.2	11.6	18	1.9	31	4	2.9	15	1.7	14	3.4	22	3.1	4	2.6	195	3.9	125	3.0	85	3.7	7				
XI			3.1	3.4	3.2	3.2	-0.4	7.0	2	-3.9	23	5	4.4	6	3.4	33	4.1	275	3.5	59	2.7	1	3.0	95	2.9	1	0.0	0	0	1		
XII			3.0	3.0	2.9	3.0	0.8	8.1	2	-3.9	17	2	3.2	05	1.0	225	5.9	275	3.7	59	3.1	95	5.1	85	4.9	10	3.8	1				
1944							5.5	6.1	5.6	5.4		3.5	22.8	-6.3		1265	3.2	97	2.9	180	3.8	207	3.4	43	2.7	175	3.9	132	3.7	995	3.4	36

## Bodø

 $\varphi = 67^\circ 17' N$   $\lambda = 14^\circ 20' E$   $g = 9.824$   $\Delta G = +1^h$ 

Monat	Mittlerer Luftdruck P <sub>a</sub> mm Hg	Mittel. Luftdruck Parameter P <sub>a</sub> mm Hg	Mittlere Lufttemperatur T <sub>m</sub>				Lufttemperatur T								Windverteilung nD, F <sub>m</sub>															
			8	14	19	Dies	Max	Min	Max	Dat	Min	Dat		N	NE	E	SE	S	SW	W	NW	C								
I	-	-	990.4	994.8	-1.2	-1.5	-0.6	-1.1	-3.4	6.5	15	-10.2	9	05	4.0	2	4.0	42	3.9	12	3.4	7	2.9	195	4.4	75	3.2	0	0	19
II			1002.2	1006.6	-0.2	0.7	0.1	0.1	-2.2	5.1	13	-10.2	27	35	3.6	45	3.9	145	3.5	65	2.9	95	3.4	5	3.4	5	3.6	0	0	3
III			01.0	05.4	-1.7	0.1	-1.5	-1.3	-3.5	5.2	9	-9.6	30	1	1.5	3	3.7	45	3.6	105	3.4	5	3.2	25	3.3	3	2.2	3	2.3	3
IV			07.9	12.3	-0.1	1.9	0.6	0.1	-3.0	7.4	22	-7.7	13	1	2.5	1	4.0	34	3.1	75	2.5	8	2.4	18	3.0	9	3.2	85	2.5	3
V			10.8	15.2	5.0	6.4	3.5	4.8	1.9	11.4	27	-2.6	5	85	3.5	3	2.7	16	3.2	125	3.0	6	2.5	35	3.3	25	2.7	55	3.2	3
VI			06.3	10.6	10.2	11.8	10.9	10.1	7.2	21.1	9	3.2	26	45	2.4	19	2													



1944

## Gratøy

 $\varphi = 67^\circ 50' N$  $\lambda = 14^\circ 47' E$  $g =$  $\Delta G = + 1^h$ 

Monat	Mittlerer Luftdruck $P_m^*$	Mittleres Klimaprinzip $P_m^*$	Mittlere Lufttemperatur $T_m$				Lufttemperatur $T$						Windverteilung $nD, F_m$																
			8	14	19	Dies	Max	Min	Max	Dag	Min	Dag	N	NE	E	SE	S	SW	W	NW	C								
			8	14	19	Dies	Max	Min	Max	Dag	Min	Dag	N	NE	E	SE	S	SW	W	NW	C								
I	0.5	0.5	0.7	0.6	-	-	-1.6	6.6	15	-6.8	8	65	3.7	6	2.5	123	2.2	9	3.2	25	3.7	11	4.4	13	4.4	6	3.0	4	
II	1.3	1.7	1.5	1.2	-	-	-0.8	5.6	15	-6.2	27	5	4.5	10	2.4	2	1.2	4	2.0	31	3.8	155	3.8	109	4.7	35	5.0	4	
III	-0.5	0.9	-0.2	-0.1	-	-	-2.0	5.0	9	-6.2	30	55	3.5	11	2.9	103	2.1	123	3.6	22	3.4	113	3.5	69	3.2	33	4.9	10	
IV	0.9	2.4	1.5	1.0	-	-	-1.3	6.0	27	-5.2	13	113	3.4	155	2.2	6	1.7	45	2.0	145	2.7	7	3.5	159	3.5	81	3.4	7	
V	5.0	5.7	5.2	4.8	-	-	2.7	11.0	9	-1.2	5	95	3.5	19	4.6	4	2.9	8	2.6	145	2.6	25	4.6	7	2.6	4	3.0	2	
VI	10.4	11.4	10.9	10.3	-	-	8.0	16.9	5	4.8	1	18	2.9	14	3.0	5	3.7	16	2.8	55	3.7	85	3.9	155	2.5	45	3.0	3	
VII	15.3	14.1	13.6	13.1	-	-	10.8	22.0	14	6.6	1	18	2.5	31	3.6	1	1.5	155	2.8	6	1.8	7	2.8	65	3.5	5	1.7	4	
VIII	11.5	12.5	12.1	11.5	-	-	9.8	20.0	24	7.5	16	7	3.1	195	3.1	3	3.2	35	3.9	115	2.6	355	4.6	45	3.2	3	2.1	5	
IX	9.7	10.1	9.9	9.5	-	-	7.4	15.8	24	-1.4	6	6	2.0	123	3.6	65	3.7	175	3.9	22	2.7	115	4.7	4	3.0	53	4.0	4	
X	8.1	8.3	7.8	8.0	-	-	6.3	13.6	18	1.8	31	1	1.0	75	1.3	35	2.1	165	3.2	32	3.0	155	3.8	65	3.4	53	4.5	5	
XI	2.8	3.5	3.1	3.1	-	-	1.2	7.5	2	-2.2	27	2	4.7	13	18	2.4	275	2.8	165	3.3	155	3.0	65	4.0	0	2.7	7		
XII	3.0	3.5	3.0	3.2	-	-	1.2	9.6	2	-3.6	17	45	3.7	3	3.0	7	2.8	35	3.4	155	3.2	13	5.0	8	4.4	5	3.2	2	
1944					5.5	6.2	5.7	5.5		3.5	22.0	-6.8	95	3.1	162	3.1	79	2.5	1675	3.1	217	3.2	1665	4.2	95	3.5	545	3.4	58

## Bjørnfjell

 $\varphi = 68^\circ 26' N$  $\lambda = 18^\circ 4' E$  $g =$  $\Delta G = + 1^h$ 

I	-8.3	-8.6	-8.6	-8.5	-	-	-12.4	-2.8	19	-20.5	4	0	-	29	3.0	355	2.7	55	3.8	0	3.0	7	5.1	32	2.3	3	1.7	7		
II	-8.3	-7.5	-7.8	-7.9	-	-	-11.2	-0.7	22	-19.7	4	0	-	55	3.7	35	2.8	0	-	-	155	2.8	215	3.2	1	1.0	9			
III	-9.6	-7.2	-7.9	-8.7	-	-	-12.0	1.0	7	-19.6	27	0	-	0	-	41	2.8	13	3.9	0	-	4	3.5	25	3.2	0	-	10		
IV	-6.6	-4.0	-6.0	-6.3	-	-	-9.6	2.8	22	-20.8	13	0	-	0	-	17	2.4	5	2.4	0	-	15	2.1	35	2.7	0	-	18		
V	-0.6	1.0	-0.1	-0.6	-	-	-3.4	6.2	30	-12.8	4	0	-	0	-	36	2.4	8	2.4	0	-	21	2.3	17	2.8	0	-	11		
VI	7.7	7.7	5.9	5.9	-	-	2.6	15.1	29	-0.9	1	0	-	2	3.5	355	3.1	105	3.0	0	-	22	2.1	14	2.9	0	-	6		
VII	9.8	12.5	11.4	10.2	-	-	6.5	22.5	15	1.7	27	0	-	22	2.2	13	2.7	65	3.0	0	1.5	19	1.9	405	2.5	0	3.0	3		
VIII	7.7	9.4	8.4	7.9	-	-	5.9	17.1	4	1.8	31	0	-	29	1.8	165	2.3	2	2.0	0	-	34	2.3	35	2.8	0	-	3		
IX	4.3	6.6	4.7	4.7	-	-	2.0	11.6	22	-5.8	6	0	-	3	3.2	35	2.2	3	2.5	2	3.2	4	2.4	36	1.7	0	-	7		
X	0.7	1.7	1.2	1.0	-	-	-1.0	7.6	15	-5.8	29	0	1.0	75	1.5	46	2.3	2	2.0	1	3.0	13	1.7	1	1.0	2				
XI	-5.6	-5.0	-5.2	-5.3	-	-	-8.0	1.0	6	-14.8	27	1	4.0	2	2.2	53	2.2	75	4.2	1	5.0	14	1.3	6	1.3	0	-	5		
XII	-5.5	-5.7	-5.9	-5.7	-	-	-8.1	3.2	2	-15.8	18	1	3.0	1	2.0	57	3.0	8	2.9	0	-	75	2.7	17	3.1	1	2.0	0		
1944					-1.3	0.1	-0.8	-1.1		-4.1	22.3	-20.8		25	3.0	275	2.5	429	2.6	72	3.1	5	3.5	176	2.3	298	2.6	7	1.6	81

## Narvik

 $\varphi = 68^\circ 25' N$  $\lambda = 17^\circ 29' E$  $g =$  $\Delta G = + 1^h$ 

I	-2.2	-2.1	-2.0	-2.1	-	-	-5.1	7.4	15	-11.7	11	15	3.3	0	3.0	0	-	135	3.4	165	2.4	335	2.3	26	3.6	13	4.0	0	
II	-1.3	-0.9	-1.4	-1.3	-	-	-4.2	4.4	15	-11.3	27	15	3.5	35	3.6	0	4.0	5	2.7	14	2.5	31	2.3	305	3.5	1	3.5	0	
III	-2.3	-0.1	-2.1	-2.0	-	-	-5.3	5.0	9	-10.0	29	3	3.2	3	2.2	0	-	24	3.1	125	2.5	305	2.2	19	3.4	1	3.0	0	
IV	0.2	2.1	-0.3	-0.2	-	-	-3.8	6.5	22	-10.8	13	85	3.3	12	2.8	0	-	14	2.8	65	2.2	20	2.6	35	3	2.7	0		
V	5.1	6.2	4.7	4.5	-	-	1.5	11.3	10	-5.8	1	85	2.9	135	3.2	65	2.5	17	3.8	3	2.0	10	2.9	255	3.8	9	3.7	0	
VI	10.5	12.0	10.9	10.1	-	-	6.7	18.2	6	2.6	1	65	3.5	135	3.2	35	4.3	14	3.9	2	2.0	12	2.9	255	3.6	43	3.3	0	
VII	13.2	15.6	14.4	13.4	-	-	9.5	24.4	15	4.9	16	27	8	2.4	105	2.5	45	2.7	1	5.0	1	3.0	255	3.8	345	3.1	8	2.8	0
VIII	10.9	12.6	11.2	11.0	-	-	8.8	16.3	4	4.4	16	45	2.4	10	2.6	24	2.4	9	2.2	0	2.0	305	2.7	335	3.8	2	3.6	0	
IX	8.6	10.4	8.8	8.8	-	-	5.9	17.3	26	-0.3	6	3	2.3	105	2.8	2	2.0	20	3.6	95	2.8	305	2.5	14	2.9	0	2.0	0	
X	5.7	7.3	6.1	6.1	-	-	3.2	13.1	18	-0.2	29	0	-	225	1.6	6	1.7	5	2.1	8	2.4	18	3.6	0	-	0	0	0	
XI	0.2	0.9	0.5	0.5	-	-	-2.2	7.6	3	-7.9	23	0	-	2	2.5	0	-	28	3.0	11	2.1	41	2.1	7	2.9	1	3.0	0	
XII	1.3	0.9	0.9	1.0	-	-	-2.1	9.6	2	-6.2	28	15	2.0	85	1.9	9	3.5	405	3.5	115	2.4	345	2.3	165	3.9	1	3.0	0	
1944	1005.6	1008.1	4.5	5.8	4.7	4.6	1.9	25.1	-11.1		7	2.2	2145	2.1	146	2.5	399	3.0	835	2.4	207	3.2	142	2.1	435	1.9	155		

## Skrøva

 $\varphi = 68^\circ 9' N$  $\lambda = 14^\circ 39' E$  $g =$  $\Delta G = + 1^h$

## Jahresübersichten

1944

$$H_1 = 6 \quad H_0 = \quad h_c = 2.1 \quad h_0 = \quad h_M = \quad h_r = 1.5$$

Grey

Monat	Mittlere Relative Feuchte U <sub>m</sub>		Mittlere Bewölkung N <sub>m</sub>		Niederschlag R	Zahl der Tage n																														
						Lufttemperatur T			Niederschl. R			Windstärke F			Regen		Sonne	Ragn. schw.	Nebel	Ragn. grau	Wol.	Gebir.	Dunk.	Nebel	Sonne schw.	Heller	Bewölk.	Schne. decke								
	8	14	19	Dien.	8	14	19	Σ	Max	Dat	8	14	19	25	30	10	15	25	30	8	14	9	*	8	9	+	Δ	R	=	III	○	○	●	■		
I	77	77	74	76	6.0	6.9	6.9	111	13	18	19	26	18	20	25	19	4	15	0	0	14	18	7	0	0	2	0	0	1	0	4	3	10	21		
II	77	78	79	78	6.4	8.5	8.4	109	26	2	18	20	10	25	24	17	2	9	0	0	21	19	14	1	0	0	0	0	0	1	4	0	19	16		
III	75	68	72	72	6.6	6.0	6.6	53	15	10	25	10	10	18	8	1	10	0	0	8	16	4	2	0	0	0	0	0	1	12	5	10	30			
IV	75	71	73	75	5.7	5.5	5.7	35	9	3	26	0	0	0	0	0	0	7	0	0	6	14	1	2	0	0	0	0	0	17	4	6	20			
V	72	69	70	72	6.9	7.0	7.2	61	15	8	4	0	0	0	0	17	12	1	13	1	0	14	4	1	1	0	0	0	0	3	0	15	0	10		
VI	71	68	68	71	5.8	5.7	6.0	54	13	19	0	0	0	0	15	10	2	4	0	0	15	0	0	0	2	0	0	0	0	0	23	7	8	0		
VII	75	75	75	76	5.6	5.8	5.4	21	10	10	0	0	0	0	23	18	5	10	0	0	23	0	0	0	0	0	0	0	0	0	1	21	0	16		
VIII	86	81	79	83	8.0	7.9	7.5	167	26	17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	8	0	16	0		
IX	74	69	73	73	6.4	6.9	7.5	65	28	19	1	0	0	0	20	13	1	10	0	0	20	0	0	1	0	0	0	0	0	0	1	13	1	10		
X	72	75	76	74	7.5	7.8	7.4	107	25	35	0	0	0	0	22	17	2	9	0	0	22	1	1	1	0	0	0	0	0	0	0	0	0	14	0	0
XI	70	68	69	69	5.2	5.8	5.1	20	5	3	13	0	0	0	0	14	7	0	8	0	0	11	5	2	0	0	0	0	0	0	0	14	4	5		
XII	69	70	68	68	5.8	7.0	6.3	108	19	30	11	0	0	0	0	17	13	4	17	1	0	17	9	8	0	0	2	0	0	3	0	0	2	9	5	5
1944	74	72	73	74	6.6	6.7	6.7	911	28	117	0	0	0	0	226	148	23	113	5	0	182	86	38	14	0	4	0	2	9	5	135	28	125	97		

$H_2 = 3.1$      $H_3 =$      $H = 1.3$      $H =$      $H =$      $H = 3.1$

Bjornfjell

$$H_0 = 49 \quad H_0 = \quad H_0 = 1.9 \quad H_0 = \quad H_0 = 9.6 \quad H_0 = 1.8$$

Narvik

$$H_a = 16 \quad H_b = 20.4 \quad h_c = 2.1 \quad h_d = \quad h_g = 14.1 \quad h_r = 1.7$$

## **Offerory**

I	78	74	72	75	7.2	7.7	7.3	102	18	15	23			2	26	18	1	7	1	0	0	9	20	3	1	2	1	0	0	5	20	26		
II	80	81	78	79	8.8	9.3	8.8	119	30	7	18			0	24	19	2	2	0	0	0	12	22	9	1	0	0	0	0	0	8	21	29	
III	71	66	69	70	6.9	6.5	7.3	56	19	9	27			0	14	9	2	2	0	0	0	7	11	5	2	1	0	0	0	0	3	15	31	
IV	70	66	68	70	7.5	6.5	6.2	54	8	27	27			0	16	0	0	1	0	0	5	14	3	1	1	0	0	0	0	0	2	10	27	
V	66	60	70	72	7.8	8.3	7.9	40	11	13	9			0	15	9	1	7	0	0	0	11	2	0	2	0	0	0	0	0	17	22	20	
VI	67	57	65	74	6.6	6.0	6.1	47	16	29	0			0	14	9	1	1	0	0	0	14	0	0	2	0	0	0	0	0	22	26	14	
VII	71	63	70	74	7.5	6.0	6.1	29	15	1	0			0	8	6	1	0	0	0	8	0	0	0	0	0	0	0	0	3	13	0		
VIII	69	55	87	92	9.0	9.3	144	36	18	0			0	24	18	6	6	6	1	0	24	0	0	4	0	0	0	0	0	1	0	26	0	
IX	78	69	78	77	7.5	7.8	7.7	54	21	19	1			0	17	11	1	4	0	0	0	17	1	1	3	0	0	0	0	0	17	9	1	
X	80	78	82	81	8.4	9.5	8.5	127	35	5	0			0	26	19	3	3	0	0	0	26	2	1	0	1	0	0	0	0	9	22	16	
XI	78	74	74	76	6.0	6.3	6.4	17	2	4	17			0	13	8	0	1	0	0	0	10	7	4	0	1	0	0	0	0	15	6	10	
XII	67	69	69	68	8.4	7.9	7.2	111	25	30	18			0	17	14	4	9	1	0	0	11	10	3	0	0	1	0	0	0	0	5	21	14
1944	75	70	74	75	7.6	7.6	7.4	900	38		140			3	212	150	22	45	3	0	154	89	28	17	4	6	1	3	4	2	163	31	208	133

$$H_0 = 11 \quad H_b = \quad h_t = 2.0 \quad h_s = \quad h_d = \quad h_r = 1.7$$

Skrova

I	77	77	75	76	6.9	7.9	6.7	73	9	19	19	18		0	22	15	0	14	3	1	13	16	6	2	0	1	0	2	0	3	4	15	18	
V	85	85	81	83	9.1	9.3	8.9	93	15	8	10	16		0	23	19	3	16	2	0	13	17	5	2	0	1	0	2	0	3	0	23	12	
V	77	75	75	72	7.5	6.6	7.3	45	12	9	21	23		0	18	11	1	7	0	0	13	13	0	0	0	0	0	0	0	0	0	0	0	
V	75	76	76	75	7.1	6.1	6.3	23	9					0	16	5	0	0	0	0	13	13	14	1	0	0	0	0	0	0	0	0	0	0
V	71	69	74	74	7.1	7.8	7.6	29	12	8	1			0	10	6	1	10	1	0	9	1	0	3	0	0	0	0	0	0	0	0	0	0
V	72	69	70	73	5.8	5.3	5.9	44	17	29	0			0	8	7	2	6	1	0	8	0	0	0	0	0	0	0	0	0	0	0	0	0
V	81	71	79	84	7.3	6.6	5.8	4	3	20				0	5	3	0	0	1	1	15	0	0	0	0	0	0	0	0	0	0	0	0	0
V	91	86	91	92	8.8	8.5	9.1	79	16	18	0			0	15	8	4	5	1	1	15	0	0	0	0	0	0	0	0	0	0	0	0	0
X	87	81	89	87	7.4	7.7	8.6	32	14	19	0			0	14	9	1	2	1	0	14	22	0	2	0	0	0	0	0	0	0	0	0	0
X	90	88	89	85	8.3	9.1	8.0	89	14	16	0			0	22	14	7	4	0	0	8	5	3	2	0	0	0	0	0	0	0	0	0	0
X	87	79	81	80	7.1	7.4	6.0	24	10	6	7			0	10	13	0	4	0	0	15	8	5	1	0	0	0	0	0	0	0	0	0	0
X	79	79	81	80	7.6	8.9	8.1	61	10	27	10			0	18	13	0	16	4	1	15	8	5	1	0	0	0	0	0	0	0	0	0	0
1944	81	79	80	81	7.5	7.6	7.4	616	17		22			0	181	117	16	97	14	3	132	75	21	37	0	9	0	0	34	3	176	31	198	80

1944

## Sörvägen

 $\varphi = 67^\circ 54' N$   $\lambda = 13^\circ 2' E$   $g =$   $\Delta G = +1^h$ 

Monat	Mittlerer Luftdruck P <sub>0</sub> Hausdruck P <sub>0,5</sub>	Mittlere Lufttemperatur T <sub>m</sub>				Lufttemperatur T								Windverteilung nD, F <sub>m</sub>															
		8	14	19	Dies	Max	Min	Max	Dat	Min	Dat	N	NE	E	SE	S	SW	W	NW	C									
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19									
1944		1.0	1.2	1.1	1.1	-1.3	7.5	15	-7.9	9	95	2.9	9	1.6	125	3.3	8	4.0	7	4.6	129	4.4	21	4.2	125	3.4	1		
		1.4	1.9	1.4	1.5	-0.6	5.8	13	-9.4	27	5	4.5	6	2.2	0	05	6.0	8	4.8	235	5.0	21	3.3	17	2.8	6			
		-0.4	0.7	-0.1	-0.1	-2.2	6.0	9	-7.2	30	49	1.3	145	2.4	19	2.7	155	4.4	2	6.0	59	4.1	12	2.9	15	2.8	7		
		-0.1	2.1	0.9	0.5	-2.0	5.0	21	-5.5	13	89	2.5	12	2.4	59	2.4	1	3.5	15	1.7	8	2.5	84	3.1	14	1.9	31		
		4.4	5.3	4.6	4.3	2.4	7.8	9	-2.5	6	79	3.1	12	2.5	25	2.0	9	2.4	21	3.8	135	2.6	95	3.3	6				
		9.5	10.6	9.9	9.3	7.1	15.5	8	3.4	1	4	2.1	245	2.4	22	2.3	5	2.4	0	-	59	2.8	12	3.3	4	3.1	13		
		11.6	13.1	13.0	12.0	9.8	22.0	14	5.3	1	155	2.8	15	2.2	275	1.9	0	-	1	1.0	29	2.2	45	2.6	2	3.5	27		
		10.8	11.4	10.9	10.6	9.2	16.0	25	6.4	22	59	1.7	15	1.5	79	1.5	65	2.1	11	3.5	265	2.6	4	2.0	8	2.6	10		
		8.7	10.0	8.7	8.8	7.1	14.5	19	2.1	6	11	2.4	9	1.9	11	45	3.1	11	3.5	23	3.7	6	1.5	79	2.0	7			
		7.0	7.4	7.1	7.1	5.8	10.5	13	0.9	6	19	4.5	2	2.2	6	1.6	8	3.6	5	3.4	22	4.6	265	2.9	11	2.7	11		
		3.5	3.4	3.5	3.4	1.9	7.3	3	-3.6	27	45	2.2	33	2.3	22	3.4	11	3.7	145	4.9	12	4.8	185	4.7	14	4.3	115	3.9	3
		3.1	3.1	2.7	3.0	0.9	8.0	2	-3.2	18	5	3.4	2	1.8	39	2.3	245	4.9	11	4.8	185	4.7	14	4.3	115	3.9	3		
		5.0	5.8	5.3	5.1	3.2	22.0	-	-9.4		82	2.7	1225	2.1	148	2.4	815	4.0	765	3.9	1895	3.9	148	3.2	1185	2.8	131		

## Rost ..

 $\varphi = 67^\circ 30' N$   $\lambda = 12^\circ 4' E$   $g = 9.806$   $\Delta G = +1^h$ 

Monat	Mittlerer Luftdruck P <sub>0</sub> Hausdruck P <sub>0,5</sub>	Mittlere Lufttemperatur T <sub>m</sub>				Lufttemperatur T								Windverteilung nD, F <sub>m</sub>														
		8	14	19	Dies	Max	Min	Max	Dat	Min	Dat	N	NE	E	SE	S	SW	W	NW	C								
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19								
1944		991.8	995.1	2.2	2.4	2.4	2.5	2.3	4.3	0.5	9.3	15	-2.9	9	89	5.6	85	3.4	75	4.7	6	5.8	20	5.2	135	5.4	2	
		1003.9	1005.3	2.4	2.8	2.7	2.5	2.7	4.6	0.5	6.7	13	-6.8	27	6	5.2	2	15	4.3	1	7.0	22	5.8	19	4.5	9		
		03.0	04.4	1.0	1.4	1.0	1.0	0.9	-0.3	7.1	9	-3.8	29	9	5.9	13	3.5	145	3.2	95	4.4	115	5.4	65	3.5	12		
		10.4	11.8	1.9	2.6	1.7	1.8	3.7	0.2	6.9	21	-2.3	12	245	3.2	45	2.6	85	3.0	7	2.9	55	4.3	55	3.5	7		
		12.9	14.2	4.7	5.2	5.1	4.6	6.3	3.3	8.8	13	0.5	6	205	4.6	45	4.3	45	4.8	13	4.3	165	4.2	245	4.4	9	3.7	10
		09.0	10.3	8.5	9.2	8.8	8.4	10.4	7.0	14.7	6	4.7	1	295	4.2	10	3.5	165	3.7	6	2.6	29	3.6	5	5.2	12	4.2	13
		13.7	15.0	10.6	11.3	10.7	10.6	12.2	9.3	17.6	14	6.8	1	245	4.1	9	3.3	13	3.1	3	2.3	25	2.8	4	1.4	3	3.1	3
		06.8	10.1	10.5	10.9	10.5	10.3	12.4	9.3	15.8	25	7.1	22	235	3.7	5	3.8	75	3.0	25	2.9	145	3.6	275	3.9	145	2.9	2.6
		08.7	10.0	8.9	9.4	8.8	8.8	10.4	7.7	13.0	22	4.2	3	165	3.9	4	3.0	10	2.7	65	3.0	165	3.6	21	4.3	8	2.3	65
		05.2	06.5	7.8	8.0	7.9	7.8	9.4	6.5	11.8	14	2.2	5	2	2.8	1	2.0	75	3.1	135	3.7	20	4.6	7	4.2	1	2	4.0
		03.5	04.7	4.5	4.5	4.4	4.4	5.7	2.8	9.3	3	0.2	21	9	6.4	4	3.8	275	3.9	5	5.8	28	5.5	115	4.5	0	1.0	2
		03.8	05.1	3.8	4.0	3.7	3.8	5.7	1.7	8.3	2	-2.8	28	25	6.8	3	4.9	105	4.7	115	5.0	28	5.6	145	5.8	7	6.4	3
		1006.2	1007.5	5.6	6.0	5.6	5.5	7.3	4.0	17.6	-	-6.8		195	4.2	695	3.5	129	3.6	71	4.0	179	5.0	187	4.4	110	4.0	1295

## Skomvaer Fyr

 $\varphi = 67^\circ 25' N$   $\lambda = 11^\circ 53' E$   $g =$   $\Delta G = +1^h$ 

Monat	Mittlerer Luftdruck P <sub>0</sub> Hausdruck P <sub>0,5</sub>	Mittlere Lufttemperatur T <sub>m</sub>				Lufttemperatur T								Windverteilung nD, F <sub>m</sub>												
		8	14	19	Dies	Max	Min	Max	Dat	Min	Dat	N	NE	E	SE	S	SW	W	NW	C						
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19						
1944		2.0	2.4	2.0	2.1	0.0	-0.7	1.0	-1.6	8.3	15	-7.7	9	10	4.7	8	4.0	5	3.6	17	3.7	165	4.6	125	3.4	0
		2.2	2.8	2.3	2.5	0.4	-0.5	5.9	13	-5.8	28	75	4.9	0	6.0	6	4.2	3	3.3	12	4.6	255	4.5	17	3.6	0
		1.0	1.4	0.8	0.9	-0.9	-0.3	5.5	8	-4.1	50	85	3.5	9	3.0	225	2.8	9	3.1	125	4.4	11	2.7	1	2.2	0
		2.2	2.6	1.7	1.9	0.0	-0.2	6.7	21	-2.9	17	165	2.8	15	2.6	155	2.1	6	2.4	10	2.6	9	2.1	12	3.2	0
		5.0	5.5	5.2	4.8	3.2	4.5	7.5	29	0.5	6	9	2.9	165	3.4	65	3.9	13	2.7	135	2.6	8	2.5	1	2.4	0
		9.0	9.3	9.1	8.6	6.9	14.9	7	4.5	3	13	2.5	20	3.1	175	7	15	4	1	6	2.7	105	2.4	115	3.2	0
		10.8	10.9	10.5	10.3	8.7																				

## Jahresübersichten

194

$$H_0 = 8 \quad H_b = 10.8 \quad h_c = 2.0 \quad h_e = 16.3 \quad h_d = 15.6 \quad h_r = 1.6$$

Root

I	89	89	89	7.0	7.2	7.1	126	16	28	12	2	0	0	27	22	2	24	9	2	19	18	9	0	0	0	0	1	0	0	2	11		
II	83	84	84	8.6	8.6	8.7	102	15	7	6	2	0	0	26	21	4	19	3	1	21	12	3	0	0	0	0	1	0	0	1	21		
III	90	91	89	7.7	8.2	8.7	90	18	9	16	2	0	0	25	21	1	10	3	0	13	21	9	0	0	0	0	2	0	0	19	18		
IV	82	83	84	7.1	6.6	7.1	44	9	21	13	0	0	0	27	9	0	4	0	8	22	1	0	0	0	0	0	0	2	0	13			
V	73	75	75	74	7.8	7.5	8.2	28	6	28	0	0	0	0	19	6	0	8	1	0	16	4	0	0	0	2	0	0	8	0	24		
VI	77	75	73	77	6.8	6.5	6.2	49	18	30	0	0	0	0	15	8	1	5	0	0	15	0	0	0	0	0	0	3	1	0	3	11	
VII	81	83	82	9.1	7.3	8.2	30	22	12	0	0	0	0	15	13	1	1	1	0	0	15	0	0	0	0	0	0	3	4	0	4	17	
VIII	89	85	88	89	8.7	8.2	8.1	91	17	23	0	0	0	0	26	13	4	5	1	0	26	0	0	0	0	0	0	3	4	0	4	20	
IX	81	80	82	81	7.5	7.1	7.3	52	10	27	0	0	0	0	21	12	0	6	1	1	21	0	0	0	0	0	0	5	2	0	0	12	
X	78	78	79	8.2	8.9	7.3	102	20	7	0	0	0	0	28	18	3	13	1	0	28	1	0	0	0	0	0	2	0	0	15	15		
XI	70	71	71	70	7.6	7.8	7.3	63	15	7	0	0	0	0	16	11	1	16	1	1	13	7	4	0	0	0	0	2	0	0	9	17	
XII	77	75	77	77	7.2	8.7	7.3	106	16	4	7	0	0	0	21	19	2	23	8	3	18	10	4	0	0	0	1	0	0	9	0	11	
1944	74	80	81	81	7.8	7.7	7.6	883	22	54	6	0	0	0	266	152	19	134	30	8	213	95	30	7	0	2	0	0	28	11	168	8	180

$$H_0 = 13 \quad H_b = \quad h_0 = 2.3 \quad h_0 = \quad h_M = \quad h_r = 1.5$$

Skomvær Fyr

$$H_0 = 4 \quad H_0 = \quad H_0 = 1.7 \quad H_0 = \quad H_0 = \quad H_0 = 1.8$$

**Eggum**

I	78	77	80	79	6.6	8.1	6.7	207	23	28	18	6	0	0	28	27	8	13	0	0	14	22	8	0	0	0	0	0	0	8	4	16	26	
II	82	84	83	89	8.9	8.3	8.7	101	16	7	13	3	0	0	26	21	3	15	0	0	22	18	9	0	0	0	1	0	0	0	1	21	15	
III	75	74	75	75	6.6	6.8	7.2	90	23	8	5	8	0	0	24	14	4	4	0	0	17	20	13	0	0	0	0	0	0	9	5	15	15	
IV	82	75	78	81	6.9	5.9	7.1	56	10 <sup>a</sup>	7 <sup>b</sup>	26	0	0	23	13	1	3	0	0	8	20	4	0	0	0	1	0	0	0	2	3	12	28	
V	76	74	75	77	8.2	7.7	7.8	57	17	28	4	0	0	0	19	10	1	3	0	0	16	3	0	0	0	0	0	0	0	8	1	20	9	
VI	78	75	78	80	6.0	5.5	5.9	106	49	29	0	0	0	0	14	10	3	3	0	0	14	0	0	0	0	0	0	0	18	7	12	0		
VII	84	83	84	86	8.6	7.6	7.0	42	10	20	20	0	0	0	16	8	0	0	0	0	16	0	0	0	0	0	0	0	18	0	18	0		
VIII	88	87	86	86	8.9	8.3	8.9	89	15	23	0	0	0	0	25	18	2	9	0	0	25	0	0	0	0	0	0	0	14	8	0	24	0	
IX	80	78	81	80	6.8	6.9	7.2	90	36	29	0	0	0	0	22	12	2	4	0	0	22	2	2	0	0	0	0	0	10	0	0	13	0	
X	80	79	80	80	6.5	8.5	7.7	175	34	31	0	0	0	0	25	21	6	6	0	0	23	1	1	0	0	0	0	0	10	0	0	18	0	
XI	73	74	74	73	7.0	5.3	5.3	81	19	6	6	0	0	0	20	11	3	6	0	0	18	15	13	0	0	0	1	0	0	1	4	11	10	
XII	72	72	72	72	6.4	8.8	6.6	160	26	1	10	1	0	0	22	17	7	10	0	0	18	11	6	0	0	0	1	0	0	0	2	14	9	
1944	71	78	79	79	7.5	7.4	7.2	1254	49	102	18	0	0	0	264	182	40	76	0	0	215	112	56	0	0	6	0	2	2	0	70	27	195	127

$$H_0 = 5 \quad H_0 = 7.0 \quad h_0 = 1.9 \quad h_0 = 10.9 \quad h_0 = 10.2 \quad h_r = 1.7$$

Andenes

I	76	76	76	76	6.8	7.7	7.6	87	12	10	22	7	0	0	0	24	19	1	15	4	2	11	19	6	0	0	0	3	3	16	19					
II	80	79	80	80	6.8	8.7	8.4	52	7	21	16	3	0	0	0	21	16	0	13	0	0	9	17	5	1	0	0	8	8	21	18					
III	74	69	68	71	6.6	6.3	6.6	56	12	10	28	10	0	0	0	19	14	1	7	0	0	6	16	3	1	0	0	22	3	12	30					
IV	78	77	78	80	7.0	7.0	6.9	103	22	15	24	1	0	0	0	24	20	3	7	0	0	5	21	2	1	0	0	20	2	15	30					
V	71	68	72	74	7.2	7.3	7.5	43	9	29	5	0	0	0	0	17	11	0	9	1	1	16	4	3	1	0	0	0	0	0	23	1	16	8		
VI	75	74	75	76	5.9	5.7	5.5	62	26	29	0	0	0	0	0	11	9	1	3	1	0	11	0	3	0	0	0	0	0	0	25	2	11	8		
VII	77	81	80	79	7.9	7.0	6.6	28	9	25	0	0	0	0	0	14	5	0	1	0	0	14	0	2	0	0	0	0	0	0	21	2	17	0		
VIII	80	78	78	79	9.3	8.7	8.8	72	7	12	0	0	0	0	0	26	17	0	9	4	0	26	0	0	6	0	0	0	0	0	0	15	0	23	0	
IX	68	64	66	67	7.5	7.6	7.4	51	11	5	0	0	0	0	0	17	11	1	5	1	1	17	2	2	0	0	0	0	0	0	17	0	15	0		
X	79	77	80	79	8.5	8.5	7.9	81	12	10	0	0	0	0	0	22	13	3	7	0	0	11	7	3	0	0	0	0	0	0	1	0	21	0		
XI	72	73	72	58	7.8	7.1	6.2	32	5	1	12	0	0	0	0	15	11	0	3	0	0	11	7	6	3	0	0	0	0	0	8	0	11	9		
XII	69	71	70	69	6.7	8.2	7.2	59	14	30	14	2	0	0	0	14	10	2	14	4	2	11	6	3	0	0	0	0	0	0	0	0	0	7		
1944	75	74	75	75	7.4	7.5	7.2	726	26	123	23	0	0	0	0	224	156	12	93	18	7	159	93	20	18	0	0	17	0	1	4	1	173	27	190	120

1944

## Torsvåg

 $\varphi = 70^\circ 15' N$  $\lambda = 19^\circ 30' E$  $g =$  $\Delta G = +1^h$ 

Monat	Mittlerer Luftdruck $F_0^*$ Höhe Lufttemperatur Pole	Mittlere Lufttemperatur $T_m$				Lufttemperatur $T$								Windverteilung nD, F <sub>m</sub>													
		8	14	19	Dies	Max	Min	Max	Dat	Min	Dat	N	NE	E	SE	S	SW	W	NW	C							
I		0.6	0.4	0.4	0.5	-1.3	5.9	19	-6.3	7	7	4.9	25	5.2	59	1.5	6	2.2	345	3.5	115	4.9	16	4.1	10	4.1	0
		1.1	2.4	1.3	1.5	-1.0	5.5	15	-9.4	27	6	4.7	45	4.6	7	4.6	265	3.9	10	4.0	15	4.0	105	4.9	1		
		-0.9	0.3	-0.5	-0.6	-2.3	4.6	9	-4.5	22	3	4.0	6	2.7	145	2.4	20	3.0	24	3.1	6	3.4	95	3.9	7	3.8	3
		-0.2	0.4	-0.2	-0.3	-2.1	6.0	21	-6.3	12	10	3.8	105	3.7	89	3.3	45	2.3	275	2.7	65	4.2	14	4.1	85	4.8	0
		3.8	4.5	4.0	3.7	1.7	10.8	10	-2.8	5	2	3.5	125	2.5	17	4.0	8	3.6	265	3.2	165	4.4	7	3.6	19	3.0	2
		8.4	9.0	8.6	8.2	6.0	15.9	14	3.2	2	3.2	16	3.0	145	4.3	17	2.6	26	2.8	145	4.1	55	2.9	25	2.8	7	
		10.0	11.3	10.8	10.2	8.2	20.2	15	5.2	6	4	1.5	20	1.9	115	3.5	35	5.1	115	1.8	12	3.4	125	2.8	69	2.7	12
		9.6	10.0	9.6	9.4	7.8	15.8	25	4.5	31	1	3.0	7	2.7	65	3.0	1	3.0	225	2.7	17	3.8	265	3.8	65	2.5	5
		8.6	9.9	9.2	8.9	6.9	18.7	20	1.0	6	55	3.2	5	2.6	5	2.6	65	4.5	375	3.4	12	3.7	9	3.6	55	2.4	4

## Loppa

 $\varphi = 70^\circ 20' N$  $\lambda = 21^\circ 20' E$  $g =$  $\Delta G = +1^h$ 

Monat	Mittlerer Luftdruck $F_0^*$ Höhe Lufttemperatur Pole	Mittlere Lufttemperatur $T_m$				Lufttemperatur $T$								Windverteilung nD, F <sub>m</sub>														
		8	14	19	Dies	Max	Min	Max	Dat	Min	Dat	N	NE	E	SE	S	SW	W	NW	C								
I		-0.2	-0.1	0.1	-0.1	-1.9	4.8	19	-6.8	7	75	2.5	1	4.0	115	2.2	23	2.7	155	2.5	185	2.6	8	3.2	5	4.0	3	
		0.2	0.8	0.3	-0.3	-1.7	6.5	13	-9.2	27	25	3.2	85	2.9	8	3.1	115	2.2	22	2.9	185	3.4	10	3.7	6	2.2	0	
		-0.5	0.7	-0.9	-0.4	-2.6	5.4	9	-5.4	25	1	2.0	95	2.0	215	2.8	26	2.3	7	2.0	16	2.7	7	3.0	5	2.5	2	
		0.6	0.8	-0.5	-0.1	-2.5	7.0	22	-6.8	12	65	3.0	13	2.5	2	2.2	4	1.4	18	2.0	265	3.0	8	3.9	3	4.2	9	
		4.7	5.1	3.9	4.1	1.6	11.9	26	-3.5	5	2	1.2	26	2.4	7	1.9	45	2.1	7	2.7	235	3.1	6	2.2	5	3.0	14	
		9.2	9.6	8.8	8.6	6.0	16.3	15	-3.4	11	3	2.3	255	2.0	135	2.6	7	2.9	3	4.7	13	2.8	6	3.5	2	2.0	5	
		11.7	12.1	11.2	11.1	8.3	24.4	15	5.2	6	9	1.5	30	1.5	55	2.5	4	2.5	0	1	1.0	355	2.5	18	2.7	2	2.0	18
		10.8	10.9	9.8	10.1	8.2	15.4	19	5.9	31	1	2.2	115	2.1	5	1.7	05	2.0	0	-	355	2.5	185	2.9	3	2.0	20	
		9.5	10.3	8.6	9.1	6.4	19.9	20	1.2	6	15	1.7	105	1.7	5	1.6	14	2.7	12	2.8	285	2.7	25	3.2	5	1.2	11	
		6.7	7.2	6.4	6.7	4.8	12.9	18	0.7	9	75	2.1	65	1.5	4	1.9	7	1.6	25	2.4	135	2.6	85	3.9	3	1.8	18	

## Alta (Elvebakken)

 $\varphi = 60^\circ 50' N$  $\lambda = 23^\circ 22' E$  $g = 9.806$  $\Delta G = +1^h$ 

Monat	Mittlerer Luftdruck $F_0^*$ Höhe Lufttemperatur Pole	Mittlere Lufttemperatur $T_m$				Lufttemperatur $T$								Windverteilung nD, F <sub>m</sub>														
		8	14	19	Dies	Max	Min	Max	Dat	Min	Dat	N	NE	E	SE	S	SW	W	NW	C								
I	999.0 1003.5 06.6 09.5 14.4 12.0 15.1 08.6 10.8	999.6 1004.1 07.2 10.1 15.0 12.6 15.7 09.2 11.3	-5.2 -4.5 -5.6 -2.7 -1.9 -0.6 -2.7 -0.2 -1.0	-5.4 -3.3 -5.1 -1.7 -1.7 -4.1 -5.0 -2.1 -2.1	-5.6 -4.1 -5.0 -2.1 -2.1 -1.5 -2.1 -0.7 -0.7	-5.4 -4.1 -5.0 -1.7 -1.7 -0.8 -1.5 -0.3 -0.3	-5.6 -4.1 -5.0 -1.7 -1.7 -0.8 -1.5 -0.3 -0.3	-9.5 -7.7 -8.7 -8.7 -7.7 -6.2 -8.7 -5.9 -5.9	3.9 3.8 2.8 2.8 3.9 2.0 2.7 2.2 2.2	15 22 25 25 20 28 27 22 22	-22.1 -18.8 -17.2 -16.7 -16.2 -16.0 -20.2 -16.7 -16.7	9 4 25 4 7 1 1 1 7	6 2.0 1.8 2.0 2.0 1.6 2.0 1.6 1.6	2 2.5 0 1 1 1 1 1 1	0 - 0 1 1 1 1 1 1	0 - 0 1 1 1 1 1 1	0 - 0 1 1 1 1 1 1	56 52 49 49 49 49 49 49 49	1.9 2.1 1.8 1.8 1.8 2.0 1.8 1.8 1.8	0 - - - - - - - -	4 115 115 115 115 115 115 115 115	2.8 3.1 2.9 2.9 2.9 2.9 2.9 2.9 2.9	9 3.1 3.0 3.0 3.0 3.0 3.0 3.0 3.0	16 22 22 22 22 22 22 22 22	2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8	9 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	16 22 22 22 22 22 22 22 22	2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8

## Galten

 $\varphi = 70^\circ 47' N$  $\lambda = 22^\circ 44' E$  $g =$  $\Delta G = +1^h$ 

Monat	Mittlerer Luftdruck $F_0^*$ Höhe Lufttemperatur Pole	Mittlere Lufttemperatur $T_m$				Lufttemperatur $T$								Windverteilung nD, F <sub>m</sub>											
		8	14	19	Dies	Max	Min	Max	Dat	Min	Dat	N	NE	E	SE	S	SW	W	NW	C					
I	-1.0 -1.1 -1.8 -0.7 3.7 8.3 10.4 9.6 8.2 5.9	-1.0 -0.7 -0.5 -0.2 3.1 9.2 11.1 10.5 8.4 6.4	-0.8 -1.0 -1.7 -0.7 3.7 8.6 8.1 10.2 8.1 5.7	-0.9 -0.6 -1.2 -1.2 4.7 17.1 10.5 8.0 8.4 5.7	-0.9 -0.6 -1.2 -1.2 5.1 15.2 10.0 6.6 6.6 5.4	-0.9 -0.6 -1.2 -1.2 5.1 15.2 10.0 6.6 6.6 5.4	-9.5 -7.7 -8.7 -8.7 -7.7 -6.2 -8.7 -6.7 -6.7 -6.7	1																	

Jahresübersichten

1944

$H_a = 22$   $H_b =$   $h_c = 1.9$   $h_d = 4.8$   $h_e =$   $h_r = 1.8$

Torsvag

Monat	Mittlere Relative Feuchte  $U_m$			Mittlere Bewölkung  $N_m$			Niederschlag  $R$			Zahl der Tage  $n$																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																													
									Lufttemperatur  $T$			Niederschl.  $R$			Windstärke  $F$			Regen			Schnee			Regen + Schnee			Niedersch.			Rauregen			Frost			Hagel			Gewitter			Dauer			Nebel			Sonne			Heiter			Bewölkt			Schneedecke																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																														
8	14	19	Dienst	8	14	19	$\Sigma$	Max	Dat	b	v	f	10	20	30	40	50	60	70	80	90	100	110	120	130	140	150	160	170	180	190	200	210	220	230	240	250	260	270	280	290	300	310	320	330	340	350	360	370	380	390	400	410	420	430	440	450	460	470	480	490	500	510	520	530	540	550	560	570	580	590	600	610	620	630	640	650	660	670	680	690	700	710	720	730	740	750	760	770	780	790	800	810	820	830	840	850	860	870	880	890	900	910	920	930	940	950	960	970	980	990	1000	1010	1020	1030	1040	1050	1060	1070	1080	1090	1100	1110	1120	1130	1140	1150	1160	1170	1180	1190	1200	1210	1220	1230	1240	1250	1260	1270	1280	1290	1300	1310	1320	1330	1340	1350	1360	1370	1380	1390	1400	1410	1420	1430	1440	1450	1460	1470	1480	1490	1500	1510	1520	1530	1540	1550	1560	1570	1580	1590	1600	1610	1620	1630	1640	1650	1660	1670	1680	1690	1700	1710	1720	1730	1740	1750	1760	1770	1780	1790	1800	1810	1820	1830	1840	1850	1860	1870	1880	1890	1900	1910	1920	1930	1940	1950	1960	1970	1980	1990	2000	2010	2020	2030	2040	2050	2060	2070	2080	2090	2100	2110	2120	2130	2140	2150	2160	2170	2180	2190	2200	2210	2220	2230	2240	2250	2260	2270	2280	2290	2300	2310	2320	2330	2340	2350	2360	2370	2380	2390	2400	2410	2420	2430	2440	2450	2460	2470	2480	2490	2500	2510	2520	2530	2540	2550	2560	2570	2580	2590	2600	2610	2620	2630	2640	2650	2660	2670	2680	2690	2700	2710	2720	2730	2740	2750	2760	2770	2780	2790	2800	2810	2820	2830	2840	2850	2860	2870	2880	2890	2900	2910	2920	2930	2940	2950	2960	2970	2980	2990	3000	3010	3020	3030	3040	3050	3060	3070	3080	3090	3100	3110	3120	3130	3140	3150	3160	3170	3180	3190	3200	3210	3220	3230	3240	3250	3260	3270	3280	3290	3300	3310	3320	3330	3340	3350	3360	3370	3380	3390	3400	3410	3420	3430	3440	3450	3460	3470	3480	3490	3500	3510	3520	3530	3540	3550	3560	3570	3580	3590	3600	3610	3620	3630	3640	3650	3660	3670	3680	3690	3700	3710	3720	3730	3740	3750	3760	3770	3780	3790	3800	3810	3820	3830	3840	3850	3860	3870	3880	3890	3900	3910	3920	3930	3940	3950	3960	3970	3980	3990	4000	4010	4020	4030	4040	4050	4060	4070	4080	4090	4100	4110	4120	4130	4140	4150	4160	4170	4180	4190	4200	4210	4220	4230	4240	4250	4260	4270	4280	4290	4300	4310	4320	4330	4340	4350	4360	4370	4380	4390	4400	4410	4420	4430	4440	4450	4460	4470	4480	4490	4500	4510	4520	4530	4540	4550	4560	4570	4580	4590	4600	4610	4620	4630	4640	4650	4660	4670	4680	4690	4700	4710	4720	4730	4740	4750	4760	4770	4780	4790	4800	4810	4820	4830	4840	4850	4860	4870	4880	4890	4900	4910	4920	4930	4940	4950	4960	4970	4980	4990	5000	5010	5020	5030	5040	5050	5060	5070	5080	5090	5100	5110	5120	5130	5140	5150	5160	5170	5180	5190	5200	5210	5220	5230	5240	5250	5260	5270	5280	5290	5300	5310	5320	5330	5340	5350	5360	5370	5380	5390	5400	5410	5420	5430	5440	5450	5460	5470	5480	5490	5500	5510	5520	5530	5540	5550	5560	5570	5580	5590	5600	5610	5620	5630	5640	5650	5660	5670	5680	5690	5700	5710	5720	5730	5740	5750	5760	5770	5780	5790	5800	5810	5820	5830	5840	5850	5860	5870	5880	5890	5900	5910	5920	5930	5940	5950	5960	5970	5980	5990	6000	6010	6020	6030	6040	6050	6060	6070	6080	6090	6100	6110	6120	6130	6140	6150	6160	6170	6180	6190	6200	6210	6220	6230	6240	6250	6260	6270	6280	6290	6300	6310	6320	6330	6340	6350	6360	6370	6380	6390	6400	6410	6420	6430	6440	6450	6460	6470	6480	6490	6500	6510	6520	6530	6540	6550	6560	6570	6580	6590	6600	6610	6620	6630	6640	6650	6660	6670	6680	6690	6700	6710	6720	6730	6740	6750	6760	6770	6780	6790	6800	6810	6820	6830	6840	6850	6860	6870	6880	6890	6900	6910	6920	6930	6940	6950	6960	6970	6980	6990	7000	7010	7020	7030	7040	7050	7060	7070	7080	7090	7100	7110	7120	7130	7140	7150	7160	7170	7180	7190	7200	7210	7220	7230	7240	7250	7260	7270	7280	7290	7300	7310	7320	7330	7340	7350	7360	7370	7380	7390	7400	7410	7420	7430	7440	7450	7460	7470	7480	7490	7500	7510	7520	7530	7540	7550	7560	7570	7580	7590	7600	7610	7620	7630	7640	7650	7660	7670	7680	7690	7700	7710	7720	7730	7740	7750	7760	7770	7780	7790	7700	7710	7720	7730	7740	7750	7760	7770	7780	7790	7800	7810	7820	7830	7840	7850	7860	7870	7880	7890	7900	7910	7920	7930	7940	7950	7960	7970	7980	7990	8000	8010	8020	8030	8040	8050	8060	8070	8080	8090	8100	8110	8120	8130	8140	8150	8160	8170	8180	8190	8200	8210	8220	8230	8240	8250	8260	8270	8280	8290	8300	8310	8320	8330	8340	8350	8360	8370	8380	8390	8400	8410	8420	8430	8440	8450	8460	8470	8480	8490	8500	8510	8520	8530	8540	8550	8560	8570	8580	8590	8600	8610	8620	8630	8640	8650	8660	8670	8680	8690	8700	8710	8720	8730	8740	8750	8760	8770	8780	8790	8800	8810	8820	8830	8840	8850	8860	8870	8880	8890	8800	8810	8820	8830	8840	8850	8860	8870	8880	8890	8900	8910	8920	8930	8940	8950	8960	8970	8980	8990	9000	9010	9020	9030	9040	9050	9060	9070	9080	9090	9100	9110	9120	9130	9140	9150	9160	9170	9180	9190	9200	9210	9220	9230	9240	9250	9260	9270	9280	9290	9300	9310	9320	9330	9340	9350	9360	9370	9380	9390	9400	9410	9420	9430	9440	9450	9460	9470	9480	9490	9500	9510	9520	9530	9540	9550	9560	9570	9580	9590	9600	9610	9620	9630	9640	9650	9660	9670	9680	9690	9700	9710	9720	9730	9740	9750	9760	9770	9780	9790	9800	9810	9820	9830	9840	9850	9860	9870	9880	9890	9900	9910	9920	9930	9940	9950	9960	9970	9980	9990	10000	10010	10020	10030	10040	10050	10060	10070	10080	10090	10100	10110	10120	10130	10140	10150	10160	10170	10180	10190	10200	10210	10220	10230	10240	10250	10260	10270	10280	10290	10300	10310	10320	10330	10340	10350	10360	10370	10380	10390	10400	10410	10420	10430	10440	10450	10460	10470	10480	10490	10500	10510	10520	10530	10540	10550	10560	10570	10580	10590	10600	10610	10620	10630	10640	10650	10660	10670	10680	10690	10700	10710	10720	10730	10740	10750	10760	10770	10780	10790	10800	10810	10820	10830	10840	10850	10860	10870	10880	10890	10900	10910	10920	10930	10940	10950	10960	10970	10980	10990	11000	11010	11020	11030	11040	11050	11060	11070	11080	11090	11100	11110	11120	11130	11140	11150	11160	11170	11180	11190	11200	11210	11220	11230	11240	11250	11260	1

1944

## Kistrand

 $\varphi = 70^\circ 27' N$   $\lambda = 25^\circ 15' E$   $g =$   $\Delta G = +1^h$ 

Monat	Mittlerer Luftdruck $P_e$ hPa	Mittlere Luftfeuchtigkeit $P_{e,h}$	Mittlere Lufttemperatur $T_m$				Lufttemperatur $T$						Windverteilung $nD, F_m$															
			8	14	19	Dies	Max	Min	Max	Das	Min	Das	N	NE	E	SE	S	SW	W	NW	C							
I			-3.7	-3.9	-3.5	-3.7	-6.3	3.6	15	-13.7	6	25	4.0	0	-	0	-	43.9	3.8	155	2.5	105	2.8	21	3.4	0		
II			-4.6	-3.5	-3.8	-4.1	-6.3	4.8	15	-14.0	29	5	4.3	25	4.4	35	4.1	05	3.0	41.5	3.8	11	3.1	12	3.5	0		
III			-4.1	-2.7	-4.0	-3.9	-6.6	0.8	22	-11.5	26	13	3.0	12	2.5	6	3.4	25	2.8	48	3.4	45	2.2	115	2.7	23	3.6	0
IV			-2.1	-1.3	-2.7	-2.6	-5.6	4.5	23	-10.1	16	125	3.0	6	2.8	0	-	155	3.5	75	2.7	235	3.1	23	3.3	2		
V			3.3	4.2	2.7	2.8	-0.1	9.6	28	-7.1	3	105	3.3	7	3.6	155	3.1	2	1.8	14	2.3	105	2.3	12	3.0	4		
VI			8.5	9.5	7.8	7.8	4.7	17.8	30	-1.4	1	9	3.0	295	3.4	9	3.6	5	3.2	16	2.7	25	1.2	8	3.4	11	3.5	6
VII			10.2	11.5	9.8	9.7	7.1	19.1	15	3.8	4	115	2.8	405	2.8	5	2.5	2	2.0	1	4.0	0	-	2	3.0	25	3.4	7
VIII			9.9	11.0	9.1	9.4	6.9	16.1	19	2.2	15	7	3.1	19	2.6	5	1.7	25	3.2	13	2.5	05	4.0	12	2.5	29	3.2	7
IX			8.1	9.4	7.1	7.7	4.6	16.8	20	-0.1	6	5	2.5	8	3.0	05	3.0	2	2.5	375	3.8	105	3.0	95	2.5	12	2.7	7
X																												
XI																												
XII																												

## Svarholt

 $\varphi = 70^\circ 58' N$   $\lambda = 26^\circ 42' E$   $g =$   $\Delta G = +1^h$ 

I			-1.4	-1.3	-1.6	-1.4	-3.9	4.0	16	-9.1	6	125	3.0	1	4.5	2	3.5	95	2.4	265	3.2	13	3.0	7	2.8	165	3.7	3
II			-2.2	-1.7	-1.7	-2.0	-4.0	5.8	13	-11.4	26	85	3.0	55	4.7	4	3.8	85	3.7	255	3.6	11	3.6	125	4.8	2		
III			-2.4	-1.3	-2.1	-2.1	-4.5	2.6	9	-9.1	26	10	2.5	4	4.6	6	5.1	105	4.0	355	2.7	10	3.2	25	3.7	10		
IV			-1.8	-1.4	-2.3	-2.2	-4.2	4.2	23	-9.0	11	26	3.5	9	5.3	15	2.7	4	2.5	175	2.3	65	4.2	6	3.1	155	4.5	4
V			3.3	4.0	2.6	2.9	0.8	9.8	10	-4.9	5	85	2.6	7	3.6	75	3.0	5	1.8	175	1.6	24	3.1	6	3.0	105	1.4	7
VI			7.3	8.4	6.9	6.9	4.5	18.8	30	-1.4	18	7	2.1	135	1.9	125	1.9	145	2.6	8	2.2	11	2.7	7	2.5	45	3.8	12
VII			8.7	10.0	9.3	8.9	6.8	16.2	14	4.5	28	175	2.5	10	2.4	8	1.7	1	2.0	26	3.0	14	3.4	19	2.0	8	2.7	11
VIII			8.9	9.8	9.2	9.0	7.4	18.0	19	3.1	31	6	2.5	15	4.3	65	2.8	10	2.0	2	2.0	26	3.0	25	3.5	5	2.2	11
IX			8.0	9.2	8.3	8.2	6.3	15.2	20	1.1	5	13	1.7	35	4.9	65	2.9	75	2.6	205	2.9	175	3.2	175	2.8	45	2.1	11
X			5.7	6.0	5.6	5.7	3.8	10.0	15	-0.9	9	35	2.7	2	2.5	5	1.7	2	2.0	355	2.2	25	2.9	11	3.5	3	2.2	8
XI																												
XII																												

## Sletnes Fyr

 $\varphi = 71^\circ 5' N$   $\lambda = 28^\circ 14' E$   $g = 9.087$   $\Delta G = +1^h$ 

I	990.7	992.0	-1.8	-1.9	-2.2	-2.0	-4.8	2.7	19	-10.5	4	75	4.5	8	4.8	1	2.5	15	3.0	11	2.9	28	4.2	185	3.9	145	4.9	3	
II	1001.6	1003.1	-2.6	-2.3	-2.5	-2.6	-5.2	3.8	13	-20.4	26	14	4.7	2	4.0	19	1.0	55	4.8	115	3.1	255	4.4	95	5.2	0			
III	06.0	07.7	-3.0	-2.1	-3.0	-2.9	-5.8	1.0	7	-10.3	26	25	5.0	45	5.9	7	5.3	10	5.1	115	3.7	255	4.4	95	4.4	3			
IV	07.3	08.6	-2.0	-1.2	-2.2	-2.2	-5.0	4.7	23	-9.6	2	155	4.1	115	4.3	55	3.7	05	4.0	65	2.5	10	3.6	265	4.3	13	6.3	1	
V	13.7	15.0	2.5	3.3	2.5	2.4	0.0	9.9	10	-8.7	4	16	2.6	85	2.6	135	4.6	65	2.8	35	2.6	8	1.9	185	3.6	165	4.0	2	
VI	12.6	13.9	7.2	7.4	5.9	6.3	4.1	19.9	30	1.2	11	125	2.2	13	2.5	21	3.1	21	4.0	3	4.0	2	2	5.0	8	5.1	95	3.8	0
VII	15.7	16.9	7.5	7.9	7.1	7.2	5.7	14.1	17	4.5	28	105	2.0	45	1.8	22	3.7	105	3.9	1	2.0	0	-	45	2.9	75	3.4	4	
VIII	07.7	08.9	6.8	9.6	6.5	8.6	6.7	17.0	19	3.5	31	115	2.6	1	3.5	7	3.4	75	3.4	4	2.6	35	3.1	22	4.7	705	3.4	4	
IX	10.0	11.2	7.9	9.2	7.5	7.8	5.2	19.2	20	0.3	5	3	3.5	15	6.0	45	5.4	5	3.9	12	3.6	19	3.6	295	4.2	115	3.4	4	
X																													
XI																													
XII																													

## Tana

 $\varphi = 70^\circ 27' N$   $\lambda = 28^\circ 16' E$   $g =$   $\Delta G = +1^h$ 

I			-7.9	-7.2	-7.7	-7.6	-15.4	2.5	16	-29.2	4	125	3.6	15	3.7	1	1.0	05	1.0	265	2.0	255	2.1	125	1.6	4	3.8	13
II			-7.2	-5.6	-5.9	-6.4	-11.2	1.4	11	-27.8	29	95	3.1	55	3.6	0	-	20	2.0	17	1.7	305	2.4	15	2.5	8		
III			-7.0	-2.7	-5.0	-5.4	-10.8	0.7	7	-23.4	25	3	2.7	45	1.3	7	1.9	8	1.4	235	1.7	205	1.5	7	1.5	45	4.6	15
IV			-2.7	-0.4	-3.4	-3.4	-9.5	4.2	23	-22.9	3	145	3.5	55	1.7	3	1.0	05	1.0	16	1.4	18	1.6	12	2.6	125	4.5	8
V			3.6	4.7	2.9	2.8	-1.2	10.8	10	-16.1	4	10	2.2	15	3.0	75	2.1	4	1.2	175	1.9	125	1.2	155	2.6	6	3.3	7
VI			9.0	10.4	8.5	8.4	4.5	22.7	30	0.8	7	95	2.5	22	2.4	75	1.5	45	2.2									

## Jahresübersichten

194

$$H_1 = 12 \quad H_2 = \quad h_1 = 2.0 \quad h_2 = \quad h_M = \quad h_T = 1.5$$

Kistrand

$H_0 = 4$        $H_0 = \dots$        $H_0 = 1.6$        $H_0 = \dots$        $H_0 = \dots$        $H_0 = 1.4$

Svarholt

$$H_1 = 7 \quad H_2 = 10.2 \quad h_3 = 1.9 \quad h_4 = 12.5 \quad h_5 = 12.0 \quad h_7 = 2.0$$

Sletnes Fyr

$$H_0 = 5 \quad H_b = \quad h_t = 1.7 \quad h_e = \quad h_d = \quad h_r = 1.7$$

Tana

$$H_0 = 10 \quad H_0 = 12.1 \quad h_c = 1.9 \quad h_0 = 9.2 \quad h_0 = 10.0 \quad h_r = 1.8$$

Vards

1944

## Ekkersøy

 $\varphi = 70^\circ 4' N$   $\lambda = 30^\circ 6' E$   $g =$   $\Delta G = +1^h$ 

Monat	Mittlerer Luftdruck P <sup>0</sup> Hausniveau P <sub>0</sub> <sup>0</sup>	Mittlere Lufttemperatur $T_m$				Lufttemperatur $T$						Windverteilung nD, F <sub>m</sub>															
		8	14	19	Dies	Max	Min	Max	Dec	Min	Dec	N	NE	E	SE	S	SW	W	NW	C							
		I	II	III	IV	V	VI	VII	VIII	IX	X	XI	XII														
I	-4.6	-4.3	-3.8	-4.2		-6.0	1.4	16	-12.0	4	2	2.8	11	3.5	0	-	7	2.7	40	4.3	25	2.9	5	3.6	2		
II	-4.9	-4.6	-4.7	-4.8		-7.2	1.5	16	-15.0	29	6	3.2	6	4.2	1	4.3	3	2.4	7	3.3	43	5.0	10	3.3	5	2.6	3
III	-3.6	-2.5	-3.2	-3.2		-5.3	0.0	7	-11.0	23	4	2.4	13	3.6	1	4.3	12	3.5	15	4.3	26	4.0	12	3.3	4	2.7	3
IV	-2.2	-1.4	-3.0	-2.8		-6.0	3.3	23	-13.0	12	4	2.1	18	3.3	5	3.0	2	4.0	1	5.0	23	3.1	22	3.6	11	3.7	3
V	2.9	3.8	2.5	2.5		-0.4	8.6	10	-7.0	3	6	2.5	15	2.7	17	4.1	2	4.4	1	2.0	15	3.1	12	2.9	9	2.8	16
VI	7.3	8.4	7.1	7.0		4.5	21.5	29	0.0	7	3	2.7	14	4.4	31	3.5	9	3.5	8	2.1	9	3.4	3	4.3	5	3.6	7
VII	8.5	9.3	8.4	8.2		6.2	13.7	27	4.9	7	7	4.3	13	4.1	35	3.3	9	2.7	15	2.1	3	3.3	1	6.0	9	4.1	1
IX																											
X																											
XI																											
XII																											

## Karpbukt

 $\varphi = 60^\circ 40' N$   $\lambda = 30^\circ 23' E$   $g =$   $\Delta G = +1^h$ 

Monat		- 8.6 - 9.1 - 8.3 - 8.7				-13.7 2.0 16 -34.2 5 0 9 5.0 0 0 0 2 3.5 28 1.9 0 -						0 0 2.0 39 2.3 2 0 0 37 2.2 0 0 24 1.6 0 - 11 3.6 50																	
		-7.9	-6.1	-6.8	-7.0	-11.8	1.6	16	-29.2	29	19	3.0	89	4.4	1	1.0	53	1.8	0 5	2.0	39 2.3 2 0 0 37 2.2 0 0 24 1.6 0 - 11 3.6 50								
IV	V	VI	VII	VIII	IX	X	XI	XII																					
I	-6.9	-3.3	-5.8	-5.9		-11.5	1.0	11	-22.8	25	0	-	8	3.4	53	2.2	0	-	2	1.5	0	-	24	1.6	0	-	21	2.7	23
II	-3.6	-1.1	-3.5	-3.5		-7.5	5.0	23	-14.4	1	2	2.8	18	3.2	0	-	2	1.5	0	-	24	1.6	0	-	21	2.7	23		
III	3.1	4.6	2.8	2.8		-0.7	10.3	28	-7.3	3	15	3.0	34	2.9	1	3.0	53	1.9	0	-	14	1.5	13	3.0	15	2.4	20		
IV	9.0	10.7	9.0	8.6		4.4	25.6	29	-1.1	7	1	3.0	48	3.2	1	3.5	11	2.2	0	-	11	2.5	29	3.2	7	3.2	7		
V	10.0	11.7	10.1	9.7		6.3	18.6	17	3.1	2	2	4.0	60	3.3	53	2.5	33	2.0	0	-	4	1.2	0	-	12	3.5	6		
VI	10.8	12.1	10.4	10.3		6.8	18.8	20	0.1	23	5	2.9	19	3.2	0.9	1.0	23	2.6	0.9	3.0	18	2.3	3	2.5	21	2.3	22		
IX	7.5	10.6	7.6	7.7		2.6	18.6	20	-5.3	7	1	3.5	8	3.1	0	-	8	2.2	0	-	39	2.7	9	3.1	7	2.6	17		
X																													
XI																													
XII																													

## Karasjok

 $\varphi = 60^\circ 20' N$   $\lambda = 25^\circ 31' E$   $g = 9.825$   $\Delta G = +1^h$ 

Monat		978.5 995.2 -12.5 -13.4 -13.6 -13.2				-20.4 0.8 16 -41.4 9 3 2.3 2 1.0 7 1.0 19 2.3 45 2.1 29 2.6 8 1.9 55 2.0 59						0 0 2.0 7 2.4 10 1.8 2 2.0 45 2.1 29 1.2 83 1.6 39 2.3 1.9 51 2.2 29																	
		995.2	1006.2	-12.6	-7.8	-10.4	-10.6	-18.0	1.0	22	-38.1	29	3	2.3	53	1.5	12	1.1	1	1.5	5	1.6	7	2.4	10	1.8	2 2.0 45		
IV	V	VI	VII	VIII	VIII	VIII	IX	X	XI	XII																			
I	91.6	98.4	-10.5	-4.0	-8.4	-8.6		-14.9	-0.2	10	-33.4	26	3	1.7	7	1.5	12	1.1	1	2.3	29	1.2	83	1.6	39	2.3 1.9 51			
II	93.8	10.5	-5.3	-0.9	-4.2	-5.5		-13.6	6.9	21	-25.5	4	9	2.1	43	1.2	25	1.0	0.9	1.0	2.3	29	1.2	7	1.8	2 2.0 29			
III	96.6	15.1	3.7	5.6	3.3	2.8		-2.5	15.6	26	-15.2	3	17	1.8	11	2.2	7	1.9	1	1.5	0.9	1.0	6	2.0	20	1.9	10	1.8	19
IV	96.6	12.6	9.6	12.6	10.8	9.5		4.5	25.5	29	-0.1	4	15	1.9	145	1.9	21	1.9	3	1.2	6	1.8	2.5	5	7	2.3	8	2.1	5
V	99.4	15.2	9.2	16.4	14.0	12.6		6.4	27.8	14	-0.4	4	28	2.1	9	1.8	17	1.4	4	1.5	55	1.0	1	1.5	7	1.4	8	2.1	15
VI	93.4	9.4	10.4	13.5	10.7	10.2		5.5	20.1	25	-2.8	15	16	1.5	6	7	1.1	0.9	1.0	4	1.5	10	2.4	14	1.9	34			
IX	96.2	12.4	5.3	11.3	5.9	6.4		0.8	19.5	20	-9.4	7	6	2.0	33	1.9	4	1.1	3	1.5	55	2.3	10	1.7	18	1.7	3	1.9	36
X																													
XI																													
XII																													

## Kautokeino

 $\varphi = 60^\circ 0' N$   $\lambda = 25^\circ 2' E$   $g =$   $\Delta G = +1^h$ 

Monat		-12.2 -12.5 -13.0 -12.6				-19.8 2.8 15 -40.9 9 3 2.3 0 1.0 0 0 0 2.1 32 2.1 11 2.6 105 2.8 79 2.6 18						0 0 2.0 38 2.5 105 3.0 95 2.8 2 0 65 1.8 11 2.1 32											

Jahresübersichten

1944

$H_a = 7$     $H_b =$     $h_c = 1.7$     $h_d =$     $h_e =$     $h_r = 1.9$

Ekkersy

Monat	Mittlere Relative Feuchte  $U_m$				Mittlere Bewölkung  $N_m$				Niederschlag  $R$				Zahl der Tage n																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																							
												Lufttemperatur T		Niederschl. R		Windstärke F		Regen		Schne		Regen- schne		Niesel		Ra- tgang		Frost- graspain		Hagel		Gewitter		Dunk		Nebel		Sonnen- stunden		Heller		Schwar- ze Stunde																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																										
8	14	19	Dm	8	14	19		$\Sigma$	Max	Dm	$\Sigma$	$\Delta$	$\sigma$	$\Sigma$	$\Delta$	$\sigma$	$F_0$	$F_1$	$F_2$	$F_3$	$F_4$	$F_5$	$F_6$	$F_7$	$F_8$	$F_9$	$F_{10}$	$F_{11}$	$F_{12}$	$F_{13}$	$F_{14}$	$F_{15}$	$F_{16}$	$F_{17}$	$F_{18}$	$F_{19}$	$F_{20}$	$F_{21}$	$F_{22}$	$F_{23}$	$F_{24}$	$F_{25}$	$F_{26}$	$F_{27}$	$F_{28}$	$F_{29}$	$F_{30}$	$F_{31}$	$F_{32}$	$F_{33}$	$F_{34}$	$F_{35}$	$F_{36}$	$F_{37}$	$F_{38}$	$F_{39}$	$F_{40}$	$F_{41}$	$F_{42}$	$F_{43}$	$F_{44}$	$F_{45}$	$F_{46}$	$F_{47}$	$F_{48}$	$F_{49}$	$F_{50}$	$F_{51}$	$F_{52}$	$F_{53}$	$F_{54}$	$F_{55}$	$F_{56}$	$F_{57}$	$F_{58}$	$F_{59}$	$F_{60}$	$F_{61}$	$F_{62}$	$F_{63}$	$F_{64}$	$F_{65}$	$F_{66}$	$F_{67}$	$F_{68}$	$F_{69}$	$F_{70}$	$F_{71}$	$F_{72}$	$F_{73}$	$F_{74}$	$F_{75}$	$F_{76}$	$F_{77}$	$F_{78}$	$F_{79}$	$F_{80}$	$F_{81}$	$F_{82}$	$F_{83}$	$F_{84}$	$F_{85}$	$F_{86}$	$F_{87}$	$F_{88}$	$F_{89}$	$F_{90}$	$F_{91}$	$F_{92}$	$F_{93}$	$F_{94}$	$F_{95}$	$F_{96}$	$F_{97}$	$F_{98}$	$F_{99}$	$F_{100}$	$F_{101}$	$F_{102}$	$F_{103}$	$F_{104}$	$F_{105}$	$F_{106}$	$F_{107}$	$F_{108}$	$F_{109}$	$F_{110}$	$F_{111}$	$F_{112}$	$F_{113}$	$F_{114}$	$F_{115}$	$F_{116}$	$F_{117}$	$F_{118}$	$F_{119}$	$F_{120}$	$F_{121}$	$F_{122}$	$F_{123}$	$F_{124}$	$F_{125}$	$F_{126}$	$F_{127}$	$F_{128}$	$F_{129}$	$F_{130}$	$F_{131}$	$F_{132}$	$F_{133}$	$F_{134}$	$F_{135}$	$F_{136}$	$F_{137}$	$F_{138}$	$F_{139}$	$F_{140}$	$F_{141}$	$F_{142}$	$F_{143}$	$F_{144}$	$F_{145}$	$F_{146}$	$F_{147}$	$F_{148}$	$F_{149}$	$F_{150}$	$F_{151}$	$F_{152}$	$F_{153}$	$F_{154}$	$F_{155}$	$F_{156}$	$F_{157}$	$F_{158}$	$F_{159}$	$F_{160}$	$F_{161}$	$F_{162}$	$F_{163}$	$F_{164}$	$F_{165}$	$F_{166}$	$F_{167}$	$F_{168}$	$F_{169}$	$F_{170}$	$F_{171}$	$F_{172}$	$F_{173}$	$F_{174}$	$F_{175}$	$F_{176}$	$F_{177}$	$F_{178}$	$F_{179}$	$F_{180}$	$F_{181}$	$F_{182}$	$F_{183}$	$F_{184}$	$F_{185}$	$F_{186}$	$F_{187}$	$F_{188}$	$F_{189}$	$F_{190}$	$F_{191}$	$F_{192}$	$F_{193}$	$F_{194}$	$F_{195}$	$F_{196}$	$F_{197}$	$F_{198}$	$F_{199}$	$F_{200}$	$F_{201}$	$F_{202}$	$F_{203}$	$F_{204}$	$F_{205}$	$F_{206}$	$F_{207}$	$F_{208}$	$F_{209}$	$F_{210}$	$F_{211}$	$F_{212}$	$F_{213}$	$F_{214}$	$F_{215}$	$F_{216}$	$F_{217}$	$F_{218}$	$F_{219}$	$F_{220}$	$F_{221}$	$F_{222}$	$F_{223}$	$F_{224}$	$F_{225}$	$F_{226}$	$F_{227}$	$F_{228}$	$F_{229}$	$F_{230}$	$F_{231}$	$F_{232}$	$F_{233}$	$F_{234}$	$F_{235}$	$F_{236}$	$F_{237}$	$F_{238}$	$F_{239}$	$F_{240}$	$F_{241}$	$F_{242}$	$F_{243}$	$F_{244}$	$F_{245}$	$F_{246}$	$F_{247}$	$F_{248}$	$F_{249}$	$F_{250}$	$F_{251}$	$F_{252}$	$F_{253}$	$F_{254}$	$F_{255}$	$F_{256}$	$F_{257}$	$F_{258}$	$F_{259}$	$F_{260}$	$F_{261}$	$F_{262}$	$F_{263}$	$F_{264}$	$F_{265}$	$F_{266}$	$F_{267}$	$F_{268}$	$F_{269}$	$F_{270}$	$F_{271}$	$F_{272}$	$F_{273}$	$F_{274}$	$F_{275}$	$F_{276}$	$F_{277}$	$F_{278}$	$F_{279}$	$F_{280}$	$F_{281}$	$F_{282}$	$F_{283}$	$F_{284}$	$F_{285}$	$F_{286}$	$F_{287}$	$F_{288}$	$F_{289}$	$F_{290}$	$F_{291}$	$F_{292}$	$F_{293}$	$F_{294}$	$F_{295}$	$F_{296}$	$F_{297}$	$F_{298}$	$F_{299}$	$F_{300}$	$F_{301}$	$F_{302}$	$F_{303}$	$F_{304}$	$F_{305}$	$F_{306}$	$F_{307}$	$F_{308}$	$F_{309}$	$F_{310}$	$F_{311}$	$F_{312}$	$F_{313}$	$F_{314}$	$F_{315}$	$F_{316}$	$F_{317}$	$F_{318}$	$F_{319}$	$F_{320}$	$F_{321}$	$F_{322}$	$F_{323}$	$F_{324}$	$F_{325}$	$F_{326}$	$F_{327}$	$F_{328}$	$F_{329}$	$F_{330}$	$F_{331}$	$F_{332}$	$F_{333}$	$F_{334}$	$F_{335}$	$F_{336}$	$F_{337}$	$F_{338}$	$F_{339}$	$F_{340}$	$F_{341}$	$F_{342}$	$F_{343}$	$F_{344}$	$F_{345}$	$F_{346}$	$F_{347}$	$F_{348}$	$F_{349}$	$F_{350}$	$F_{351}$	$F_{352}$	$F_{353}$	$F_{354}$	$F_{355}$	$F_{356}$	$F_{357}$	$F_{358}$	$F_{359}$	$F_{360}$	$F_{361}$	$F_{362}$	$F_{363}$	$F_{364}$	$F_{365}$	$F_{366}$	$F_{367}$	$F_{368}$	$F_{369}$	$F_{370}$	$F_{371}$	$F_{372}$	$F_{373}$	$F_{374}$	$F_{375}$	$F_{376}$	$F_{377}$	$F_{378}$	$F_{379}$	$F_{380}$	$F_{381}$	$F_{382}$	$F_{383}$	$F_{384}$	$F_{385}$	$F_{386}$	$F_{387}$	$F_{388}$	$F_{389}$	$F_{390}$	$F_{391}$	$F_{392}$	$F_{393}$	$F_{394}$	$F_{395}$	$F_{396}$	$F_{397}$	$F_{398}$	$F_{399}$	$F_{400}$	$F_{401}$	$F_{402}$	$F_{403}$	$F_{404}$	$F_{405}$	$F_{406}$	$F_{407}$	$F_{408}$	$F_{409}$	$F_{410}$	$F_{411}$	$F_{412}$	$F_{413}$	$F_{414}$	$F_{415}$	$F_{416}$	$F_{417}$	$F_{418}$	$F_{419}$	$F_{420}$	$F_{421}$	$F_{422}$	$F_{423}$	$F_{424}$	$F_{425}$	$F_{426}$	$F_{427}$	$F_{428}$	$F_{429}$	$F_{430}$	$F_{431}$	$F_{432}$	$F_{433}$	$F_{434}$	$F_{435}$	$F_{436}$	$F_{437}$	$F_{438}$	$F_{439}$	$F_{440}$	$F_{441}$	$F_{442}$	$F_{443}$	$F_{444}$	$F_{445}$	$F_{446}$	$F_{447}$	$F_{448}$	$F_{449}$	$F_{450}$	$F_{451}$	$F_{452}$	$F_{453}$	$F_{454}$	$F_{455}$	$F_{456}$	$F_{457}$	$F_{458}$	$F_{459}$	$F_{460}$	$F_{461}$	$F_{462}$	$F_{463}$	$F_{464}$	$F_{465}$	$F_{466}$	$F_{467}$	$F_{468}$	$F_{469}$	$F_{470}$	$F_{471}$	$F_{472}$	$F_{473}$	$F_{474}$	$F_{475}$	$F_{476}$	$F_{477}$	$F_{478}$	$F_{479}$	$F_{480}$	$F_{481}$	$F_{482}$	$F_{483}$	$F_{484}$	$F_{485}$	$F_{486}$	$F_{487}$	$F_{488}$	$F_{489}$	$F_{490}$	$F_{491}$	$F_{492}$	$F_{493}$	$F_{494}$	$F_{495}$	$F_{496}$	$F_{497}$	$F_{498}$	$F_{499}$	$F_{500}$	$F_{501}$	$F_{502}$	$F_{503}$	$F_{504}$	$F_{505}$	$F_{506}$	$F_{507}$	$F_{508}$	$F_{509}$	$F_{510}$	$F_{511}$	$F_{512}$	$F_{513}$	$F_{514}$	$F_{515}$	$F_{516}$	$F_{517}$	$F_{518}$	$F_{519}$	$F_{520}$	$F_{521}$	$F_{522}$	$F_{523}$	$F_{524}$	$F_{525}$	$F_{526}$	$F_{527}$	$F_{528}$	$F_{529}$	$F_{530}$	$F_{531}$	$F_{532}$	$F_{533}$	$F_{534}$	$F_{535}$	$F_{536}$	$F_{537}$	$F_{538}$	$F_{539}$	$F_{540}$	$F_{541}$	$F_{542}$	$F_{543}$	$F_{544}$	$F_{545}$	$F_{546}$	$F_{547}$	$F_{548}$	$F_{549}$	$F_{550}$	$F_{551}$	$F_{552}$	$F_{553}$	$F_{554}$	$F_{555}$	$F_{556}$	$F_{557}$	$F_{558}$	$F_{559}$	$F_{560}$	$F_{561}$	$F_{562}$	$F_{563}$	$F_{564}$	$F_{565}$	$F_{566}$	$F_{567}$	$F_{568}$	$F_{569}$	$F_{570}$	$F_{571}$	$F_{572}$	$F_{573}$	$F_{574}$	$F_{575}$	$F_{576}$	$F_{577}$	$F_{578}$	$F_{579}$	$F_{580}$	$F_{581}$	$F_{582}$	$F_{583}$	$F_{584}$	$F_{585}$	$F_{586}$	$F_{587}$	$F_{588}$	$F_{589}$	$F_{590}$	$F_{591}$	$F_{592}$	$F_{593}$	$F_{594}$	$F_{595}$	$F_{596}$	$F_{597}$	$F_{598}$	$F_{599}$	$F_{600}$	$F_{601}$	$F_{602}$	$F_{603}$	$F_{604}$	$F_{605}$	$F_{606}$	$F_{607}$	$F_{608}$	$F_{609}$	$F_{610}$	$F_{611}$	$F_{612}$	$F_{613}$	$F_{614}$	$F_{615}$	$F_{616}$	$F_{617}$	$F_{618}$	$F_{619}$	$F_{620}$	$F_{621}$	$F_{622}$	$F_{623}$	$F_{624}$	$F_{625}$	$F_{626}$	$F_{627}$	$F_{628}$	$F_{629}$	$F_{630}$	$F_{631}$	$F_{632}$	$F_{633}$	$F_{634}$	$F_{635}$	$F_{636}$	$F_{637}$	$F_{638}$	$F_{639}$	$F_{640}$	$F_{641}$	$F_{642}$	$F_{643}$	$F_{644}$	$F_{645}$	$F_{646}$	$F_{647}$	$F_{648}$	$F_{649}$	$F_{650}$	$F_{651}$	$F_{652}$	$F_{653}$	$F_{654}$	$F_{655}$	$F_{656}$	$F_{657}$	$F_{658}$	$F_{659}$	$F_{660}$	$F_{661}$	$F_{662}$	$F_{663}$	$F_{664}$	$F_{665}$	$F_{666}$	$F_{667}$	$F_{668}$	$F_{669}$	$F_{670}$	$F_{671}$	$F_{672}$	$F_{673}$	$F_{674}$	$F_{675}$	$F_{676}$	$F_{677}$	$F_{678}$	$F_{679}$	$F_{680}$	$F_{681}$	$F_{682}$	$F_{683}$	$F_{684}$	$F_{685}$	$F_{686}$	$F_{687}$	$F_{688}$	$F_{689}$	$F_{690}$	$F_{691}$	$F_{692}$	$F_{693}$	$F_{694}$	$F_{695}$	$F_{696}$	$F_{697}$	$F_{698}$	$F_{699}$	$F_{700}$	$F_{701}$	$F_{702}$	$F_{703}$	$F_{704}$	$F_{705}$	$F_{706}$	$F_{707}$	$F_{708}$	$F_{709}$	$F_{710}$	$F_{711}$	$F_{712}$	$F_{713}$	$F_{714}$	$F_{715}$	$F_{716}$	$F_{717}$	$F_{718}$	$F_{719}$	$F_{720}$	$F_{721}$	$F_{722}$	$F_{723}$	$F_{724}$	$F_{725}$	$F_{726}$	$F_{727}$	$F_{728}$	$F_{729}$	$F_{730}$	$F_{731}$	$F_{732}$	$F_{733}$	$F_{734}$	$F_{735}$	$F_{736}$	$F_{737}$	$F_{738}$	$F_{739}$	$F_{740}$	$F_{741}$	$F_{742}$	$F_{743}$	$F_{744}$	$F_{745}$	$F_{746}$	$F_{747}$	$F_{748}$	$F_{749}$	$F_{750}$	$F_{751}$	$F_{752}$	$F_{753}$	$F_{754}$	$F_{755}$	$F_{756}$	$F_{757}$	$F_{758}$	$F_{759}$	$F_{760}$	$F_{761}$	$F_{762}$	$F_{763}$	$F_{764}$	$F_{765}$	$F_{766}$	$F_{767}$	$F_{768}$	$F_{769}$	$F_{770}$	$F_{771}$	$F_{772}$	$F_{773}$	$F_{774}$	$F_{775}$	$F_{776}$	$F_{777}$	$F_{778}$	$F_{779}$	$F_{780}$	$F_{781}$	$F_{782}$	$F_{783}$	$F_{784}$	$F_{785}$	$F_{786}$	$F_{7$

Pentadenmittel der Lufttemperatur

1944

Pentaden.	Røros	Alydal	Dombås	Vinstra	Vollen i Slidre	Lillehammer	Rens	Vang på Hedmark	Østre Toten	Flesa	Modum	Nesbyen	Horten	As	Eidsberg	Gvær	Byglandsfjord	Kristiansand S.	Klepp
1.I - 3.I	- 8.9	- 12.0	- 6.6	- 9.5	- 7.2	- 7.9	- 13.4	- 7.0	- 5.2	- 9.7	- 4.1	- 9.0	- 1.2	- 3.3	- 4.3	- 5.0	- 1.8	0.9	1.6
6.I - 10.I	- 18.8	- 18.1	- 13.5	- 19.2	- 10.0	- 10.5	- 14.2	- 9.7	- 8.1	- 9.3	- 5.4	- 9.0	- 1.8	- 4.1	- 4.4	- 4.5	- 3.6	- 0.9	1.1
11.I - 15.I	- 7.8	- 11.7	- 7.9	- 16.0	- 7.8	- 11.0	- 16.3	- 8.9	- 6.7	- 13.2	- 5.3	- 12.9	- 1.2	- 5.7	- 5.1	- 7.1	- 1.3	2.9	2.9
16.I - 20.I	- 6.9	- 6.8	- 2.9	- 11.6	- 3.2	- 7.4	- 7.0	- 4.0	- 4.0	- 4.1	- 4.5	- 7.0	- 0.6	- 2.2	- 0.9	- 6.7	- 0.7	2.7	4.7
21.I - 25.I	- 6.3	- 7.4	- 4.9	- 8.0	- 2.0	- 8.8	- 7.3	- 3.2	- 4.1	- 2.9	- 2.2	- 6.3	1.5	0.5	0.4	- 1.5	0.9	3.1	4.1
26.I - 30.I	- 4.3	- 4.8	- 3.6	- 5.8	- 3.1	- 4.7	- 4.9	- 2.8	- 1.6	- 1.7	1.1	- 3.4	2.7	1.4	1.2	- 0.4	2.4	4.5	5.2
31.I - 4.III	- 5.5	- 5.0	- 2.9	- 3.0	- 1.4	- 3.7	- 4.4	- 1.9	- 2.5	- 1.5	0.9	- 0.6	2.3	1.0	1.4	2.0	4.4	4.9	
5.II - 9.II	- 4.4	- 4.8	- 5.3	- 3.5	- 5.2	- 4.3	- 5.5	- 3.1	- 2.8	- 3.7	- 1.4	- 4.1	1.2	- 0.9	- 1.4	- 1.0	- 0.2	2.1	1.7
10.II - 14.II	- 6.5	- 5.2	- 5.5	- 4.6	- 6.3	- 4.4	- 5.7	- 4.5	- 4.2	- 6.0	- 3.3	- 6.5	- 1.0	- 2.9	- 3.6	- 2.9	0.0	- 0.7	0.5
15.II - 19.II	- 9.5	- 9.2	- 8.3	- 8.4	- 9.4	- 6.3	- 6.7	- 5.4	- 6.7	- 4.4	- 7.2	- 2.6	- 4.0	- 3.5	- 3.6	- 2.5	- 1.0	0.5	
20.II - 24.II	- 2.4	- 2.2	- 2.2	0.0	- 5.7	- 0.8	- 2.6	- 2.0	- 4.8	- 2.8	- 4.3	- 8.5	- 0.1	- 1.3	- 1.4	- 4.7	- 2.5	0.6	0.2
25.II - 1.III	- 11.8	- 9.9	- 9.2	- 8.3	- 9.3	- 8.2	- 8.3	- 6.9	- 6.6	- 7.4	- 5.0	- 8.0	- 2.6	- 4.1	- 3.6	- 5.1	- 5.5	- 1.0	- 0.3
2.III - 6.III	- 5.1	- 6.5	- 5.6	- 4.9	- 5.2	- 6.3	- 7.6	- 6.0	- 4.3	- 6.0	- 4.0	- 7.8	- 1.4	- 3.6	- 3.6	- 4.7	- 4.3	- 1.0	0.4
7.III - 11.III	- 0.1	- 1.9	- 1.0	- 0.6	- 1.1	- 0.3	- 1.3	- 1.3	- 0.3	- 0.3	- 0.3	- 1.6	1.0	- 0.3	- 0.5	- 0.4	0.5	2.2	2.7
12.III - 16.III	- 7.7	- 6.1	- 5.5	- 3.9	- 5.2	- 3.6	- 4.0	- 3.5	- 2.6	- 2.6	- 1.1	- 4.5	- 0.5	- 1.2	- 0.5	- 1.1	- 0.7	1.4	2.3
17.III - 21.III	- 6.6	- 4.6	- 5.0	- 3.0	- 2.8	- 2.6	- 3.0	- 2.2	- 2.0	- 1.4	0.5	- 1.2	2.0	0.9	0.7	1.2	0.8	3.2	3.1
22.III - 26.III	- 6.0	- 4.7	- 3.7	- 3.6	- 2.1	- 2.8	- 3.6	- 2.8	- 2.4	- 2.6	- 0.3	- 0.8	1.6	- 0.1	0.0	0.9	0.8	2.7	3.4
27.III - 31.III	- 7.2	- 5.5	- 6.2	- 3.8	- 3.1	- 2.9	- 3.7	- 3.4	- 3.0	- 3.5	- 0.6	- 1.3	- 0.6	- 0.6	- 1.7	0.3	0.0	1.1	1.9
1.IV - 5.IV	- 11.3	- 8.3	- 6.3	- 5.5	- 6.1	- 4.6	- 7.3	- 4.9	- 4.3	- 3.8	- 2.3	- 4.4	0.5	- 0.4	- 0.7	- 0.8	- 1.7	0.4	2.8
6.IV - 10.IV	- 3.9	- 0.7	- 1.4	0.6	0.2	0.6	- 0.3	1.0	1.6	1.9	2.6	1.3	3.7	2.9	3.2	3.3	1.9	3.6	5.7
11.IV - 15.IV	1.1	1.0	1.9	3.5	2.9	1.7	1.6	2.1	1.6	1.8	2.9	2.6	3.5	2.8	2.6	3.4	3.2	5.5	6.8
16.IV - 20.IV	- 1.8	- 0.5	- 0.2	2.1	1.7	1.6	1.6	2.0	1.4	2.9	3.1	3.2	4.5	3.7	3.0	4.0	3.8	5.5	6.5
21.IV - 25.IV	0.6	2.7	2.6	4.8	4.3	4.1	3.5	4.0	4.6	4.3	6.3	5.0	8.5	6.8	6.1	8.0	6.7	9.5	7.1
26.IV - 30.IV	- 1.1	1.2	- 0.1	3.2	3.4	3.1	2.7	2.8	3.1	3.9	5.1	4.7	7.2	5.6	4.9	5.9	5.5	8.0	5.8
1.V - 5.V	- 1.9	0.1	- 1.1	2.2	2.3	2.1	2.0	2.3	1.6	2.6	3.4	3.7	5.4	4.1	4.4	5.7	5.4	7.0	6.5
6.V - 10.V	- 0.9	2.4	1.9	5.1	3.8	6.2	5.4	6.6	6.3	5.8	6.4	5.5	8.2	7.1	6.4	7.2	6.1	7.7	6.6
11.V - 15.V	4.5	6.1	5.6	8.6	8.2	8.6	8.3	9.1	9.2	9.8	9.7	8.7	10.1	9.6	10.2	8.5	8.9	10.5	9.7
16.V - 30.V	2.8	5.0	5.2	8.8	8.8	9.0	8.3	8.2	8.6	9.2	9.1	8.8	10.9	9.9	9.1	11.6	10.4	10.4	11.2
21.V - 25.V	0.3	1.5	0.8	5.2	4.6	4.9	4.7	4.7	4.6	4.7	6.1	5.9	7.3	5.9	4.5	6.8	6.3	9.4	6.7
26.V - 30.V	5.3	7.2	6.7	9.8	9.4	10.6	13.5	10.5	11.3	11.1	13.1	11.7	13.3	15.0	11.5	12.9	12.6	14.6	11.4
31.V - 4.VI	4.7	6.0	5.5	7.9	7.9	8.6	8.3	8.5	8.6	8.7	9.3	9.2	10.5	9.7	9.1	10.6	9.4	10.9	9.1
5.VI - 9.VI	8.7	9.0	9.0	10.7	10.1	10.5	10.1	10.1	9.6	9.9	10.9	11.6	12.0	11.8	11.5	12.0	10.7	11.8	10.6
10.VI - 14.VI	6.0	6.8	7.2	8.9	9.0	9.0	8.9	8.3	8.6	9.0	10.2	9.9	10.7	10.3	9.7	10.9	9.8	11.8	10.9
15.VI - 19.VI	9.0	11.1	9.9	15.0	11.5	13.2	12.7	13.0	13.5	13.1	14.3	13.0	14.0	14.2	13.1	13.3	12.7	14.0	11.5
20.VI - 24.VI	6.2	8.6	7.9	11.4	10.9	12.4	11.6	11.5	12.1	12.0	13.3	12.7	13.6	13.4	12.7	13.9	14.6	13.7	11.0
25.VI - 29.VI	10.2	11.3	10.8	12.9	12.1	13.0	13.1	13.1	13.5	13.5	14.5	14.0	15.0	14.2	13.9	15.1	12.6	13.8	13.9
30.VI - 4.VII	13.1	15.4	13.2	14.4	14.8	15.2	15.6	15.4	15.4	16.4	16.0	15.0	15.7	16.7	16.3	16.1	15.1	16.3	15.3
5.VII - 9.VII	18.2	20.5	18.0	21.5	19.7	21.2	22.2	21.2	21.8	22.0	21.9	20.4	20.8	20.8	21.2	20.2	20.5	18.9	
10.VII - 14.VII	14.0	14.0	11.9	14.6	13.4	14.9	14.9	15.2	14.9	14.8	15.2	15.6	14.5	15.2	16.0	15.1	16.2	14.0	15.6
15.VII - 19.VII	13.8	15.3	14.5	17.1	16.9	17.5	17.1	17.0	17.6	17.0	18.4	17.0	19.0	18.7	17.2	18.2	16.5	17.6	14.1
20.VII - 24.VII	9.9	11.6	12.0	14.2	14.7	15.2	14.7	14.6	15.3	14.9	15.9	15.4	17.3	17.0	16.1	16.6	16.9	17.3	13.8
25.VII - 29.VII	10.6	10.9	10.7	12.5	12.1	13.2	13.0	13.0	13.0	13.2	14.1	13.7	15.6	15.0	14.6	15.1	13.9	15.7	14.8
30.VII - 3.VIII	14.5	16.0	15.8	17.5	16.8	17.9	17.9	18.0	17.9	17.8	18.6	17.5	19.6	19.7	18.8	19.1	18.3	19.1	15.6
4.VIII - 8.VIII	14.1	16.7	16.2	18.5	17.1	18.6	18.6	18.8	18.7	18.2	19.2	18.1	18.9	19.4	18.8	19.2	18.3	18.4	15.7
9.VIII - 13.VIII	11.2	12.1	12.1	13.4	14.1	14.2	14.4	14.4	14.8	14.8	15.5	13.9	16.9	16.1	16.1	15.5	14.6	15.6	15.0
14.VIII - 18.VIII	10.3	11.3	9.8	12.2	11.3	13.2	13.2	13.2	14.0	14.4	14.8	12.5	15.4	14.9	14.2	14.8	14.6	15.3	14.5
19.VIII - 23.VIII	11.2	11.7	10.4	13.0	13.8	15.8	15.9	14.1	13.6	15.3	16.7	14.9	16.5	16.7	16.4	17.1	17.0	17.4	15.0
24.VIII - 28.VIII	13.6	14.7	14.3	15.2	14.8	15.5	15.5	16.2	15.2	16.6	17.3	15.4	17.7	17.5	17.8	15.3	15.9	17.4	17.6
29.VIII - 2.IX	7.8	8.4	8.4	10.0	10.3	10.5	10.5	10.6	10.7	10.5	11.7	10.7	15.1	12.3	12.4	11.6	10.9	12.7	12.4
3.IX - 7.IX	6.3	7.8	7.0	9.3	8.3	9.6	9.5	9.3	9.0	9.7	9.4	9.2	11.0	10.5	9.9	11.2	10.3	11.7	12.1
8.IX - 12.IX	5.6	6.6	5.9	7.8	7.4	8.6	8.7	8.3	9.3	9.5	10.0	8.1	11.1	11.0	10.3	10.9	10.7	12.0	11.5
13.IX - 17.IX	7.0	8.1	8.2	9.3	8.5	10.0	10.5	10.0	9.8	10.2	10.5	9.4	11.8	11.6	11.4	11.5	11.8	13.3	13.3
18.IX - 22.IX	9.7	9.0	9.0	10.2	9.7	10.4	10.2	10.1	10.0	10.5	11.8	10.9	12.2	11.2	10.7	11.9	13.4	12.9	
23.IX - 27.IX	5.9	6.4	5.4	7.5	6.5	7.9	8.2	8.2	8.4	8.5	9.3	7.6	10.0	9.4	9.3	10.1	7.8	14.1	
28.IX - 2.X	3.0	3.6	3.4	4.5	4.4	5.2	5.4	5.8	6.1	5.7	6.5	4.6	6.9	6.9	6.				

Pentadenmittel der Lufttemperatur

1944

Pentaden.	Saude	Ullensvang	Syfjord	Lekanger	Brandsøy i Kinn	Nordfjorddeid	Tafjord	Runde	Tingvoll	Vallersund	Trondheim (Voll)	Kjervi i Snøsæ	Brennøystrand	Ytteren i Rana	Bodø	Offørøy	Tromsø	Alta (Elvebakken)	Karibukt
1.I - 5.I	-2.3	-0.2	-1.6	-0.2	-1.4	-0.3	-0.5	2.8	-0.3	-1.2	-3.3	-9.6	-3.0	-11.3	-5.2	-4.4	-6.4	-13.0	-18.7
6.I - 10.I	-1.9	-0.6	-1.6	-2.0	-0.4	-3.9	-2.4	0.5	-4.7	-0.8	-5.3	-9.9	-2.2	-11.7	-5.9	-6.2	-6.3	-9.0	-10.0
11.I - 15.I	-1.1	0.7	0.2	1.1	2.9	-0.6	1.2	4.1	0.4	2.2	0.3	-3.6	0.3	-8.1	-1.5	-1.6	-1.4	-3.9	-6.8
16.I - 20.I	1.0	2.0	3.9	3.9	6.0	4.7	5.2	7.1	2.9	5.3	3.3	1.7	5.0	3.2	4.2	4.0	2.6	0.3	-3.5
21.I - 25.I	2.4	2.7	2.4	2.6	3.2	1.4	3.3	3.4	1.5	2.2	0.7	-2.0	2.4	-2.7	0.7	0.8	-0.1	-1.8	-5.0
26.I - 30.I	2.9	3.8	3.7	2.8	4.3	2.6	2.0	4.3	1.7	2.8	1.0	-0.4	2.1	-1.9	0.8	0.4	-1.4	-4.8	-8.0
31.I - 4.II	2.8	3.7	4.1	2.2	4.2	2.2	3.6	4.3	1.0	2.9	1.1	-0.6	1.4	-2.2	0.0	-1.2	-1.5	-5.9	-6.5
5.II - 9.II	0.0	1.2	0.3	0.5	1.4	0.3	1.1	1.9	0.3	1.9	0.0	-0.8	2.2	0.1	0.9	0.1	-0.3	-4.9	-7.6
10.II - 14.II	-0.1	-0.9	0.4	-0.5	1.8	-0.4	-0.5	2.9	-1.1	1.9	-0.5	-3.8	1.6	-4.7	0.7	0.5	0.5	-1.5	-5.8
15.II - 19.II	-2.0	-0.1	0.1	-0.1	2.5	1.9	2.3	4.1	-1.0	1.9	-1.8	-4.4	2.8	-3.8	1.5	2.6	2.2	-1.9	-5.8
20.II - 24.II	-2.9	-0.7	0.2	0.4	3.7	1.3	1.3	4.0	2.1	4.0	1.9	0.8	3.4	1.1	2.1	1.5	0.7	-0.8	-4.4
25.II - 1.III	-2.7	-1.7	-3.7	-2.9	-0.7	-2.2	-2.1	-0.9	-2.5	-2.0	-3.5	-6.8	-1.9	-7.7	-3.7	-4.2	-6.1	-9.3	-11.7
2.III - 6.III	-2.6	-1.9	-1.2	-0.3	0.8	-0.3	0.1	1.5	-0.1	1.9	-0.6	-3.6	0.1	-3.0	-1.0	-1.7	-2.8	-4.8	-5.1
7.III - 11.III	-0.4	0.6	0.8	1.6	2.9	1.0	1.2	4.4	2.6	4.0	2.6	1.9	4.0	2.5	3.2	2.3	1.0	-1.8	-3.2
12.III - 16.III	0.0	1.1	0.4	0.8	1.7	0.6	0.6	2.2	-1.1	0.2	-2.2	-2.3	0.2	-2.6	-1.3	-1.5	-2.9	-6.2	-4.2
17.III - 21.III	1.3	2.3	1.2	1.5	2.4	2.7	1.2	2.4	-0.4	1.7	-0.3	-1.8	1.0	-2.6	-0.9	-0.6	-1.2	-3.8	-5.9
22.III - 26.III	-0.1	0.8	0.8	0.9	2.5	1.3	1.4	3.6	0.1	0.4	-1.8	-4.1	-1.3	-4.7	-3.7	-2.8	-4.1	-6.6	-8.9
27.III - 31.III	0.4	0.9	0.1	0.6	1.2	-0.1	-0.4	1.7	-0.5	-1.7	-3.4	-5.2	-2.2	-5.7	-4.5	-3.8	-4.1	-6.7	-8.3
1.IV - 5.IV	1.2	1.1	1.1	1.3	2.0	-0.1	1.1	2.1	-0.9	0.9	-2.7	-3.9	0.9	-3.7	-1.5	-1.1	-2.0	-4.6	-6.5
6.IV - 10.IV	4.7	3.8	4.6	3.0	4.8	3.7	3.8	5.1	1.9	2.3	-0.2	-0.3	1.7	-2.8	-0.7	0.3	-1.4	-4.1	-4.1
11.IV - 15.IV	5.8	5.6	5.5	6.2	6.0	5.3	5.3	5.8	3.5	3.9	2.2	1.5	2.4	-1.7	-1.2	-1.7	-3.7	-4.2	-5.3
16.IV - 20.IV	6.7	6.9	5.6	5.5	5.7	5.1	5.6	5.3	4.1	3.5	1.7	2.8	-0.5	0.4	0.3	-1.6	-2.9	-4.0	-4.0
21.IV - 25.IV	6.7	7.2	6.3	7.0	6.5	6.0	6.9	5.8	4.9	4.9	3.8	2.6	4.5	2.6	2.6	2.1	1.7	-1.1	0.8
26.IV - 30.IV	4.8	5.6	4.5	5.0	4.4	3.8	3.8	4.2	2.4	3.4	2.4	1.4	3.1	0.9	1.1	0.7	-0.3	-1.9	-1.9
1.V - 5.V	5.9	5.3	6.0	4.6	5.8	4.4	4.3	4.6	3.8	3.5	2.5	0.7	3.4	1.0	2.0	1.8	0.0	-1.8	-1.8
6.V - 10.V	5.3	6.9	6.0	6.5	7.3	7.3	7.9	8.2	6.7	6.9	5.5	4.0	7.7	4.9	6.6	5.8	4.6	5.2	3.5
11.V - 15.V	8.7	9.1	8.4	8.4	7.5	7.4	8.7	6.9	6.2	7.2	6.4	5.4	6.5	4.7	5.8	5.4	4.8	6.8	5.5
16.V - 20.V	11.2	12.2	11.4	12.3	11.5	7.8	8.3	6.3	7.1	5.8	5.8	5.2	5.1	4.3	4.1	3.7	2.4	3.2	2.2
21.V - 25.V	6.4	7.3	5.3	6.7	5.8	4.0	4.3	4.5	2.7	4.5	3.4	2.2	4.0	3.8	3.6	3.8	2.1	2.2	1.5
26.V - 30.V	9.9	9.6	10.0	11.0	9.8	9.2	10.5	9.5	8.0	8.3	8.7	6.3	7.8	6.8	6.8	6.0	6.4	7.9	5.7
31.V - 4.VI	9.4	10.2	8.9	10.7	10.0	9.9	9.2	8.4	8.7	8.9	8.1	7.0	8.6	8.6	8.5	8.6	6.8	6.4	3.1
5.VI - 9.VI	11.5	12.1	12.0	14.4	13.2	13.6	14.3	12.4	14.6	14.3	12.8	11.6	13.8	14.0	15.1	13.2	9.7	9.0	4.7
10.VI - 14.VI	9.9	9.3	10.1	11.0	10.8	11.0	11.5	10.7	11.4	11.3	9.8	8.9	10.7	9.1	9.7	10.8	10.5	10.2	7.1
15.VI - 19.VI	13.3	12.5	11.5	13.0	11.9	10.9	11.7	10.3	11.2	11.3	11.3	11.4	10.9	10.4	10.1	9.9	12.3	12.6	12.6
20.VI - 24.VI	13.7	13.2	11.2	12.6	10.9	10.0	10.3	9.4	9.3	8.6	8.3	7.3	7.9	7.7	7.2	7.3	5.6	7.8	7.9
25.VI - 29.VI	12.5	12.2	12.9	13.3	13.3	12.8	13.5	12.1	13.2	12.2	12.7	12.6	12.2	13.1	10.4	10.1	9.1	12.1	12.8
30.VI - 4.VII	14.5	14.5	16.5	15.9	16.7	15.7	14.2	13.2	14.9	11.6	14.5	15.3	10.5	12.1	10.4	11.0	7.9	11.3	11.6
5.VII - 9.VII	17.9	17.7	18.9	18.8	19.4	20.3	16.2	16.5	18.6	13.6	18.7	17.9	12.6	14.1	11.3	11.4	7.5	9.0	7.6
10.VII - 14.VII	14.1	14.1	15.6	15.1	14.6	14.4	14.7	13.6	15.3	15.3	15.6	16.5	16.1	16.2	16.5	15.9	14.9	15.0	9.5
15.VII - 19.VII	15.7	16.1	14.4	17.2	16.2	15.6	15.4	13.5	16.2	13.3	15.1	14.3	12.5	14.8	14.0	15.3	14.3	16.9	10.9
20.VII - 24.VII	18.0	17.8	15.4	18.0	16.4	15.5	14.5	11.6	12.9	11.0	11.5	10.5	10.7	11.8	10.5	11.4	9.2	11.0	9.0
25.VII - 29.VII	15.2	15.2	14.8	15.2	14.2	14.7	14.8	14.1	14.8	14.5	14.0	13.5	14.9	14.1	13.7	12.2	13.6	10.5	10.5
30.VII - 3.VIII	18.9	18.1	16.6	18.3	16.1	17.2	16.8	14.1	17.0	13.8	15.7	14.8	13.2	14.6	12.5	12.9	10.5	12.1	10.2
4.VIII - 8.VIII	19.0	18.9	15.6	18.1	14.4	15.9	15.2	12.9	14.8	12.6	14.4	13.3	12.0	13.2	11.4	11.4	11.6	11.6	10.2
9.VIII - 13.VIII	14.6	14.5	14.0	14.1	13.6	12.7	14.7	13.2	13.0	12.3	12.5	11.6	12.3	12.3	11.9	11.8	9.6	11.1	11.0
14.VIII - 18.VIII	12.9	12.7	13.1	12.4	13.0	13.1	14.3	13.5	12.5	12.5	12.0	11.5	11.5	11.0	10.8	10.5	9.0	10.2	8.9
19.VIII - 23.VIII	14.8	14.3	13.7	14.5	12.3	12.6	11.6	11.6	11.8	10.9	10.9	10.4	10.6	10.4	10.5	10.0	9.5	11.8	11.4
24.VIII - 28.VIII	16.8	15.5	15.0	14.6	15.2	12.9	16.9	14.6	14.3	14.6	14.1	14.1	14.9	13.6	13.6	12.1	11.4	13.2	11.8
29.VIII - 2.IX	11.4	11.8	12.1	12.7	13.1	12.6	11.6	11.4	10.7	10.5	9.8	9.0	10.4	9.6	8.7	8.3	6.2	7.7	7.7
3.IX - 7.IX	11.4	11.1	11.3	12.2	11.5	10.5	10.6	9.9	9.1	8.9	8.4	6.3	8.5	6.2	5.8	5.0	4.1	4.1	4.1
8.IX - 12.IX	10.0	9.7	10.0	9.9	9.3	9.3	9.6	8.9	8.9	8.9	7.9	6.6	8.4	6.0	6.7	6.9	5.5	5.5	5.6
13.IX - 17.IX	11.6	10.7	12.2	11.2	12.3	12.0	12.3	13.1	10.9	12.0	10.7	10.2	12.0	9.3	10.1	9.6	8.8	7.2	5.6
18.IX - 22.IX	12.0	11.3	12.9	12.1	13.5	12.4	14.1	14.5	11.9	14.1	12.6	12.3	13.7	11.3	12.8	11.9	12.6	13.0	12.4
23.IX - 27.IX	9.5	9.2	9.2	8.9	9.3	8.9	10.3	9.6	9.8	10.0	9.4	8.7	10.8	10.9	11.7	12.3	11.6	11.6	10.5
28.IX - 2.X	7.2	7.2	7.1	7.2	5.9	6.8	7.9	7.7	7.4	7.4	6.5	5.6	8.1	8.1	8.5	8.1	8.1	8.1	8.1
3.X - 7.X	7.9	7.9	7.9	10.2	8.6	8.5	7.9	9.2	6.4	7.3	6.5	4.6	6.3	3.8	4.5	4.0	3.5	3.5	3.5
8.X - 12.X	8.0	8.2	8.5	9.0	9.7	6.2	8.7	10.4	8.0	9.6	8.7	8.2	9.5	6.8	7.6	6.2	4.5	4.5	4.5
13.X - 17.X	10.1	9.7	9.3	10.4	9.9	9.5	12.6	10.6	11.5	10.7	10.1	8.5	10.9	7.6	8.9	8.6	7.2	7.2	7.2
18.X - 22.X	4.8	5.1	5.6	5.8	7.2	6.6	7.3	8.7	5.5	7.4	4.8	4.2	8.4	6.5	7.9	7.7	7.1	7.1	7.1
23.X - 27.X	8.0	7.5	8.6	9.8	9.7	11													